Technical Report and Resource Estimation for the Longstreet Property, Nye County, Nevada

Prepared for

Star Gold Corporation

By

Paul D. Noland

CPG, QP and Consulting Geologist

December 8, 2025

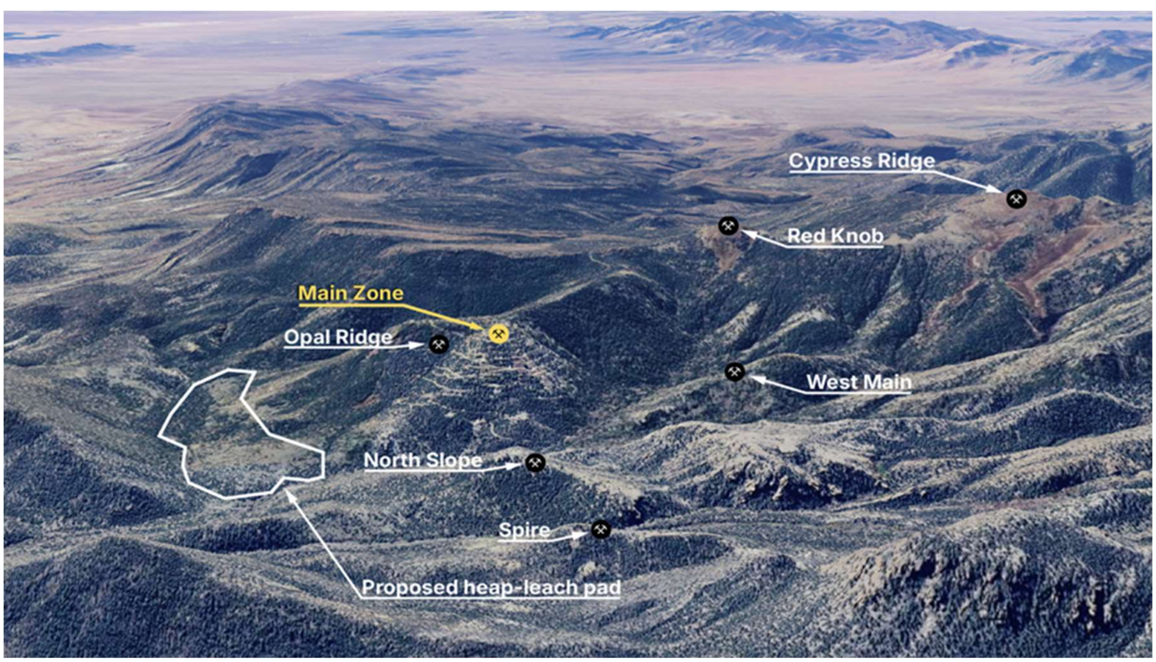

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Table 6-1 Exploration History

Star Gold Corp. – Longstreet Au-Ag Project, Nevada

Year	Company	Type of Work						Remarks
		Geology	Lithogeochemical Sampling	Drilling				
				RC		DD		
				ft.	No of Holes	ft.	No of Holes	
1903		v						Discovery of mineralized boulders?
1929	Gold Coin Company							Development of Golden Lion Mine (Main Zone)
1980	Keradamex / E & B	v	v			N/A	8	
1982	Minerva Exploration							Bulk sampling and resource estimation
1984-87	Naneco Resources Ltd.		v	54,221	332			Resource estimation, metallurgical test work & Prefeasibility study
1987	Cyprus Minerals Company					3,000	7	Property evaluation
2002	MinQuest Inc.	v	107					
2003	REM/Harvest Gold			11,285	32			Metallurgical testwork
2011	Star Gold Corp.	v	v	5,270	16			Property evaluation and preliminary resource estimation
2012	Star Gold Corp.			10,240	23	1,295	4	
2013	Star Gold Corp.			6,930	20			
Totals			**107+**	**87,846**	**423**	**4,293+**	**19**	

Source: Prenn, 1988, Noland, 2012 and Star Gold, 2012.

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1.0 Executive Summary

This report was prepared as an initial assessment level Technical Report Summary in accordance with the Securities and Exchange Commission (SEC) S-K regulations Title 17 for Star Gold Corporation (Star), by Paul D. Noland, CPG, QP.

Sections of this report were taken or modified and updated from previous technical reports prepared by Paul Noland, (Noland, 2012 and 2014) and Agnerian (2013). Paul Noland has no affiliation with Star Gold, nor does he own any stock of Star Gold.

1.1Property Description, Mineral Tenure, Royalties, Permits

The Longstreet Project (the Project, or Project) is located in northern Nye County, in the central part of the State of Nevada, USA. . The Project consists of 142, unpatented mining claims covering approximately 2,500 acres, located on United States Forest Service (USFS) and United States Bureau of Land Management controlled land. The resource and primary exploration areas fall within land controlled by the USFS.

Star Gold Corp. (Star) entered into an exclusive option agreement with MinQuest on the Longstreet Project in December, 2010. This option agreement gave Star the right to obtain a 100% interest in the Longstreet property, minus a 3% NSR royalty, by meeting the financial obligations outlined in the agreement.

Subsequent the execution of the MinQuest option agreement, all terms and payments have been satisfied. Consequently, Star now controls 100% ownership in the property minus the 3% Net Smelter Royalty (NSR) as per the initial MinQuest agreement. Star Gold holds an option with MinQuest to purchase up to one-half of the 3% NSR, resulting in a carried 1.5% NSR, for a one time cash price of $1.5 million USD.

Star has conducted exploration and drilling programs under permits with the United States Forest Service (USFS) which limit total surface disturbance to 5 acres (categorical exclusion). Star has since submitted an Exploration Plan of Operation (PoO) which will allow additional disturbances for further exploration and predevelopment activities. Approval of this PoO is expected in 4th quarter of 2025.

1.2 Geology and Mineralization

The Longstreet Project is located in the Nevada portion of the Basin and Range Province. This geological province is characterized by repeated episodes of compressional deformation in

Paleozoic and Mesozoic time followed by extensional deformation and extensive magmatism and volcanism in Cenozoic time.

The Longstreet Project is located in the Monitor Range, adjacent to the northwest trending Walker Lane volcanic-hosted gold trend that includes such world-class deposits as the Comstock and Goldfields mining camps.

Local Geology at Longstreet is characterized by moderately to poorly welded rhyolite ash-flow tuff containing conspicuous exotic lithic fragments and pumice. A thin discontinuous unit of volcaniclastic and siliceous sediments , including sinter is deposited upon the ash-flow tuff unit. units. Altogether these volcanic ash flow units host Siliceous alteration resulting in the development of gold and silver bearing, sheeted quartz vein systems.

The tectonic fabric on the Longstreet Project includes two Main directions of faulting/fracturing that have an influence on the mineralization. An east-trending steeply north-dipping system of fractures and faults has been noted at five of the seven gold / silver zones on the. Quartz – adularia – limonite veins / veinlets and 'rusty fractures' following this trend contain gold mineralization. The other important gold / silver-bearing fault/fracture direction is 300-330° with steep north dips, and is characterized by sheeted quartz veins / veinlets and 'rusty fractures'. This mineralized trend occurs at all seven of the gold / silver zones known on the Longstreet Project. Major displacement is not a feature of these structures.

1.3 Exploration and Drilling

Star and MinQuest have conducted several episodes of systematic rock chip sampling and drilling in the 'modern era' of exploration since 2002. Detailed rock chip sampling conducted by MinQuest over the entire property resulted in the definition of numerous exploration 'targets', only some of which have been tested by drilling.

Prior to 2002, several mining and exploration companies conducted drilling and other exploration activities at Longstreet. Star currently has reliable data for 364 historical drill holes representing over 66,000 feet of drilling. Most of these drill holes and the assays and logs associated with them were determined to be valid and reliable for use in the current resource estimation. The validation process of these old drill holes consisted partly of two separate 'twin drill' programs, where historical holes were duplicated with modern drilling, and the results were compared statistically.   The Author and QP of this report has verified the validity of all drill holes utilized in the current resource.

In total, Star has completed 63 drill holes for a total of 23,735 feet at Longstreet. Almost all of the drilling has been conducted within the 'Main' target zone. The current resource is confined to the 'Main' zone.

1.4 Resource Estimate

A mineral resource estimation has been prepared for the Longstreet Project. The resource estimate is confined to the Main Target Zone . Both an Indicated Mineral Resource and an additional Inferred Mineral Resource have been determined. The resource is summarized in Table 1-1 below:

A Table 1-1 Longstreet Resource Summary

Table 1-1: Longstreet Resource Summary							
Category	Tonnage	AuEq (opt)	Au (opt)	Ag (opt)	AuEq (oz)	Au (oz)	Ag (oz)
Indicated	8674951	0.0199	0.0131	0.4118	172944	113409	3571986
Inferred	2399648	0.0167	0.0079	0.5284	40138	19005	1267945
Total	11074599	0.0192	0.0120	0.4370	213082	132414	4839931
Pit	30263060	Lower cutoff grade: 0.005 opt AuEq					
Waste	19188460						
Strip Ratio	1.73						

The resource provided and described in this report was initially created and designed to meet the standards and definitions of CIM and NI 43-101 as part of an NI 43-101 Technical Report and Resource estimation on the Longstreet Project (Noland, 2014).

The definitions and standards utilized are described below:
"*In this Instrument, the terms "mineral resource", "inferred mineral resource", "indicated mineral resource" and "measured mineral resource" have the meanings ascribed to those terms by the Canadian Institute of Mining, Metallurgy and Petroleum, as the CIM Standards on Mineral Resources and Reserves Definitions and Guidelines adopted by CIM Council on August 20, 2000, as those definitions may be amended from time to time by the Canadian Institute of Mining, Metallurgy, and Petroleum."*

Further definitions and standards adhered to in this report are summarized here:

*"A **Mineral Resource** is a concentration or occurrence of natural, solid, inorganic or fossilized organic material in or on the Earth's crust in such form and quantity and of such a grade or quality that it has reasonable prospects for economic extraction. The location, quantity, grade, geological characteristics and continuity of a Mineral Resource are known, estimated or interpreted from specific geological evidence and knowledge."*

The terms Measured, Indicated and Inferred as used in this report adhere to the following definitions:

"A ***'Measured Mineral Resource'*** *is that part of a Mineral Resource for which quantity, grade or quality, densities, shape, physical characteristics are so well established that they can be estimated with confidence sufficient to allow the appropriate application of technical and economic parameters, to support production planning and evaluation of the economic viability of the deposit. The estimate is based on detailed and reliable exploration, sampling and testing information gathered through appropriate techniques from locations such as outcrops, trenches, pits, workings and drill holes that are spaced closely enough to confirm both geological and grade continuity."*

*"An '***Indicated Mineral Resource***' is that part of a Mineral Resource for which quantity, grade or quality, densities, shape and physical characteristics, can be estimated with a level of confidence sufficient to allow the appropriate application of technical and economic parameters, to support mine planning and evaluation of the economic viability of the deposit. The estimate is based on detailed and reliable exploration and testing information gathered through appropriate techniques from locations such as outcrops, trenches, pits, workings and drill holes that are spaced closely enough for geological and grade continuity to be reasonably assumed."*

*"An '***Inferred Mineral Resource***' is that part of a Mineral Resource for which quantity and grade or quality can be estimated on the basis of geological evidence and limited sampling and reasonably assumed, but not verified, geological and grade continuity. The estimate is based on limited information and sampling gathered through appropriate techniques from locations such as outcrops, trenches, pits, workings and drill holes."*

The 2014 resource is presented here unmodified. The author is aware that SK 1300 definitions vary slightly from those of NI 43-101. However, it is the author's opinion that the methods and data utilized are sufficient to meet current SK 1300 criteria for 'indicated' and 'inferred' resource.

The author further recognizes that current metals prices would certainly impact factors such as the gold-silver equivalency (AuEq) and cut off grades in a new resource calculation. However, the 2014 resource, as presented here, is considered to be a valid 'base line' resource until additional drilling, resource development and definition, metallurgical testing and economic analyses are completed for Longstreet.

1.5 Data Verification

1.5.1 Verification of Historical Drill Data

Information on sampling procedures during geochemical sampling and RC drilling programs carried out by Keradamex/E & B, Minerva, Naneco, and REM/Harvest Gold in the 1980s and 1990s, is not available at this time. Sampling was done at 2 ft., 5 ft., and 10 ft. intervals. The bulk of the sampling, however, was done at 5 ft. intervals, and sampling was done throughout the entire hole. In general, samples from earlier drilling were assayed mainly for gold and silver. The exact methods of gold and silver determinations, however, are not available.

It is the author's opinion that data from these historical programs were collected using methods and safeguards common and prevalent at the time, and that no bias was likely introduced by the operators. The use of these drill holes in a resource estimation must be made on a 'case by case' basis and the determination of validity conducted by the QP based on availability of data, proximity to 'twin' drilling or validation by other geologic considerations.

Further attempts at 'verification' of historical drilling were made by conducting 'twin drilling' programs whereby historical drill holes are duplicated as closely as possible with new drilling and the assay results compared. Two separate 'twin drilling' programs have been conducted at Longstreet as a way of verifying validity of historical drilling.

1.5.2 Verification of Star and MinQuest Drill Data

During the most recent work by Star Gold (2010-2013) sampling of drill chips was done by MinQuest technical personnel contracted by Star Gold. Sampling procedures during the drilling programs included splitting the drill chips using a two-way wet sample splitter, at 5 ft. sample intervals, under the supervision of the Project Geologist. Material from one half of the sample (A sample) was put in securely sealed bags and sent to the ALS sample preparation laboratory in Reno, Nevada. ALS carries ISO certification. Samples were numbered on the sample bags, according to the drill hole number and footage of the hole. The other half of the sample (B sample) was kept at the site for future reference. The chain of custody of logging and sampling was the responsibility of the Project Geologist.

All drilling data utilized in the resource estimation was verified by the author, including available historic QA/QC measures. Assay certificates for current and historic drilling were inspected by the author, compared to assay tables utilized in resource calculations, and thereby confirmed. The author also has inspected the assay certificates from surface and underground sampling conducted at Longstreet by MinQuest and can verify the results as presented in this report.

1.6 Conclusions and Recommendations

The Longstreet project has a demonstrated resource which appears to be economically viable for open pit, heap leach mining and recovery. The next phase(s) of work should be designed to enhance the known resource, demonstrate economic viability and further define operating parameters.

A series of studies is proposed to accomplish these objectives. Additionally, a limited exploration drilling program is proposed to enhance the known resource. A production well is proposed in order to reduce drilling and operational costs as the project moves forward, and two water monitoring wells are proposed to allow a base line and facilitate future permitting requirements.

Estimated budget for these recommendations is $1,740,000 USD. A breakdown of this estimate is provided in Table 1-2 below:

B Table 1-2 Recommended Budget for Longstreet

Table 1-2. Recommended Budget for Longstreet

	#	Unit $	
Production Water Well	1	200,000	$ 200,000
Monitor Well	2	20,000	$ 40,000
RC Drilling	10000	100	$ 1,000,000
			$ -
PEA or similar study		100,000	$ 100,000
Updated Resource Estimate		100,000	$ 100,000
Initial Permits for Mining		100,000	$ 100,000
Engineering Mine Design		100,000	$ 100,000
Contingency (EIS, etc.)		100,000	$ 100,000
Total Estimated Recommendation Budget			**$ 1,740,000**

2.0 Introduction

2.1 Registrant for Whom the Technical Report was Prepared

This report was prepared as an initial assessment level Technical Report in accordance with Securities and Exchange Commission (SEC) S-K regulations (Title 17, Part 229, Item 1300) for Star Gold Corporation (Star).

2.2 Terms and References and Purpose of Report

The quality of information, conclusions, and estimates contained in this report as based on: 1) information available at the time of preparation, and 2) the assumptions, conditions, qualifications and definitions set forth in this report.

The author grants Star permissions to file this report as Technical Report Summary with the United States securities regulatory authorities pursuant to SEC S-K regulations. The responsibility for any disclosure is that of Star.

The Initial Assessment is preliminary in nature. It includes Inferred and Indicated Mineral Resources that are considered too speculative geologically to have necessary economic considerations applied to them which would enable them to be categorized as 'Mineral Reserves'. Mineral Resources have no demonstrated economic viability. There is no certainty that the resource nor the Initial Assessment will be realized.

2.3 Sources of Information

This report is based in part on internal data and reports from MinQuest and Star, including published and unpublished technical reports by various authors as cited throughout the report and noted in the References Section.

2.4 Details of Inspection

The author conducted site visits to the Longstreet Property on May 17, 2011, May 31, 2011 and on February 10-11, 2012. These visits were conducted to confirm existence of roads and historical drill sites, underground workings, and examine newly constructed and planned drill roads and sites.

The author visited several of the known exploration targets described in this report to examine the nature of outcrop geology, mineralization style and alteration.

In addition to the site visits to the Longstreet property, the author has on several occasions had opportunities to examine drill products, both core and chips from RC drilling.

2.5 Qualified Person

The author, Paul D. Noland, is the sole Qualified Person (QP) for this report. Paul D. Noland meets the definitions of QP as stated in 17. CFR section 229.1300. Details of qualifications are given in the Date and Signature page.

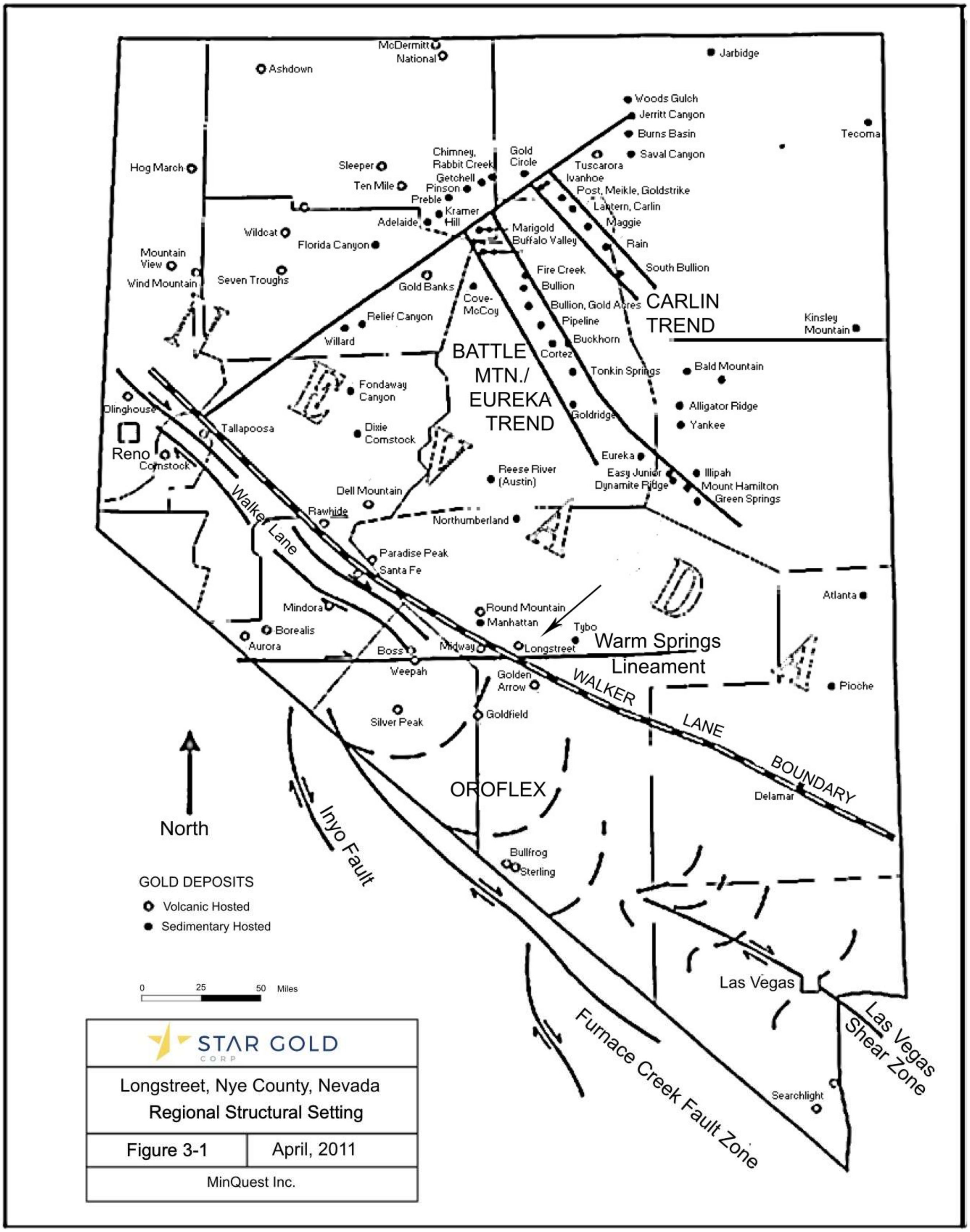
Sections of this report were taken wholly or partly from previous published and unpublished reports. In all cases, the veracity of this information has been verified by the current author and QP.

3.0 Property Description and Location

3.1 Property Description

The Longstreet Project (the Project, or Project) is located in northern Nye County, in the central part of the State of Nevada, USA (Figure 3-1). The project falls within the McCann Canyon and Georges Canyon Rim 7 1/2' topographic quadrangles. The Project consists of 142, unpatented mining claims covering approximately 2,500 acres, located on United States Forest Service (USFS) and United States Bureau of Land Management controlled land. The resource and primary exploration areas fall within land controlled by the USFS.

A Figure 3-1 Regional Structural Setting

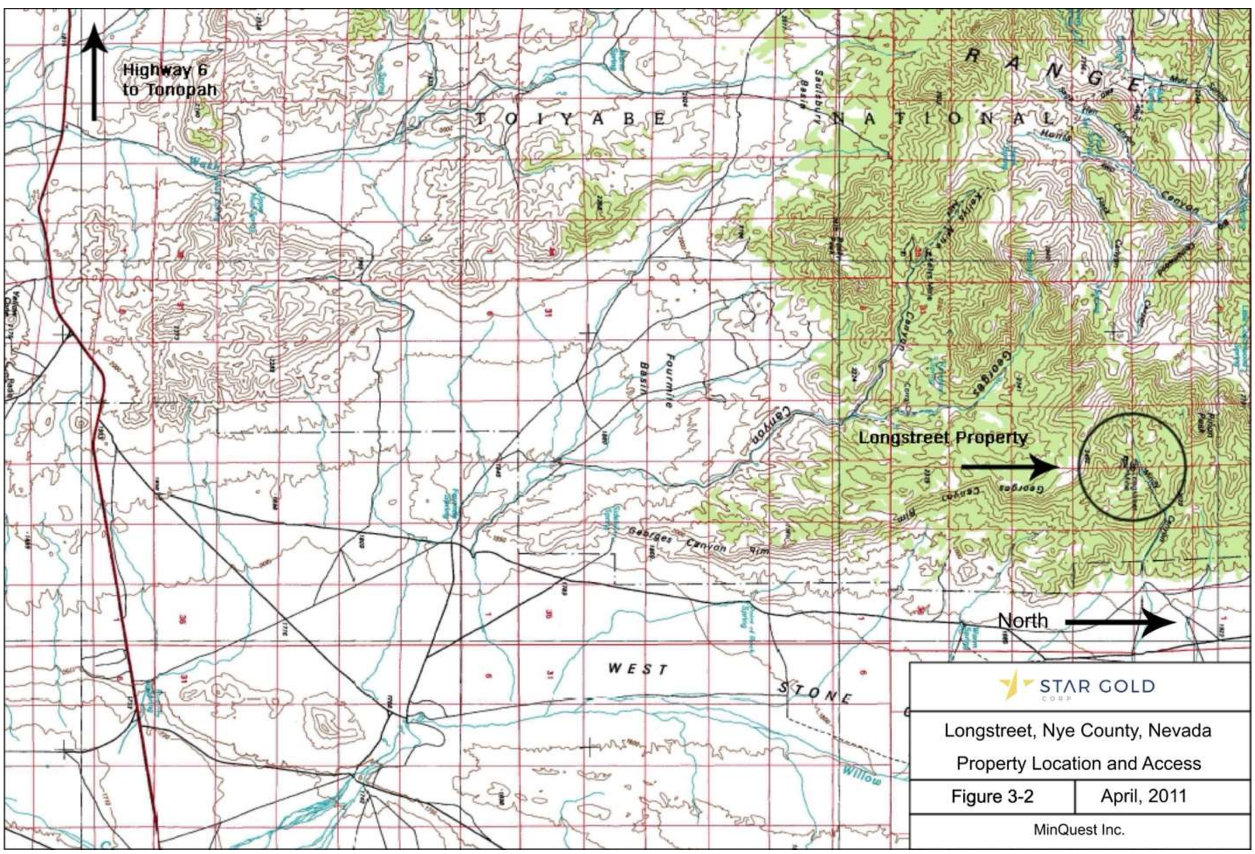


Star Gold has staked 26 claims (Leach Pad Claims) adjacent to the eastern boundary of the property, with the objective of providing the site for leach pads planned for future development of the Main Zone. These claims are included in the total of 142 claims making up the property holdings. These claims fall within land controlled by the BLM. In addition, Star Gold has staked 12 claims along a corridor leading from the main Longstreet property to the Leach Pad Claims.

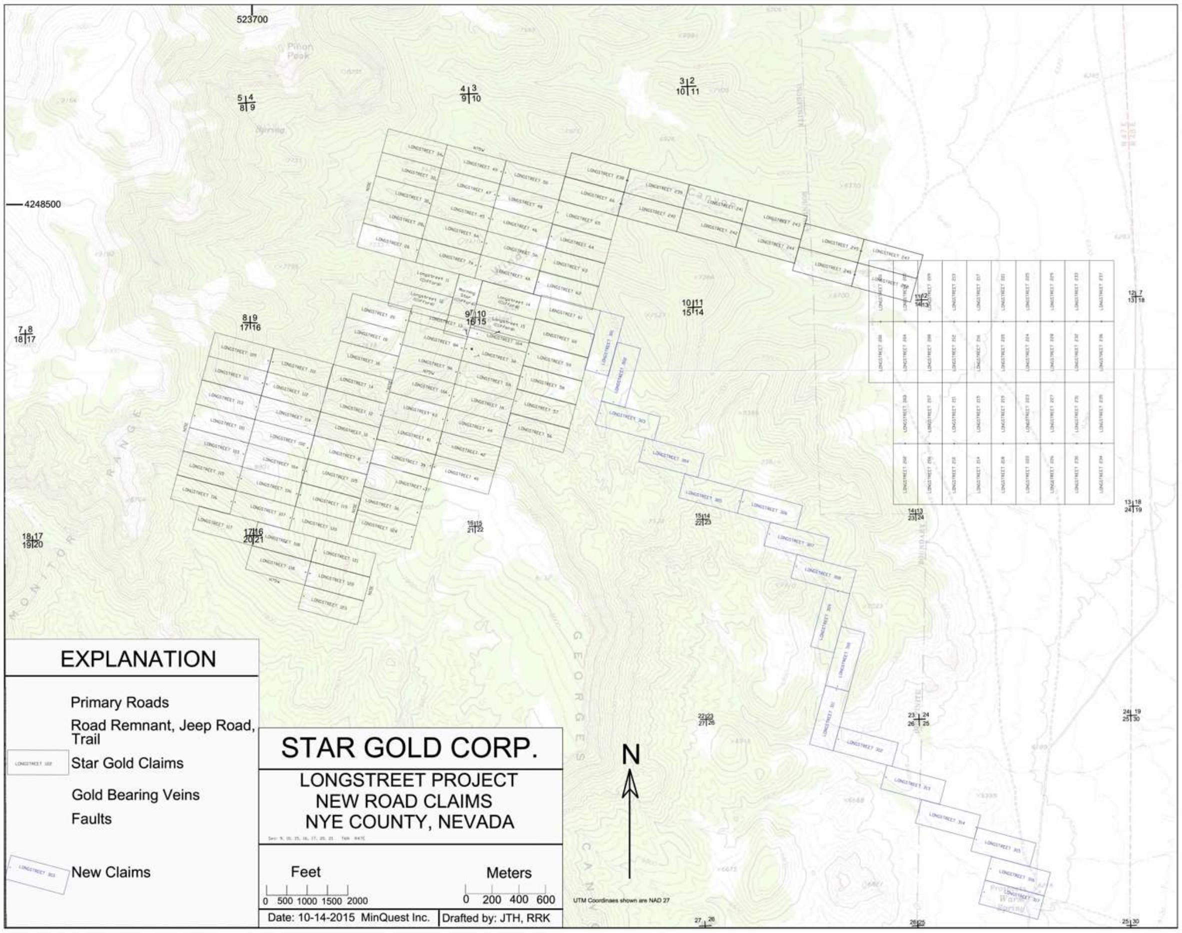
The claims are located in Sections 9, 10, 15, 16, 17, 20 and 21 of T6N, R47E, MDB&M, Nye County, Nevada (Figure 3-2). A list of claims is provided in Appendix 1, and a claim map of the property is provided as Figure 3-3. This location falls on the eastern slope of the Monitor Range and within the Monitor Range portion of the Humboldt-Toiyabe National Forest.

Unpatented mining claims allow the owner to explore for and mine mineral commodities on public land. Surface disturbances and mining activities are regulated by a series of permits issued by the State of Nevada and the Federal Government (BLM and USFS).

B Figure 3-2 Location and Access



C Figure 3-3 Longstreet Claim Map



3.2 Mineral Tenure

Star Gold Corp. (Star) entered into an exclusive option agreement with MinQuest on the Longstreet Project in December, 2009. This option agreement gave Star the right to obtain a 100% interest in the Longstreet property, minus a 3% NSR royalty, by meeting the financial obligations outlined in the agreement. Please refer to Table 3-1 below, for a summary of the payment schedule and expenditure obligations in the Star-MinQuest option agreement.

Subsequent the execution of the MinQuest option agreement, all terms and payments have been satisfied. Consequently, Star now controls 100% ownership in the property minus the 3% Net Smelter Royalty (NSR) as per the initial MinQuest agreement. Star Gold holds an option with MinQuest to purchase up to one-half of the 3% NSR, resulting in a carried 1.5% NSR, for a one time cash price of $1.5 million USD. A separate agreement covering 5 unpatented claims (the

Clifford agreement) has also been satisfactorily completed so that Star now owns 100% of those claims.

Figure 3-3 illustrates the land holdings. All the unpatented claims within the Longstreet Project have both U.S. Bureau of Land Management (BLM) and Nye County, Nevada fees paid and current through August 2026. Copies of receipts for the most recent annual claims fees for both Nye County, NV and the BLM are provided in the Appendices.

The U.S. Forest Service is responsible for the surface and subsurface mineral estate in the active exploration areas. Star Gold has conducted intermittent exploration activities, including exploration drilling, under a Plan of Operation with the local U. S. Forest Service (USFS) office in Tonopah. In July 2025, Star submitted an expanded Plan of Operation to the USFS to allow for additional resource and exploration drilling, water production well drilling, and monitor well construction. The Plan of Operation describes the proposed exploration and pre-mining activities and anticipated surface disturbances that will require reclamation. A reclamation plan and bond are part of the Plan of Operation (POO). The recently submitted POO is awaiting USFS approval. USFS approval is anticipated sometime in the 4th quarter of 2025. Meanwhile, Star continues to be permitted and bonded for casual exploration activities through the previous POO. USFS and BLM roads are open to the general public without permit requirement or fees.

C Table 3-1 Summary of Star Gold Option Agreement from 2009

Year No.	Payment (Cash)	Payment In Star Gold Shares (stock + options)*	Expenditure Obligation
On Signing	$20,000	50,000	
1	$0	50,000	$ 200,000
2	$20,000	50,000	$ 250,000
3	$30,000	50,000	$ 350,000
4	$30,000	50,000	$ 450,000
5	$50,000	50,000	$ 550,000
6	$50,000	50,000	$ 750,000
7	$50,000	50,000	$ 1,000,000

* Stock and Option payments for each of the years is broken into 25,000 shares of stock and 25,000 options 'at fair market value'.

3.2 Property Location and Access

The 142 claims making up the project are located in Sections 9, 10, 15, 16, 17, 20 and 21 of T6N, R47E, MDB&M, Nye County, Nevada (Figure 3-2). A list of claims is provided in Appendix 1, and a claim map of the property is provided as Figure 3-3. This location falls on the eastern slope of the Monitor Range and within the Monitor Range portion of the Humboldt-Toiyabe National Forest.

The Longstreet Au-Ag Project is located approximately 170 miles (275 km) northwest of Las Vegas and approximately 50 miles (80 km) northeast of Tonopah, a town of approximately 2,500 people, in west-central Nevada. The northeast-southwest oriented property extends approximately 1.8 miles (3 km) along strike within the Monitor Range. The geographic coordinates of the central part of the property are approximately 38°22'00"N Latitude and 116°40'00"W Longitude.

Access to the Longstreet Project area is by paved and gravel road. Access is by two-lane paved highway (Nevada HWY 6 to Warm Springs) approximately 30 miles (48 km) east from Tonopah, and then by gravel road (Stone Cabin Road) approximately 25 miles (40 km) north and a further 2.5 miles (4 km) west along a trail to Windy Canyon to reach the Longstreet property. The total distance from Tonopah to the property is approximately 57 miles (92 km). Supplies and heavy equipment are brought to the site by trucks, or other four-wheel drive vehicles. Currently, there is no permanent camp at the site. Casual labor would likely be sourced from Tonopah, Reno, Elko or Ely, Nevada. Experienced mining operations would likely be via contract and be sourced from Reno, Salt Lake City, Utah or other mining centers.

Production mining will be conducted by contract miners in order to reduce start up capital requirements. Star has already obtained a bid and proposal from N. A. Degerstrom of Elko, NV for contract mining and crushing. Other contract mining companies active in the region include Ledcor, Turner Mining Group, and Small Mine Development (SMD).

4.0 Climate, Local Resources, Infrastructure and Physiography

4.1 Physiography

The Monitor Range is about 100 miles long and from 5 to 15 miles wide. Summit elevations for most of its length are between 6,500 and 9,000 feet, with the highest point being approximately

10,000 feet. The Longstreet Project is located in rugged topography at the head of Windy Canyon, on the eastern slope of the Monitor Range (Figure 3-2). Elevations on the property range from about 6,000 feet in the northeast to 8,000 feet in the southwest part of the property. The hills are sparsely covered with pinion pine, juniper, sagebrush and greasewood. A mixture of mountain mahogany, willows, wild roses and various grasses occupy the valley bottoms.

4.2 Climate

Arid to semi-arid climatic conditions prevail in this part of Nevada. The annual precipitation is in the order of 5 inches (measured at Tonopah). Winter snowfall is typically about 6 inches, with the largest accumulations at elevations above 7,500 feet. Summer temperatures average 75 degrees F. in Tonopah, and winter temperatures average 23 degrees F. Prevailing climatic conditions allow year-round exploration and mining activities.

4.3 Infrastructure

Local infrastructure is available at Tonopah, Las Vegas or Reno. There is no infrastructure at the site, and electric power is provided by diesel generators. Infrastructure at Tonopah includes electrical power, internet service and limited road building equipment, and cell phone network. Reno and Las Vegas, although more distant, provide a full range of services and infrastructure typically associated with metropolitan areas of the Western USA. Potable water is provided in bottles, and industrial water is drawn from wells. Diamond and RC drilling equipment is available in Reno, and Elko, NV, and is also brought from other cities in neighboring States, such as Montana, Utah, Arizona or Idaho. For drilling programs, water is brought in by trucks from the Clifford Ranch. There is an airstrip close to Tonopah, but there is no regular commercial air service between Tonopah and Las Vegas or Reno.

Star intends to permit for and construct production water wells during a subsequent phase of work at Longstreet in preparation for mining. Once at least one of these wells is completed, water for drilling and all other needs will be supplied on site.

Electrical power requirements for any future mining operations on the Longstreet Project need to rely on diesel generators, and process water can be obtained from aquifers located in Windy Canyon. The detailed technical study by MDA in 1988 indicates that an open pit heap-leach mine exploiting the Longstreet Main Zone would have sufficient space for waste and tailing disposal storage (MDA, 1988).

5.0 History

5.1 Property History Prior to MinQuest and Star Gold Corporation

The Property was discovered in the early 1900's, but had limited development work until the 1920's. A 1929 report and maps show development of the "Golden Lion Mine" on two levels spaced 75 meters apart vertically (J.M. Butler, 1935). The report indicates the Golden Lion Mine operators targeted '300,000 tons of vein material' averaging 0.20 oz/ton (6.8 g/t) gold and 8 oz/ton (274 g/t) silver. The basis for this tonnage is not clear, but grades are confirmed by select underground sampling. A mill was constructed, the remnants of which are still on the property. However, the small stopes underground and very limited tailings material below the mill indicate very little mining was done and the operation was abandoned. For this reason, the current resource does not take into account the removal of any significant material by historic mining activities. This is explained in greater detail in the 'Resource' section of this report.

The following discussion provides several accounts of historic 'resource' estimates at the Longstreet property. Each is identified by source and references are provided. The resource estimates were conducted by reputable companies in an attempt to arrive at economic evaluations of mining potential at Longstreet. For this reason, they are considered relevant and reliable. Each of the historic resources appears to utilize drill data available at the time, and underground sampling in combination to derive what they refer to as 'indicated', or 'drill inferred' resources. However, the historical reports presented here do not define 'indicated' or 'inferred', nor do they always distinguish between 'resource' and 'reserve'. Therefore, the categories utilized in these historic reports do not adhere to current NI 43-101 or SK 1300 categories or definitions of 'resource' or 'reserve'. The differences are not certain, since the methods used in the historic accounts are not sufficiently detailed. It was determined that a current, NI 43-101 or SK 1300 compliant resource estimate required more modern drilling accompanied by a documented QA/QC program, and that these historic resources could not be 'upgraded' or 'converted' to NI 43-101 or SK 1300 compliant resources by any available means. One of the objectives of recent drilling at Longstreet has been to confirm much of the historic data utilizing methods suggested by NI 43-101 and SK 1300 standards. Neither the current author nor any other Qualified Person has done sufficient work on the historic estimates to classify them as current resources or reserves. Consequently, none of the historic resources or reserves reported below are treated by Star, or in this report, as 'current mineral resources or mineral reserves'.

The property lay idle until 1980 when Keradamex Inc. and E & B Exploration formed a joint venture to explore the property. The venture conducted soil and rock chip geochemical surveys, limited underground sampling and drilled seven (one was abandoned) angle core holes into the Main mine workings area. Details for much of the historic drilling are missing or only partially available. A summary of known drilling activity during significant exploration efforts is summarized in Table 5-1. Keradamex drilling revealed the presence of fracture related gold mineralization up to 36 meters thick extending into the hanging wall of the vein structure. Gold mineralization within this zone averaged 0.02- 0.528 oz/ton (0.7-18.1 g/t) and revealed the presence of a heap leachable target.

D Table 5-1 Historic Drilling Summary

Date	Company	No. of Holes	Total Footage
1980	Keradamex	7	NA
1982-1983	Minerva	0	(UG Sampling, no drilling)
1984-1997	Naneco	approx. 500	NA, RC and air track
1987	Cyprus	7	3,000
2002-2005	R.E.M.	30	11,000

5-1

None of the historic resource estimates described below have been verified by current author, and are not treated or presented as current mineral resource estimates. They do not adhere to any of the NI43-101or SK 1300 resource categories. None of the historic resources listed above or below in this section of the report meet the criteria of any of the 'resource' categories defined by NI43-101 standards, CIM or SK 1300 definitions. Consequently, these historic resource estimates should not be relied upon for current property evaluations or investment recommendations.

In 1982 Minerva Exploration optioned the property and initiated an underground sampling program. In 1983 a joint venture was formed with Geomex Canada Resources Ltd. Derry, Michener, and Booth were commissioned to assess the property and conducted underground sampling, bulk sampling and metallurgical testing. They concluded there were reserves* of 60,000 tons averaging 0.11 oz/ton (3.8 g/t) gold and 5 oz/ton (171 g/t) silver.

In early 1984 Naneco Resources Ltd., an Alberta company, acquired all of the assets of Minerva and an additional 10 percent interest in the property from Geomex. As operator, Naneco immediately initiated drilling. In 1985, with over 200 RC holes drilled, the venture announced an oxidized 'drill inferred reserve'* (not defined) of 850,000 tons averaging 0.079 oz/ton (2.7 g/t) gold and 1.1 oz/ton (38 g/t) silver along with an additional low grade reserve* of 1.5 million tons averaging 0.021 oz/ton (0.72 g/t) gold and 0.4 oz/ton (14 g/t) silver.

During the next few years Naneco increased its interest from 53 percent to 100 percent, conducted additional metallurgy, economic evaluation and drilling. In 1988, Naneco retained Mine Development Associates (MDA) of Sparks, Nevada, to carry out a Prefeasibility study on the Longstreet property. As part of this Prefeasibility study, Kappes, Cassiday and Associates (KCA) of Sparks carried out metallurgical testwork (bottle roll) on a representative composite of mineralized material from 31 RC drill holes (Prenn, 1988). Results of this metallurgical testing is provided in a later section of this report.

Naneco's last reported resource indicates a "drill proven reserve"* of 140,000 ounces of gold. At least 492 RC holes have been drilled, most within the Main resource area. Naneco's last announcement also states that total property potential is "considerably higher than the 280,000 ounces currently believed to exist". Unable to raise money because of falling gold prices and strapped with high land payments to the claim owners, Naneco dropped the property in 1998.

MinQuest acquired it shortly thereafter. The Cyprus Ridge target, which was evaluated by Cyprus Minerals Company in 1987 was acquired by MinQuest in early 2002.

The property was optioned to Rare Earth Metals Corp. (REM) in May of 2002. REM later changed its name to Harvest Gold. Mapping and geochemical sampling of the 7 targets shown in Figure 6-3, Longstreet Targets, was completed in October, 2002. From 2003 through 2005 REM drilled 30 holes into Main totaling 3,350 meters (11,000 feet). The drill holes were angled toward the intersection of the two primary sheeted vein sets. Results showed a 20% improvement in average grade over vertical drilling. REM relinquished rights to the Longstreet property back to MinQuest in August 2009.

MinQuest and Star Gold Corp. agreed to terms for an option/purchase agreement in late 2009. The agreement between MinQuest and Star Gold was executed in January 2010.

*These stated historical 'reserves' are not defined and do not meet standards set by NI 43-101 or SK 1300 for mineral resources or reserves. They are presented here for reference.

5.2 Property Exploration Under MinQuest and Rare Earth Metals 2002-2005

From 1998 to 2002, MinQuest carried out detailed geological mapping and lithogeochemical sampling over various target areas. Assay values of the 107 samples collected by MinQuest ranged from 0.02 g/t Au to 35.45 g/t Au and from 0.1 g/t Ag to 108 g/t Ag. At the Cyprus Ridge target area, assay values of 50 samples ranged from 0.03 g/t Au to 11.6 g/t Au, with an average value of approximately 0.5 g/t Au and 0.1 g/t Ag to 47 g/t Ag, with an average value of 7.2 g/t Ag. Based on these results, MinQuest concluded that "the gold values are leakage anomalies from a deeper boiling zone" and considered the Cyprus Ridge as a high priority target area (Noland, 2012).

MinQuest crews sent the samples to ALS Minerals (ALS) in Reno, Nevada, for sample preparation, and then to ALS Minerals Laboratories in North Vancouver, British Columbia for Au and Ag assays. Results from this program are provided in are summarized in Table 5-2 below.

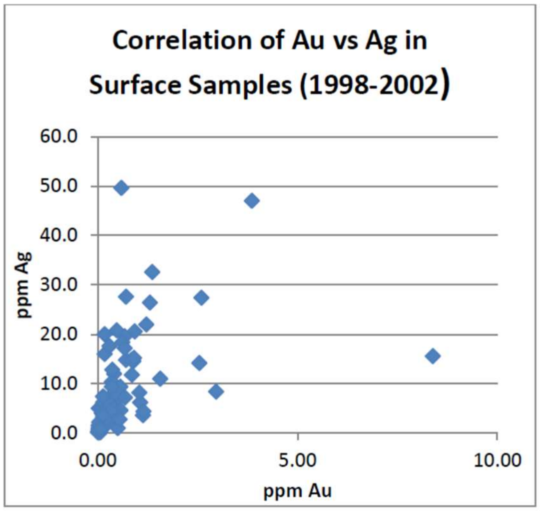
E Table 5-2 Surface Geochemical Sampling Results (199-2002)

Table 5-2 Surface Geochemical Sampling Results (1998-2002)							
Star Gold Corp. – Longstreet Au-Ag Project, Nevada							
Target Area	**No. of Samples**	**Range of Assay values**					
		g/t Au			**g/t Ag**		
		From	**To**	**Average**	**From**	**To**	**Average**
Main Zone	3	0.38	35.45	12.4	3.5	108.0	48.0
Opal Ridge	15	0.02	0.27	0.15	0.6	9.2	2.3
NE Main	2	0.11	0.93	0.52	4.0	20.6	12.3
North	12	0.03	18.14	1.93	0.6	49.6	15.2
Spire	8	0.03	0.45	0.24	0.4	20.0	9.7
Knob Hill	17	0.03	2.97	0.61	0.1	27.4	7.5
Cyprus Ridge	50	0.03	11.16	0.90	0.1	47.0	7.2
Total	**107**	**0.02**	**35.45**		**0.1**	**108.0**	

Table 5-2 In May 2002, Rare Earth Metals Corp. (REM) optioned the property from MinQuest and carried out geological mapping and geochemical sampling over the Main Zone as well as six other target areas. Later in that year, REM changed its name to Harvest Gold Inc. (Harvest Gold), and from 2003 to 2005, Harvest Gold completed approximately 3,440 m (11,285 ft.) in 32 inclined RC drill holes on the Main Zone. In August 2009, Harvest Gold returned the property to MinQuest.

Results from the MinQuest lithogeochemical sampling program indicate that, with few exceptions, there is good correlation between gold and silver values, as shown in Figure 5-1.

D Figure 5-1 Au vs Ag Correlation



5.3 Property Exploration Star Gold 2010-2013

In January 2010, Star Gold entered into an option agreement with Messrs. Kern and Duerr of MinQuest to earn a 100% interest in the Longstreet property, and commenced a systematic exploration program, including 1,728 m (5,270 ft.) of drilling in 16 RC holes and lithogeochemical sampling completed in 2011. All of the 2011 drilling by Star Gold was done on the Main Zone.

From August 5 to October 19, 2012, Star Gold completed 3,122 m (10,240 ft.) of drilling in 23 RC holes and 395 m (1,295 ft.) of diamond drilling in four holes (LS-1216C, LS-1217C, LS-1222C, and LS1224C). Detailed discussion on exploration by Star Gold is provided in the Drilling section.

From May 8 to July 29, 2013, Star Gold completed approximately 2,123 m (6,930 ft.) of drilling in 20 RC holes. Detailed discussion on exploration by Star Gold is provided in the Drilling Section.

Exploration data indicate that work done to date has been concentrated on the Main Zone in the central part of the property, and the target areas tested by drilling cover less than 10% of the total area interpreted to host gold-bearing veins and fracture zones within the rhyolitic tuffs of the Longstreet property. The Author is of the opinion that additional drill testing of the remaining target areas is warranted.

To date, Star Gold has spent approximately $1,500,000 on exploration on the Longstreet property, including option payments (Star Gold, 2012 and 2013). Table 6-2 is a summary of the exploration on the Longstreet property.

Additional details of historical exploration and drilling is provided in the EXPLORATION and DRILLING Sections of this report, below.

F Table 6-1 Exploration History

Table 6-1 Exploration History

Star Gold Corp. – Longstreet Au-Ag Project, Nevada

Year	Company	Type of Work						Remarks
		Geology	Lithogeochemical Sampling	Drilling				
				RC		DD		
				ft.	No of Holes	ft.	No of Holes	
1903		v						Discovery of mineralized boulders?
1929	Gold Coin Company							Development of Golden Lion Mine (Main Zone)
1980	Keradamex / E & B	v	v			N/A	8	
1982	Minerva Exploration							Bulk sampling and resource estimation
1984-87	Naneco Resources Ltd.		v	54,221	332			Resource estimation, metallurgical test work & Prefeasibility study
1987	Cyprus Minerals Company					3,000	7	Property evaluation
2002	MinQuest Inc.	v	107					
2003	REM/Harvest Gold			11,285	32			Metallurgical testwork
2011	Star Gold Corp.	v	v	5,270	16			Property evaluation and preliminary resource estimation
2012	Star Gold Corp.			10,240	23	1,295	4	
2013	Star Gold Corp.			6,930	20			
Totals			**107+**	**87,846**	**423**	**4,293+**	**19**	

Source: Prenn, 1988, Noland, 2012 and Star Gold, 2012.

6.0 Geological Setting

6.1 Regional Geology

The Longstreet Project is located in the Nevada portion of the Basin and Range Province. This geological province is characterized by repeated episodes of compressional deformation in Paleozoic and Mesozoic time followed by extensional deformation and extensive magmatism and volcanism in Cenozoic time. Gold deposits are often described as being associated with ‘mineralization trends’, that are a reflection of deep crustal structures and magmatism, such as the ‘Walker Lane’ and the ‘Carlin Trend’. The Longstreet Project is located in the Monitor Range, adjacent to the northwest trending Walker Lane volcanic-hosted gold trend that includes such world-class deposits as the Comstock and Goldfields mining camps (Figure 3-1).

The Monitor Range is a westward-tilted fault block that has been elevated by normal faults along its eastern front, and is typical of the uplifted mountains of the Basin and Range Province. The ranges are topographic highs rising above alluvium-filled valleys generated by Tertiary extensional tectonics. Central Nevada was an area of intense Oligocene – Miocene ash-flow volcanism that created numerous calderas and their outflow products. At least 13 calderas that range in age between 32 and 22 Ma have been mapped or interpreted in the area extending from the Shoshone Mountains eastward to the Monitor Range (see Figure 6-1). The southern Monitor Range consists mainly of Tertiary age volcanics and hypabyssal rocks related to the eruption of the Big Ten Peak volcano and a nearby unnamed 29 Ma caldera (Kleinhampl and Ziony, 1985) intruding and overlying Paleozoic sedimentary and metamorphic rocks (Figure 6-1).

The Paleozoic rocks are thrust-faulted marine sedimentary rocks comprised of quartzite, argillite and limestone of Cambrian, Ordovician and Silurian age. Minor amounts of Permian marine sediments (Palmetto Formation?) are also present in the Georges Canyon area.

In the southern Monitor Range Tertiary age volcanic rocks comprise more than 90% of the exposed bedrock (Figure 6-2). These rocks are more than 1 km thick and are predominantly flat-lying. Early Oligocene to early Miocene rhyolitic to dacitic ash-flow tuffs, with rhyolitic welded tuff are the thickest and most extensive units. Most of the Tertiary intrusions in the region are rhyolitic, but several small dacitic to andesitic dikes are present in the Georges Canyon area.

Mineral deposits in this part of the Basin and Range Province are varied and widespread and some of them have (had) substantial metal production. The producing Round Mountain gold deposit is about 25 miles northwest, and the past-producing Manhattan Mining Camp (gold/silver) is about 20 miles west-northwest of the Longstreet Property.

The Round Mountain Mine is a giant among epithermal precious metal deposits hosted by volcanic rocks, and the mineralization is a classic example of low sulphidation epithermal gold mineralization (White and Hedenquist, 1995). Gold deposits were discovered at Round Mountain in 1906 (Shawe, 1982) and by 1959 about 410 thousand ounces (troy ounces) of gold had been produced from placer and narrow vein lode deposits. Current production by open-pit mining methods commenced in 1977. Kinross (2010) reported an annual production for 2010 at 184,554 ounces of AuEq, with over 66 million tons of proven and probable reserves.

The oxidized ore is described as a closely spaced set of steeply dipping veins and veinlets following northwest-trending faults and associated joints over broad areas. Significant gold mineralization is not found in northeast-trending faults and fractures. The vein/veinlet system contains quartz, adularia, limonite (oxidized from pyrite), manganese oxide and associated native free gold. Flat veins are similar to the steep veins in character and mineral content, but with more brecciation of the wall rocks. Gold contents also appear to be higher in the flat veins. The adularia in the ore related veins is dated at 25.9 to 26.6 Ma, which is indistinguishable from the age of the enclosing ‘Tuffs of Round Mountain’ welded ash flow tuffs. These tuffs were erupted from the Round Mountain caldera and were deposited within the caldera (Henry, Castor and Elson, 1996). The author notes here that both the nature of the host rocks and style of mineralization at Longstreet is very similar to that at the Round Mountain Mine.

Hydrothermal alteration associated with the bulk mineable ore is evidenced by silicification and the replacement of magmatic feldspar by hydrothermal feldspar engendered by a potassium-rich hydrothermal fluid (Sander, 1988). Resources at Round Mountain as of December 31, 2010 included measured and indicated resources of 46 million tons grading 0.75 g/t Au, and 'Proven and Probable' reserves of 66 million tons grading 0.62g/t Au (Kinross 2010 Annual Report). The resource categories are NI 43-101 compliant.

The Manhattan gold / silver camp is located approximately 20 miles west-northwest of the Longstreet Mine and is an example of Tertiary epithermal mineralization superimposed on Paleozoic sedimentary rocks. Gold / silver deposits were discovered at Manhattan in 1905 (Shawe, 1982) and by 1959 about 10,500 kg of gold and 4,400 kg of silver had been produced from placer and lode deposits. The lode deposits in the Manhattan district are of a variety of types, although they occur together in a coherent belt about 1 km wide, which follows the south side of the Manhattan caldera for about 10 km. The most productive deposits formed in strongly faulted argillite and quartzite of the Cambrian age Gold Hill Formation. The generally north-trending zones of mineralized fractures are stockworks containing quartz, adularia, pyrite (oxidized to limonite) and native gold similar to the sheeted zones at Round Mountain. The silver production recorded for this camp is related to electrum and various silver-bearing sulphosalts.

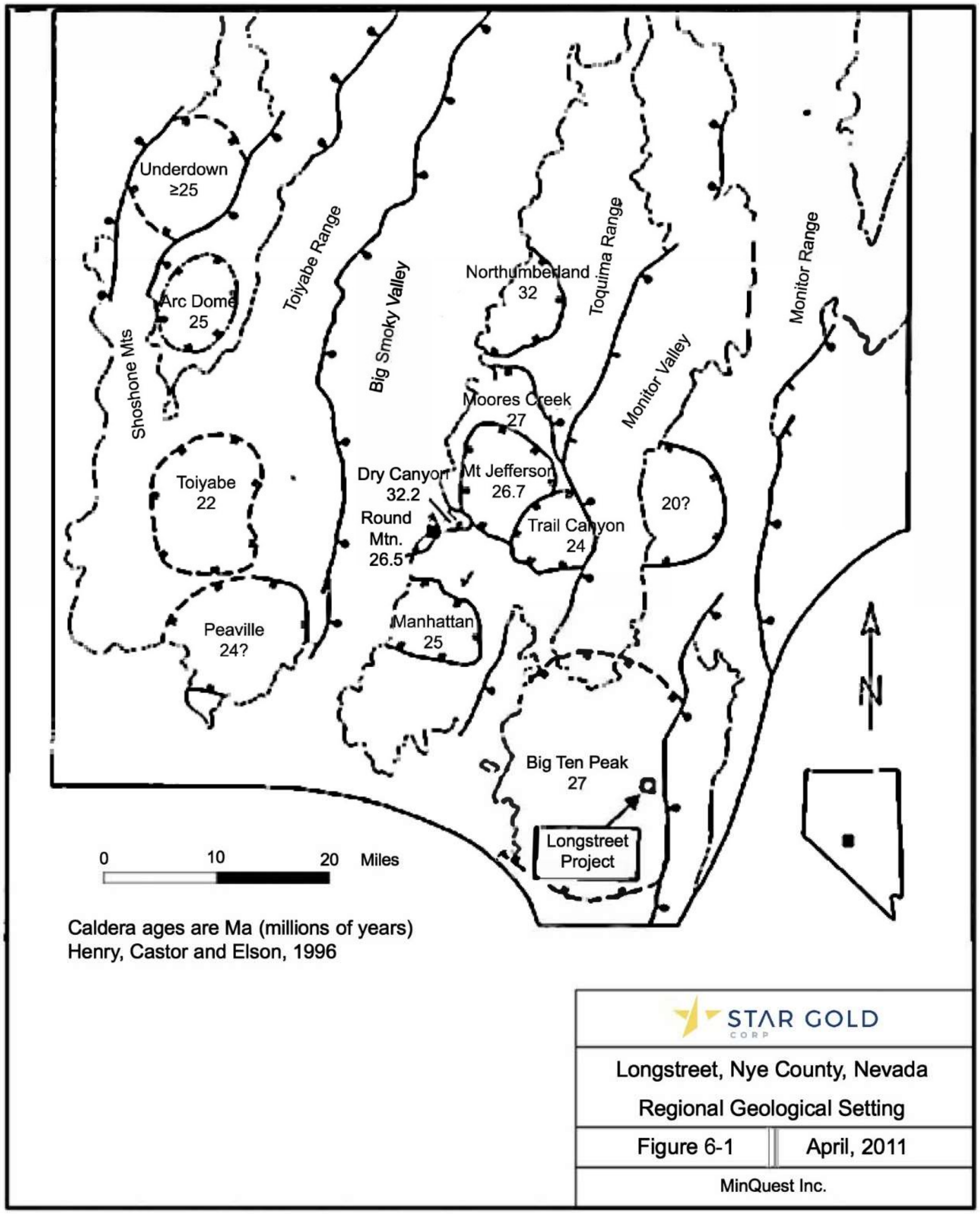
The Clipper Mine located approximately 5 miles southwest of the Longstreet Mine near Murphy Camp was discovered in 1903 and was worked intermittently until 1943. The mine was initially developed during World War I and included a 175 foot shaft and a 370 foot adit. Recorded production is about $12,000 (current 1951dollars) from mineralization having a gold: silver ratio of 1:1 and assaying from $34-124 per ton (1951 dollars). Host rocks are welded rhyolite ash-flow tuffs similar to the Longstreet mine (Kleinhampl and Ziony, 1984).

The Little Joe Claim located 6 miles south-southwest of the Longstreet Mine was developed by a 75 foot inclined shaft. Gold-bearing veins in ‘rhyolitic tuff’ were mined but production details are lacking.

Mineralization on the Last Chance claims located 11 miles west-northwest of the Longstreet Mine and southwest of Big Ten Peak was discovered in the 1920s. Mineralization consists of argentiferous galena, minor sphalerite and pyrite occurring in irregular pipes and chimneys generally at the intersection of cross faults within a northwest-trending shear zone in pre-Tertiary rocks. This property was developed by a 30 m two compartment shaft and a 61 m adit. Production in the late 1920s is recorded as 13.6 tons containing an average of 720 g/t Ag, 21%

Pb and 2% Zn. A further 18.1 tons produced in 1938 contained 240-275 g/t Ag and 8% Pb (Kleinhampl and Ziony, 1984).

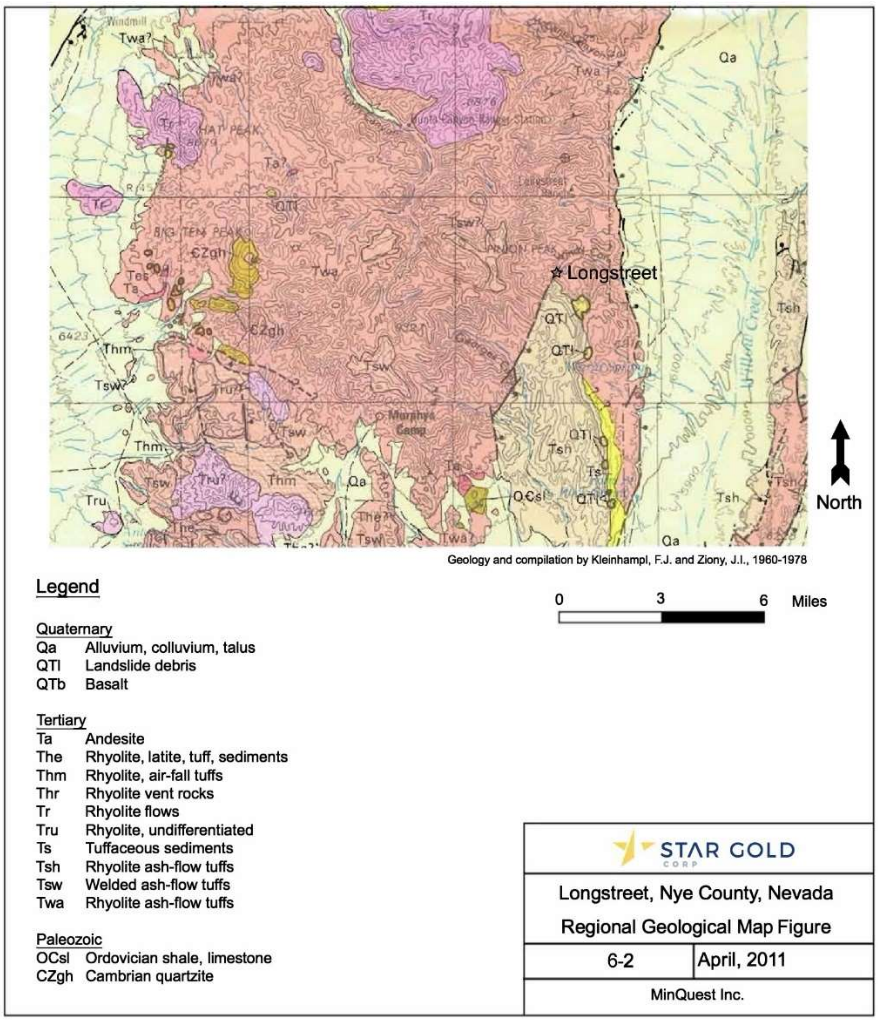
E Figure 6-1 Regional Geological Setting



6.2 Local Geology

Outcrops of Cambrian to Jurassic metasedimentary rocks and volcanic rocks occur in the general area of the Longstreet property. The Tertiary volcanic rocks have been deposited on the basement rocks, and include fine-to-medium-grained, felsic tuff and breccia. The contact zones between the extrusive rocks and metasedimentary rocks are favorable for gold and silver mineralization, as evidenced by a number of surface showings.

F Figure 6-2 Regional Geological Map



6.3 Property Geology

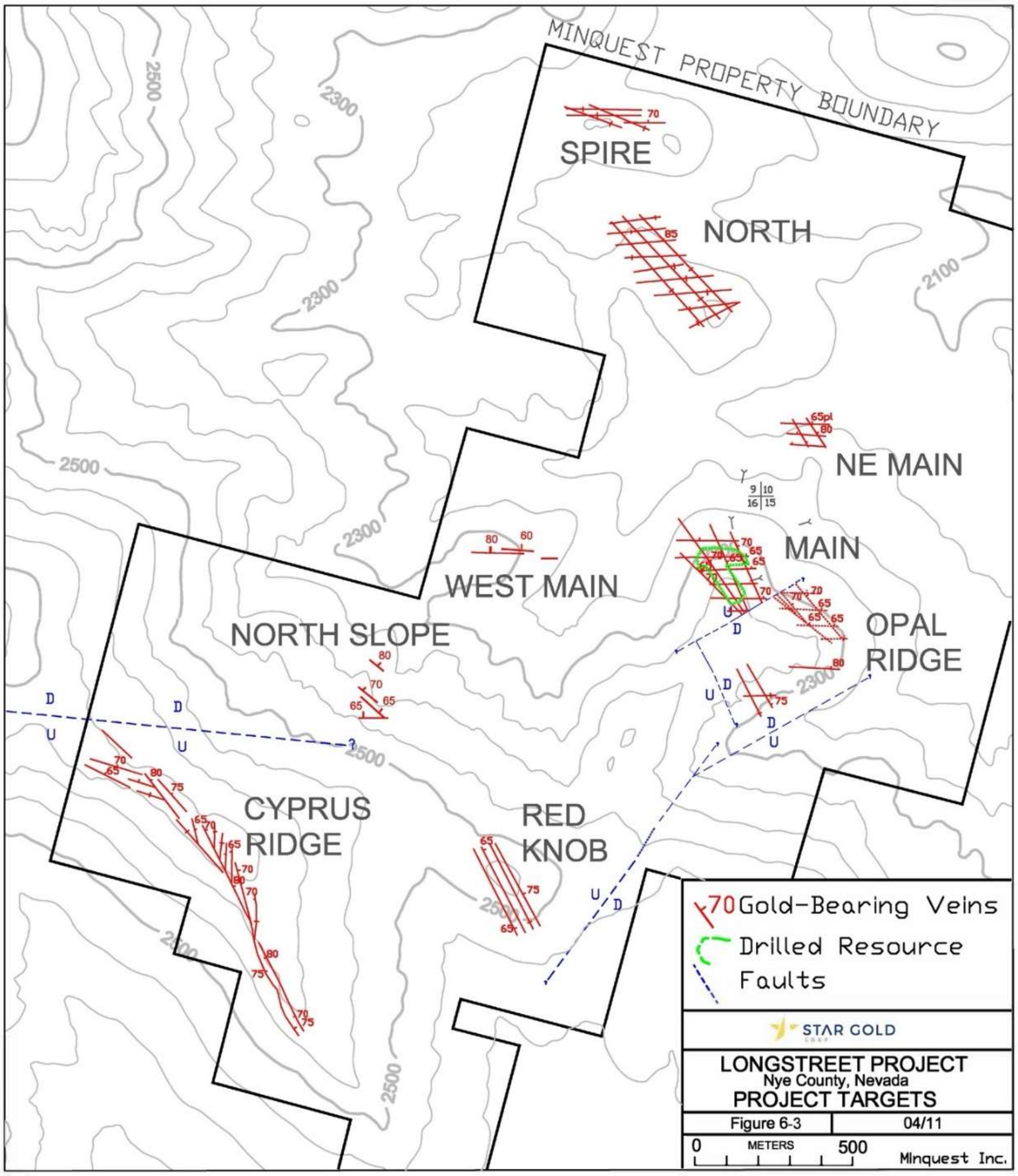
Geologic mapping by MinQuest since 2002 indicates that the majority of the Longstreet Project is underlain by moderately to poorly welded rhyolite ash-flow tuff ('Tat') containing conspicuous exotic lithic fragments and pumice (Figures 6-4 trhough 6-6). The ash-flow tuff unit is buff to gray, and contains <10% quartz phenocrysts, 15% feldspar phenocrysts, 5-15% pumice and 5-20% other exotic fragments in an aphanitic groundmass (Liedtke, 1984). Hydrothermal alteration is prevalent and consists of argillic (bleaching and clay mineral development), silicic (pervasive silica flooding, or extremely high veinlet density) and potassic (adularia in quartz veinlets). Limonite and geothite development is considered to be weathering phenomena. These felsic ash-flow tuffs of Oligocene age are similar in age and character to the 'tuffs of Round Mountain', which host the Round Mountain Mine.

The Tat tuff unit (Figures 6-4 through 6-6) displays horizontal bedding and may be in the order of 3,000 feet thick. The ash-flow tuff is intruded by rhyolite porphyry dykes ('Trp') exhibiting various orientations, and may represent feeder conduits to now-eroded rhyolitic lithologies higher in the stratigraphy.

A thin discontinuous unit of volcaniclastic and siliceous sediments ('Ts'), including sinter is deposited upon the ash-flow tuff unit. The unit is white, yellowish and light gray, bedded in part and probably represents a hiatus in volcanism. Siliceous alteration resulting in the development of sheeted quartz vein systems affects the Tat, Ts and Trp rock units.

Overlying the Tat tuff and the Ts sediments is a black to brown strongly welded ash-flow tuff ('Trt') that forms bluffs and caps ridges. This unit has a distinctive thin (about 10 feet) vitrophyre zone near its base. This unit is estimated to be 300 to 450 feet thick and possibly a correlative of the Saulsbury Wash Formation (21.6 +/- 0.6 Ma).

G Figure 6-3 Project Targets



6.4 Structural Setting

The structural setting of the Longstreet area is not well understood. Regional geological mapping indicates that there are three sets of mineralized veinlet and fracture systems within the Longstreet property, which include at least nine mineralized target areas. These fracture systems are:

- Northwest trending vein and fracture system: a structural feature commonly present at the Main Zone, Opal Ridge, Red Knob, North Slope, and Cyprus Ridge target areas in the central and southwestern parts of the explored area, and Northeast Main, North, and Spire target areas in the northern part of the explored area.
- East trending vein and fracture system: a structural feature commonly present at the Main Zone, Opal Ridge, Red Knob, North Slope, Northeast Main, North, West Main, and Cyprus Ridge target areas.
- West-northwest trending vein and fracture system: a structural feature present at the Spire target in the northern part and northern portion of the Cyprus Ridge target area in the southwestern part of the property.

An east-tending fault dipping 40-55° is associated with the highest-grade gold / silver mineralization known to date. The bulk of the gold / silver mineralization in the Longstreet Mine is contained in steeply dipping multiple vein sets parallel to or semi-parallel to the fault. The author is of the opinion that east-trending vein and structure systems targets such as Red Knob, Cyprus Ridge, Red Knob and Opal Ridge should be highest priority targets for future exploration and drilling.

Liedtke (1984) indicates that similar fault directions are known 4,600 feet south and 2,800 feet north of the Longstreet Mine, which may host similar high-grade gold / silver mineralization.

H Figure 6-4 Main, NE Main

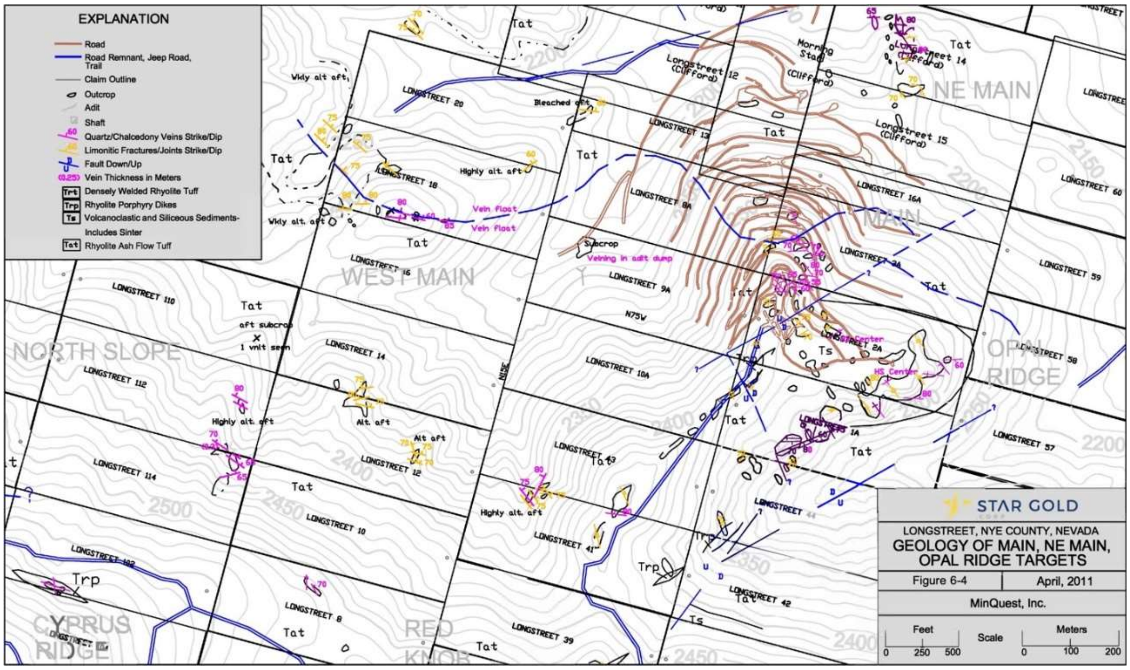
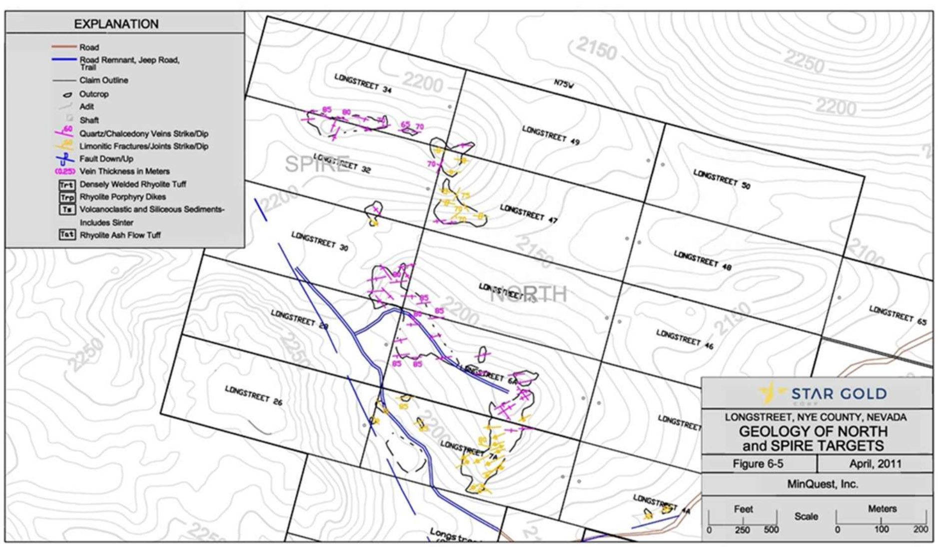


Figure 6-5 North Hill and Spire Targets



7.0 Mineralization and Alteration

7.1 Hydrothermal Alteration

Hydrothermal alteration is a metamorphic reaction in which excess water, silica, and carbon dioxide react with primary minerals of the host rock to form secondary minerals. New assemblages are formed in response to temperature, pressure, and composition of the altering fluids.

Hydrothermal alteration at Longstreet varies from early K-feldspar and sericitic alteration and silicification, both associated with and peripheral to the gold-silver mineralized zones. The latter comprise east trending and steeply north dipping quartz-adularia-limonite veinlets and fracture filled material, and northwest trending and steeply north dipping veins and stockwork zones with similar composition as the east trending veins (Agnerian, 2013).

7.2 Mineralization Style

Exploration work to date suggests that gold-silver mineralization at Longstreet occurs at the eastern margin of the Big Ten Peak collapsed caldera, near a north-northeast trending regional fault, which separates rhyolitic ash flow tuffs in the west from down faulted Quaternary unconsolidated sediments in the east. In the area of the property, the Oligocene volcanic rocks (approximately 27 MA) lie within an area cut by east, northeast and northwest trending faults. An east to northwest trending fault, the Adit Fault, separates the Main Zone mineralization from Opal Ridge.

Gold and silver mineralization within the Main Zone of the Longstreet property is associated with zones of strong hydrothermal alteration and quartz veins. From west to east, the thicknesses of the mineralized zones range from less than 3 m to approximately 85 m. Surficial alteration due to weathering is pervasive, and may extend more than 5 m below the surface. In general, the mineralized zones dip gently to moderately to the north or northeast. Based on available data, however, the individual zones may have some discontinuities regarding the relatively higher grade Au-Ag mineralization. Consequently, the author recommends additional drilling to better outline the mineralized zones. The different areas of mineralization on the property are discussed below.

7.3 Main Zone

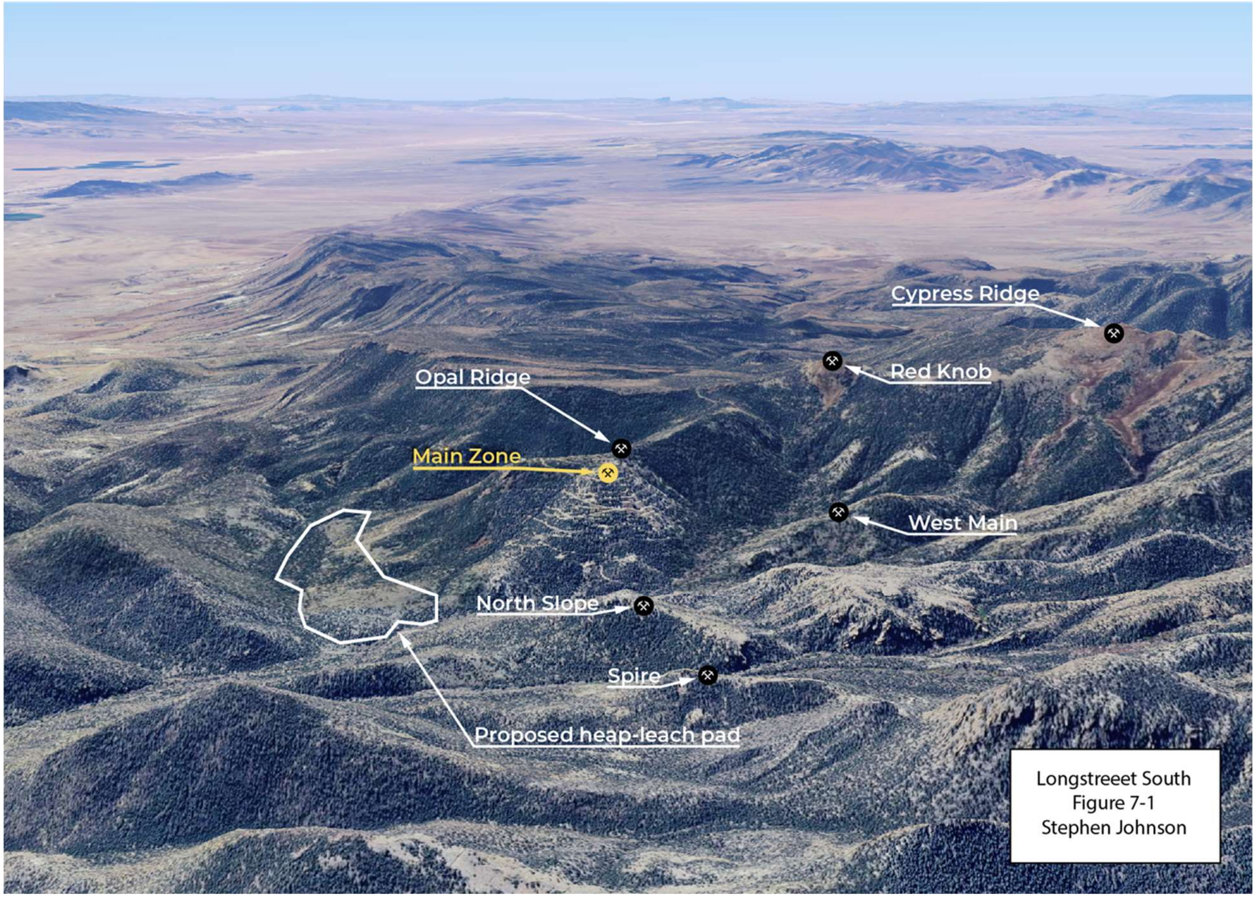
The Main Zone hosts the current Mineral Resources and has received the bulk of past exploration at Longstreet. It is approximately 325 m long and 200 m wide situated at elevations ranging from 2,460 m to 2,525 m on the southern slope of Windy Canyon, and in the east-central part of the property (Figure 7-1). Gold mineralization is hosted by fractured and stockwork zones within Oligocene ash flow tuffs.

G Table 7-1 Statistics of Mineralized Drill Intersections

Table 7-1 Statistics of Mineralized Intersections in Drill Holes, Main Zone		
Star Gold Corp. – Longstreet Au-Ag Project, Nevada		
	g/t Au	**g/t Ag**
Number	7,720	7,583
Maximum	62.80	999.0
Minimum	0.10	0.3
Average	0.63	24.0
Median	0.27	10.5
Standard Deviation	1.26	65.8

Note:
1. The Main Zone has been tested by 403 RC holes and 12 diamond drill holes.
2. The above statistics are based on intersections of significant mineralization of more than 0.10 g/t Au, since that was the detection limit of the laboratory(s) during historic drilling.
3. In general, mineralized intersections are 5 ft., but range from 2 ft. to 10 ft.

Figure 7-1 Oblique Areal View of Longstreet Target Zones



7.4 Opal Ridge

The Opal Ridge Zone is situated close to and east of the Main Zone, and forms part of the down-faulted block of the Main Zone. Vertical displacement along a northeast trending fault is interpreted to be in the order of 65 m and the horizontal displacement is in the order of 10 m. There are a number of outcrops of sinter deposits, which are interpreted to be remnants of a much larger area but reduced due to erosion. Lithogeochemical sampling results indicate values of eleven samples ranging from 0.03 g/t Au to 0.51 ppm Au (Noland, 2012).

7.5 Red Knob

The Red Knob Zone is approximately 300 m long and 150 m wide, and is situated approximately one kilometre south-southwest of the Main Zone. Gold mineralization occurs in northwest trending sheeted quartz veins with adularia. The veins range in thickness from 1.0 cm to one metre. Lithogeochemical sampling results of fifteen samples ranged from 0.05 g/t Au to 2.97 g/t Au, and drill results from two holes testing this target ranged from 0.99 g/t Au over 7.6 m to 5.6 g/t Au over 4.6 m (, Prenn, 1988, and Noland, 2012).

7.6 Cyprus Ridge

The Cyprus Hill Zone is approximately 800 m long and 100 m wide, situated in the southwestern corner area of the Longstreet property, approximately 1.5 km southwest of the Main Zone, in an area with abundant sinter material. Gold mineralization is associated with northwest trending and steeply southwest or northeast dipping veins and anastomosing north trending veins. In the northwestern part of the zone, east-southeast trending veins are common. In 1987, Cyprus tested this zone with a 7-hole, 3,000 ft. diamond drilling program, as noted in Section 6, History. Assay values of the 47 lithogeochemical samples collected by MinQuest in 2002 ranged from 0.03 g/t Au to 11.6 g/t Au, with an average value of approximately 0.5 g/t Au. Based on these results, MinQuest concluded that "the gold values are leakage anomalies from a deeper boiling zone" and considered the Cyprus Hill as a high priority target area (Noland, 2012).

7.7 North Slope

The North Slope Zone is situated approximately one kilometre west-southwest of the Main Zone in the western part of the Longstreet property. A number of northwest trending and steeply to moderately northeast dipping quartz veins (up to one metre thick) outline an area 200 m long and 100 m wide. This area has received little geological investigation and no drill testing in the past.

7.8 West Main

The West Main Zone is situated approximately 500 m west of the Main Zone in the western part of the Longstreet property. A number of east trending and steeply north dipping sheeted quartz veins outline an area 200 m long and 50 m wide. This area has received some geological investigation in the past, as evidenced by old workings, but no drill testing of targets.

7.9 Spire Zone

The Spire Zone is situated approximately 750 m north of the Main Zone in the northwestern part of the Longstreet property. Several east and northwest trending subvertical sheeted quartz veins outline an area 400 m long and 150 m wide. This area has received some geological investigation in the past with values ranging from 0.03 g/t Au to 18.1 g/t Au in seven lithogeochemical samples. Prospecting also indicates that the northwestern part of the target area is better exposed with higher grade mineralization (Noland, 2012).

7.10 North Zone

The North Zone is situated approximately 1.2 km north-northwest of the Main Zone in the northwestern corner area of the Longstreet property. A number of east and east-southeast trending subvertical quartz veins outline an area 250 m long and 100 m wide. This area has received some geological investigation in the past. Lithogeochemical sampling results indicate values of twelve samples ranging from 0.03 g/t Au to 18.4 ppm Au (Kern, 2012a). Drill results from three holes testing this target ranged from 0.78 g/t Au over 6.1 m to 4.0 g/t Au over 3.0 m (Prenn, 1988).

7.11 Northeast Main

The Northeast Main Zone is situated approximately 400 m northeast of the Main Zone in the northeastern part of the Longstreet property. The area is poorly exposed, but field observations indicate that it has similar characteristics as the Main Zone. Assay values from four lithogeochemical samples range from 0.04 g/t Au to 0.93 g/t Au (Noland, 2012).

8.0 Deposit Types

Gold and silver mineralization on the Longstreet property is typical of low-sulphidation epithermal Au-Ag systems associated with hydrothermal alteration assemblages within felsic volcanic rocks. These deposits are formed at relatively shallow depth, typically within a hundred metres of the surface, from hydrothermal fluids with temperatures of <150oC to 300oC. Berger (1992) describes the style of gold mineralization related to hot spring Au-Ag deposits as shown in Figure 8-1and reproduced below:

Description: *Fine-grained silica and quartz in silicified breccia with gold, pyrite, and Sb and As sulphides.*
Geological Environment:

- *Rock Type: Rhyolite.*
- *Texture: Porphyritic, brecciated.*
- *Age Range: Mainly Tertiary and Quaternary.*
- *Depositional Environment: Subaerial volcanic centres, rhyolite domes, and shallow parts of related geothermal systems.*
- *Tectonic Setting(s): Through-going fracture systems related to volcanism above subduction zones, rifted continental margins. Leaky transform faults.*
- *Associated Deposit Types: Epithermal quartz veins, hot spring Hg, placer gold.*

Deposit Description:

Mineralogy: *Native gold + pyrite + stibnite + realgar; or arsenopyrite ± sphalerite ± chalcopyrite± fluorite; or native gold + Ag-selenite or tellurides + pyrite.*

Texture/Structure: *Crustified banded veins, stockworks, breccias (cemented with silica or uncemented). Sulfides may be very fine grained and disseminated in silicified rock.*

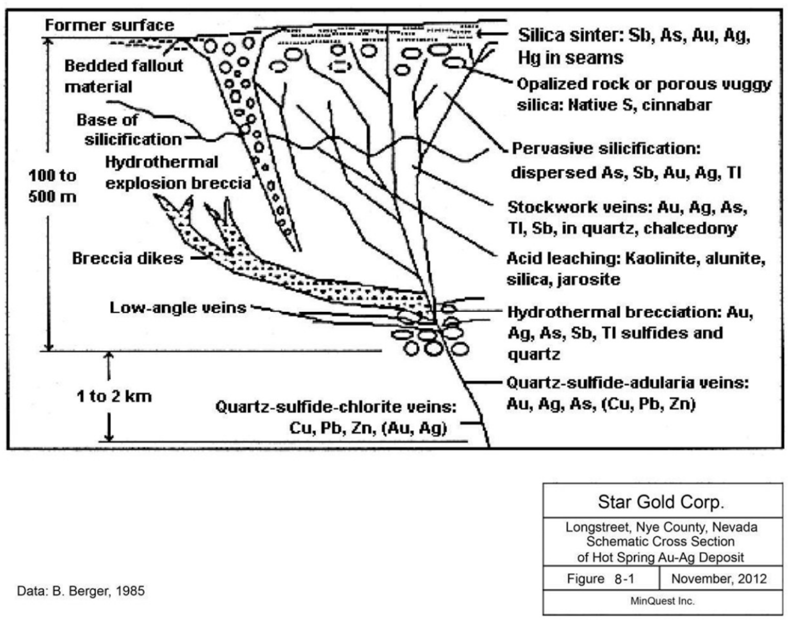
Alteration: *Top to bottom of system: chalcedonic sinter, massive silicification, stockworks and veins of quartz + adularia and breccia cemented with quartz, quartz + chlorite. Veins generally chalcedonic, some opal. Some deposits have alunite and pyrophyllite.*

Ore controls: *Through-going fracture system, brecciated cores of intrusive domes; cemented breccias important carrier of ore.*

Weathering: *Bleached country rock, yellow limonites with Jarosite and fine-grained alunite, hematite, goethite.*

Geochemical Signature: *Au + As + Sb + Hg + Tl higher in system, increasing Ag with depth, decreasing As + Sb + Tl + Hg with depth. Locally, NH4, W.*

I Figure 8-1 Hot-Springs Au-Ag Deposit



Mineralization at Longstreet is contained in altered rocks, which are localized by geological structures, and range in size from 5 m to more than 100 m wide and up to 800 metres long. Two dominant sets of mineralized structures are observed; one trending east and the second one trending north-northwest. A third (less common) structure trends east-southeast. Mineralization is comprised of altered zones, quartz stockworks, and hydrothermal breccia zones that contain disseminated pyrite. In addition, occasional quartz veins are associated with high grade gold mineralization, mainly as fracture coating material.

The alteration halos extending outward in the wallrock away from the mineralized zones are typically large in extent, and in places, are overprinted by surficial oxidation. This is evidenced by the numerous small limonitic pseudomorphs of pyrite near the old Golden Lion Mine adits and along the hills underlain by the Oligocene welded tuffs. Soil sampling results also indicate short dispersion of gold and silver from the mineralized structures at the footwall area of the Main Zone.

Gold and silver mineralization at Longstreet is similar to nearby gold mines and prospects. These are discussed below.

8.1 Round Mountain

The Round Mountain Mine is located approximately 30 mi northwest of the Longstreet property. It ranks among the world's largest precious metal epithermal systems. The mine hosts a large gold deposit, which is considered to be a classic low sulphidation epithermal gold-silver deposit spatially related to a collapsed caldera (White and Hedenquist, 1995). Gold mineralization was discovered at Round Mountain in 1906, and to date the mine has produced more than 10 million ounces of gold. At a cut-off grade of 0.005 oz/ton Au the in-pit Proven and Probable Mineral Reserves are reported to contain 82.5 million tons at an average grade of 0.018 oz/ton Au (0.59 g/t Au) (Pickens, 2012 and Kinross 2011 Annual Report).

Gold mineralization at Round Mountain occurs mainly in poorly to moderately welded ash flow tuffs, and less commonly in strongly welded tuffs or in basement metasedimentary rocks. The gold is hosted by two sets of veins; closely spaced northwest trending and steeply dipping veins and almost horizontal veins. The grade distribution is similar across all lithologic types. The "oxidized ore" is associated with the first set of veins and joints over broad areas. The veins and veinlets contain quartz, adularia, limonitic pseudomorphs of pyrite, manganese oxide, and native gold. The "flat" veins are similar to the steeply dipping veins but exhibit more brecciation in the wall rocks. Geochronological (40Ar/39Ar) dating of the adularia in the quartz veins indicates an age of 25.94±0.04 MA to 26.05±0.05 MA, i.e., essentially the same age as the Tertiary volcanism of the caldera (Henry, Castor, and Elson, 1996).

The nature and age of host rock, as well as the type and style of mineralization at Round Mountain are all similar to those found at Longstreet.

8.2 Manhattan Mine

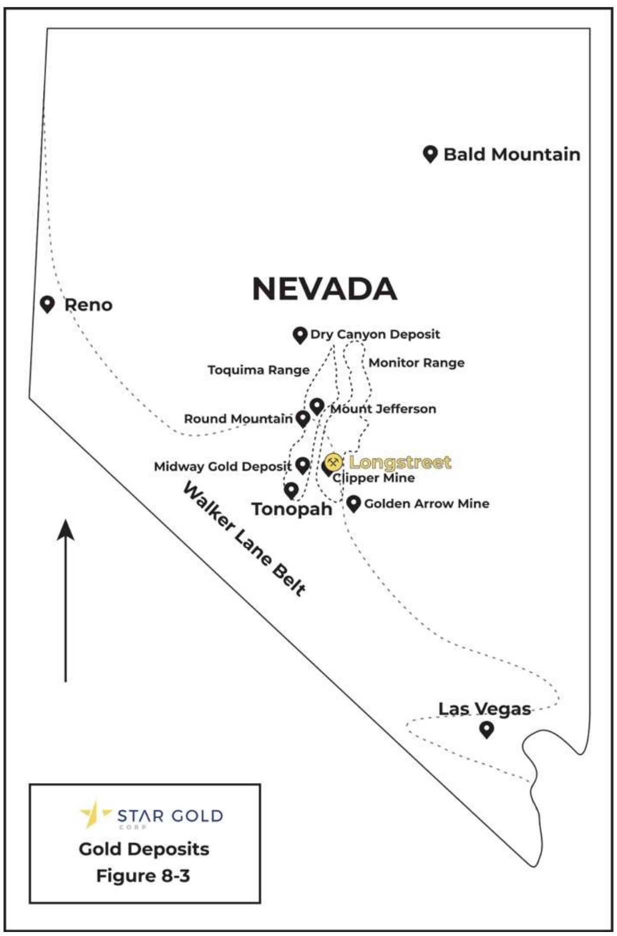
The Manhattan Mine is located approximately 20 mi west-northwest of the Longstreet property. The geologic environment and style of mineralization are similar to that at Round Mountain, i.e., epithermal gold and silver mineralization overlies Paleozoic sedimentary rocks. Gold mineralization was discovered at Manhattan in 1905, and by 1959 approximately 10,500 kg of gold and 4,400 kg of silver had been produced from placer and lode deposits (Noland, 2012).

Gold and silver mineralization occurs in a structural zone, 10 km long and 1 km wide, adjacent to the southern part of the Manhattan caldera.

8.3 Other Deposits

There are a number of gold deposits situated within the Monitor Range and Toquima Range, which hosts the Round Mountain deposit. These include the Clipper Mine (5 mi southwest of Longstreet), Dry Canyon and Mount Jefferson, approximately 2 mi and 4 mi northeast of Round Mountain, respectively, Midway gold deposit, and Golden Arrow Mine. The Round Mountain deposit, in particular, shares similarities to the Longstreet deposit including type and age of host rock as well as hot-spring-style mineralization.

J Figure 8-3 Gold Deposits Similar to Longstreet



8.3.1 Midway Gold Deposit

The Midway gold deposit in Nye County is located approximately 24 km northeast of Tonopah, in the Ralston Valley along the northeastern flank of the San Antonio Mountains. It is situated at the intersection of the Round Mountain/Goldfield gold trend and the Walker Lane Trend. Mineralization comprises a low-sulphidation epithermal gold system with near-vertical quartz-adularia-gold veins.

Host rocks are Ordovician black argillite of the Palmetto Formation, unconformably overlying Tertiary rhyolitic volcanic rocks. Mineralized veins occur in subparallel clusters, 10 ft. to 20 ft. apart, with an average width of 6 ft. Veins hosted in the argillite form well-defined veins and hydrothermal breccias. Where the veins pass upward into the volcanic rocks, they splay out to form numerous thinner subparallel veins in a braided stockwork zone (Midway Gold Corporation website (http://www.midwaygold.com, 2012).

8.3.2 Golden Arrow Deposit

The Golden Arrow deposit in Nye County is located approximately 60 km east of Tonopah, on the western flank of the Kawich Range, and situated along the northeastern margin of the Walker Lane Trend. The property is underlain by Oligocene-to Miocene-age andesitic to rhyolitic and volcaniclastic rocks. Gold and silver mineralization is typical of low-sulphidation epithermal mineral systems and hot-springs-type epithermal mineral systems (Ristorcelli and Christiansen, 2009).

Figure 8-2 Map of Gold Deposits in Region Which are Similar to Longstreet

9.0 Exploration

The exploration methodology applied in the past by early operators, and during recent exploration programs by Star Gold, has been to evaluate the mineralized zones by drilling, and determine favourable areas for epithermal Au-Ag mineralization of the host poorly to moderately welded tuffs, which are moderately altered and brecciated. To date, at least 107 lithogeochemical (rock chip) samples have been collected, and approximately 422 mostly RC drill holes have been completed by various operators on the property.

In December 2009, Star Gold entered into an option agreement with Messrs. Kern and Duerr of MinQuest to earn a 100% interest in the Longstreet property, and commenced a systematic exploration program, including 6,841 m (22,440 ft.) of RC drilling in 59 of RC holes, 395 m of diamond drilling in four holes, and lithogeochemical sampling, which was completed in 2011, 2012, and 2013 (Figure 9-1). All of the drilling by Star Gold was done on the Main Zone.

9.1 Lithogeochemical Sampling

Upon signing the option agreement with MinQuest, Star Gold commenced a program of sampling mineral showings at several target areas and structures on the Longstreet property. Star Gold contracted MinQuest to carry out this work. MinQuest crews sent the samples to ALS in Reno, Nevada, for Au and Ag assays. Results from this program indicate that, with few exceptions, the gold and silver values in surface samples show moderate to good correlation, with a ratio of approximately 1Au:10Ag, as discussed in Section 5, History.

9.1.1 Main Zone

MinQuest collected and analyzed three surface samples from the Main Zone in 1998, and the results are as follows.

H Table 9-1 Main Zone Geochemical Sampling

ID	EAST	NORTH	DESCRIPTION	Au (ppm)	Ag(ppm)
RK21	525341	4247444	most S. min. outcrop. Select of N35W/v chal. veinlets	1.37	32.6
RK1	525312	4247315	E. side hilltop, near RCH #325 0.6m chip across N40W/ 70NE chalc vnlts (2-3 cm thick) in ash flow tuff. Moderate limonite staining of host.	35.45	108.0
RK2	525331	4247298	20m SE of RK1, below RCH #338. 1m across N40E/ 60NE chalc vnlts (2-3 cm thick) in ash flow tuff.	0.38	3.5

9.1.2 Opal Ridge

The Opal Ridge Zone occurs in a detached fault block located along a ridge at a mean elevation of 7,675 feet. This zone is adjacent to and southeast of the Longstreet Main zone mineralization (Figure 6-4). Bounding faults trend northeast and geological observations indicate an apparent 200 foot vertical displacement and a northward displacement of less than 30 feet for this block. The bedrock consists of moderately welded ash-flow tuff and epiclastic sediments capped by an opalized sinter apron. Quartz-adularia sheeted vein systems and limonitic fractures occur over an area measuring approximately 650 feet by 650 feet. Both steeply dipping northeast and northwest-trending vein systems with limonitic fractures are present.

Two vertical RCHs (S-1 and S-2) completed in this area by Naneco in 1984 reported anomalous Au and Ag values over 400 feet (Liedtke, 1984).

The following table (9-2) lists 15 surface samples collected by MinQuest in 2002. The values reported are similar to the drill intersections. However the presence of opal (sinter) at surface implies that physiochemical conditions appropriate for the deposition of Au and Ag mineralization will be located at some depth beneath the sinter.

I Table 9-2 Opal Ridge Zone Surface Sampling

ID	EAST	NORTH	DESCRIPTION	Au (ppm)	Ag(ppm)
RK3	525289	4246988	Cliffs W section top. Select of 90/ 60-80 S opaline vns 2-3 cm in width in silic sediments.	0.05	0.3
RK4	525391	4247217	NW side grab of quartz/chalcedony as irreg seams in siliceous sediment	0.16	1.2
RK5	525415	4247219	NW side. grab of dark chalcedony veinlets in subcrop of siliceous sediment.	0.07	<0.3
RK 22	525430	4247220	NW side. 1m q.v. with calcite replacement texture and irreg banding presence of high temp. qtz. in sinter indicates this is hot springs center	0.07	0.2
RK23	525323	4246982	Cliffs W section top select of 90/ 60-80 S opaline vns 2-3 cm in silic sediments.	0.02	0.2
RK24	525368	4247009	Cliffs W section top select of N40W/v chal vnlts in ash flow tuff.	0.51	9.2
RK25	525357	4246958	Cliffs W section bottom 3 m N70E/ 80N chal vn with assoc. rhyolite porph. dike (?).	0.09	2.4

RK26	525388	4246997	Cliffs W section bottom select of 90/ 60N chal. vnlts up to .1 m thick.	0.20	2.2
RK27	525408	4247007	Cliffs W section bottom select of chal. vnlts N35W/ 75 NE vnlts. with assoc. rhyolite porph. w stkwk veining. near base of sediments.	0.38	7.8
RK28	525503	4247048	Cliffs E section bottom 1 m thick N35W/v chal. vn in sil. seds. Unmineralized fault above.	0.05	1.2
RK29	525647	4247146	Cliffs E section bottom 02 m thick N35W/v. brec chal vn in sil. seds. Discontinuous.	0.08	0.6
RK30	525662	4247153	Cliffs E section bottom 0.3m thick N70E/ 60S chal. vn in sil. seds. Calcite replacement texture.	0.12	1.8
RK31	525632	4247120	Cliffs E section bottom narrow 90/v. chal. vn in sil. seds.	0.15	1.2
RK32	525566	4247075	Cliffs E section bottom 1m thick N70W/ 80NE qtz./chal. vn in sil. seds. Multiphase texture.	0.27	4.6
RK33	525524	4247110	Cliffs E section 2/3 way up cliff 0.5m thick N60E/v multiphase qtz vein in sil. seds. Calcite replacement texture. Pos. late-stage hot springs center.	0.10	1.0

9.1.3 NE Main Zone

The NE Main Zone is located at a mean elevation of 7125 ft, approximately 1500 feet northeast of the Longstreet Mine (Figure 6-4). The mineralization is poorly exposed over an area measuring about 500 ft by about 230 ft along a 340° axial direction, and has not been drill tested. Sheeted vein systems and limonitic fractures trend both 90° and 315° with steep dips to the north and southwest, respectively. Preliminary rock chip sampling yielded a best value of 0.93 ppm Au and 20.6 ppm Ag.

J Table 9-3 NE Main Zone Surface Sampling

ID	EASTING	NORTHING	DESCRIPTION	Au (ppm)	Ag(ppm)
RK19	525570	4247807	N end of a sm ridge. Select 2.5 cm lim. stained chal. vein striking 90/v	0.93	20.6
RK20	525563	4247720	S 100m from 19. Select of lim stained fract (no quartz) trending 90/ 70N & N30W/ 70 SW.	0.11	4.0

9.1.4 North Zone

The North Zone is located at a mean elevation of 7350 ft about 3300 feet north-northwest of the Longstreet Mine (Figure 6-5) An east-northeast striking fault of unknown character separates this mineralization from the Longstreet Mine. Both northwest trending and east to northeast-trending vein systems and related limonitic fractures are present in outcrops. The gold mineralization is known over an area measuring 1800 ft by 1100 ft. MDA (1988) reports that 22 vertical RCs (3700 ft) were drilled at this location, with potentially economic mineralization found in four holes.

MinQuest collected 12 surface samples from the North target area in 2002. Gold values in the range of 0.031 to 18.1 ppm and Ag values in the range of 1.0 to 49.6 ppm are recorded at this location. The highest Au value is from an east-west trending sheeted quartz vein system near the northwestern end of the zone.

The gold values recorded in the RCs and the surface samples indicate that the area contains potentially economic mineralization.

K Table 9-4 North Zone Surface Sampling

ID	EAST	NORTH	DESCRIPTION	Au (ppm)	Ag(ppm)
RK91	525185	4248031	SE end. Select. Lim filled fract/joints. N40W/v &90/v.	0.051	1.0
RK92	525268	4248148	Select. 2 cm wh Qtz/chal vnlts. 90/v.	0.031	5.0
RK93	525249	4248198	Select. 2-3 cm wh Qtz/chal vnlts. N60E/v & N40W/ 80NE.	0.709	27.6

RK94	525292	4248156	Select. Lim stained fracts with qtz. fill, N60E/v.	0.123	5.6
RK95	525022	4248316	Select. 3 cm gray chal vein. N80E/ 85S	0.709	14.8
RK96	524982	4248452	W end. Select. 2-3 cm gray sheeted qtz/chal vnlts. N40W/v	0.596	49.6
RK97	525062	4248379	Select. 3-5 cm gray Qtz/chal vnlts. 90/v	18.144	32.2
RK99	524965	4248449	W end. grab. <1 cm gray sheeted chal vnlts & lim-rich joints. N80E/v	0.031	0.6
RK100	524961	4248481	W end. grab. same as 99	1.572	11.0
RK101	525017	4248514	Select. 1-4 cm gray chal vnlts. N40W/v & N80E/v.	0.483	20.8
RK102	525018	4248477	Select. 1-4 cm gray chal vnlts. Most N80E/ 85N.	0.421	12.0
RK103	525201	4248318	Select. 1-2 cm gray chal vnlts. Most N75E/v.	0.247	2.4

9.1.5 Spire Zone

MinQuest visited the Spire Zone area in 2002 and collected eight rock samples. The analytical results indicate gold values in the range of 0.031 to 0.45 ppm with Ag values in the range of 1.0 to 20.0 ppm over an area measuring approximately 1000 ft by 150 ft along an east-trending ridge. The oxidized mineralization is hosted in an east-northeast-trending, steeply north dipping to vertical sheeted quartz vein system. Northwest-trending veins are present, but not abundant.

L Table 9-5 Spire Zone Surface Sampling

ID	EAST	NORTH	DESCRIPTION	Au (ppm)	Ag(ppm)
RK104	524821	4248843	Select 2-5 cm discontinuous wh qtz/chal vnlts. N80E/v.	0.370	5.2
RK105	524826	4248845	Select 2-3 cm wh/pink qtz/chal vnlts. N80E/v.	0.185	16.0
RK106	524917	4248834	Select 5-10 cm gray/pink qtz/chal vnlts. N80E/v, large area of strong veining.	0.452	6.8
RK107	524942	4248816	Select 4-8 cm gray qtz/chal vnlts. N80E/v, large area of strong veining.	0.360	10.4
RK108	524869	4248802	Select Abund 2-8 cm lt gray qtz/chal vnlts. N20E/v.	0.298	17.6
RK109	525049	4248813	Select 1-3 cm gray qtz/chal vnlts. E-W/ 70N abund lim.	0.031	0.4
RK110	525109	4248739	Select 3 cm gray qtz/chal vnlt. N20E/ 70NW.	0.072	1.0
RK111	525138	4248612	Select 3 cm wh-gray qtz/chal vnlt. 90/v	0.175	20.0

9.1.6 Red Knob

The Red Knob Zone is located between 8250 ft and 8400 ft elevation about 4600 ft south-southwest of the Longstreet Mine (Figure 6-6). The mineralization occurs in a well developed sheeted quartz-adularia vein system that trends northwest and dips steeply both northeast and southwest. Liedtke (1984) reported a best grab sample assay of 4.1 ppm Au from this location. Quartz vein material > 3 feet in width was noted by MinQuest in 2002 in talus at this location. A best gold value of 2.96 ppm Au in a vein sample hosted in Tat is reported from the 16 samples collected in this target area by MinQuest, (Table 9-6).

M Table 9-6 Red Knob Zone Surface Sampling

ID	EAST	NORTH	DESCRIPTION	Au (ppm)	Ag(ppm)
RK17	524605	4246406	3' horz near SE end Red Knob;V. sil lim stained rhy lith ash flow tuff w 1 qtz/ad vnlt	2.60	27.4
RK18	524593	4246460	5' horz NW end Red Knob; like RK17, but more sheeted vnlts.	0.45	3.2
RK34	524967	4246828	Ridge SW of Main. Select. 1 small E-W chal. Vnlts. In bleached ash flow tuff. Weak limonite	0.010	<0.2
RK35	524899	4246505	Small knob E of Red Knob-SW end of outcrop only. Select. Vert. N35W dark chal. Vnlts. In aft.	0.051	<0.2
RK36	524680	4246291	SE end. Select. N35W 75 NE dip gray chal. Vnlts in aft and sil. Sed(?) Fine py in dark gray streaks	0.678	19.6
RK37	524671	4246310	SE end. Select. N35W 70 NW dip orange/brown chal. Vnlts in aft and sil. sed(?).	1.068	6.2
RK38	524639	4246348	Select. N35W 80 NE dip sheeted white/gray/tan chal. vnlts.in aft and sil. Seds(?).	0.360	4.8
RK39	524611	4246415	Select. N35W vert dip sheeted white chal. vnlts.in aft and sil. seds(?). E of RK17	0.092	1.4
RK40	524574	4246458	Select. N35W 75 SW dip sheeted white chal. vnlts.in aft.	0.185	7.0
RK41	524662	4246291	Select. Numerous vert N35W dark gray chal. Vnlts.in aft and sil seds. Fine py.	0.616	18.4
RK42	524640	4246302	Grab. N35W 70 NE dip 0.3m white chal. vn. in aft. and sil. seds.	0.092	5.0

RK43	524608	4246356	Select. N30W 80 SW dip sheeted dark gray sulfide bearing chal. vnlts.in sil. aft or sil. seds(?). Hvy. Limonite in vnlts.	0.904	14.6
RK44	524552	4246385	Select. N40W 60 NE dip sheeted gray/tan chal. vnlts.up to 0.2 m thick in sil. aft or sil. seds(?). Some calcite replacement textures	2.969	8.4
RK45	524541	4246409	Select. Numerous N25W 70 NE dip sheeted gray chal. vnlts. in sil. aft or sil. seds(?). Abundant here to RK 44.	0.144	3.2
RK46	524528	4246480	NW end. Select. Weak N35W 70 NE dip sheeted white chal. vnlts. in aft.	0.031	1.6
RK47	524320	4246707	Outcrop 250m NW of Red Knob. Select. Numerous small vert. N-S gray limonite stained drusy quartz vnlts. in aft.	0.031	1.0
RK98	524557	4246571	near LM L8. Select. Outcrop? Up to 10 cm width gray chal vnlts. N40W, 75 SW	0.144	6.2

9.1.7 Cyprus Ridge Zone

The Cyprus Ridge Zone is located between elevations of 8400 and 8850 ft. along the crest of a southwest sloping ridge approximately 1.5 miles southwest of the Longstreet Mine (Figure 6-6). The Tat unit hosts quartz veins up to 15 feet thick in the southeastern part of the northwest-trending sheeted vein system, which measure more than 1.7 miles long by 150 feet wide. The quartz vein system is described as a hanging wall vein dipping steeply northeast. Conjugate veins developed in the hanging wall are parallel structures with southwest dips. In the northwestern part of the vein system the hanging wall vein is supplanted by northwest-trending northeast dipping, and an east-trending north-dipping quartz vein systems. MinQuest mapped the intricate vein system in 2002 and collected 41 surface samples listed in the following table. A best gold value of 11.2 ppm is recorded from this target area.

N Table 9-7 Cyprus Ridge Zone Surface Sampling

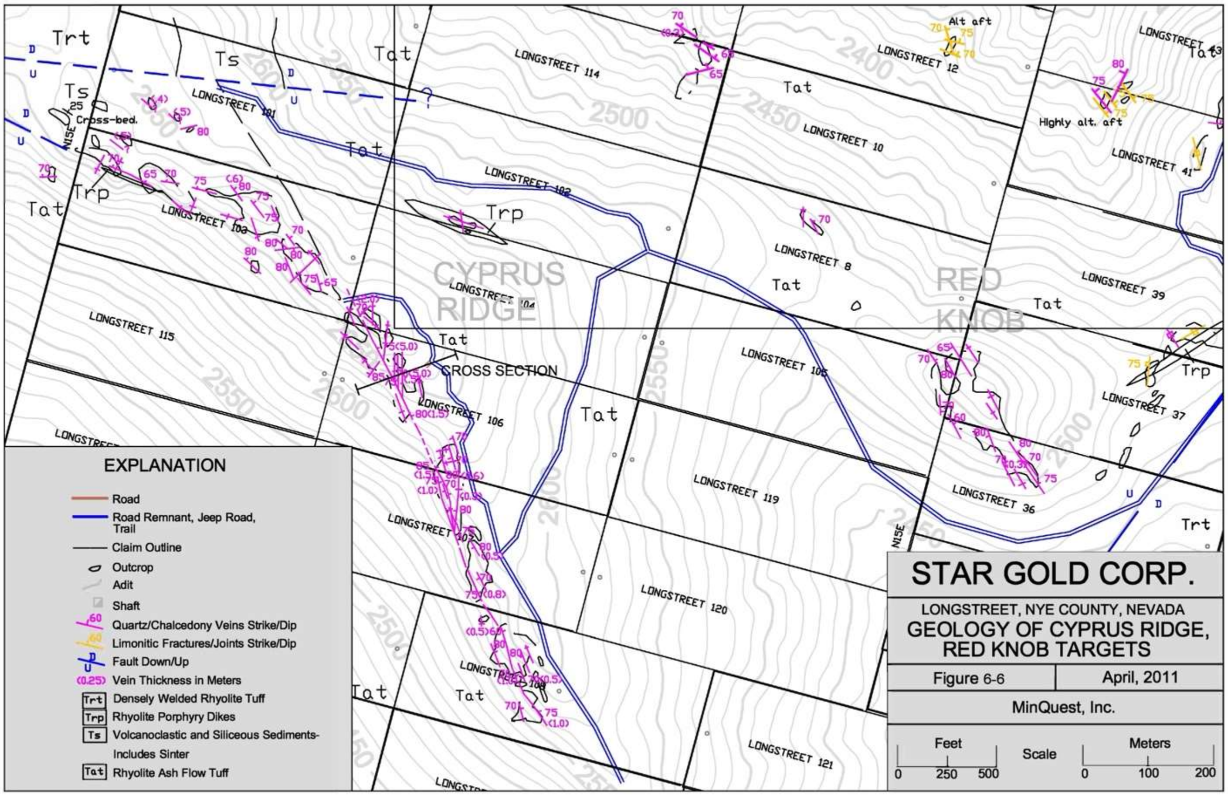
ID	EAST	NORTH	DESCRIPTION	Au (ppm)	Ag(ppm)
RK10	523216	4246795	1.83 m horz. NW end of zone; Sil. Rhy ash flow lith tuff	<0.07	<0.2
RK11	523411	4246736	2.74 m hor. hangingwall of zone 90-80SW dip sil. Tuff with qvs to 7.6 cm coarse ox py.	<0.07	0.2
RK12	523497	4246700	1.83 m horz Near top highest ridge numerous narrow sheeted vns in rhy tuff; mod lim	0.14	7.4
RK13	523613	4246636	1.83 m horz.partiy.sil. Rhy lith ash flow tuff; a few vert. Qtz/ad vnlts.	<0.07	0.8
RK14	523902	4246036	3.05 m horz zone vert sil lith tuff w/ vert sheeted vnlts every 0.3-1 m	0.21	2.4
RK15	523795	4246285	0.61 m horz across vert chal multistage vn white/pink quartz, gray/tan chal. vein 180/v numerous sheeted vns at 90	11.16	11.4
RK16	523724	4246400	2.44 m horz across N20W/ 80NE qtz/chal vein mass/ banded occa. calcite replace texture	0.45	8.6
RK48	523798	4246274	S of RK15 same vein. Channel sampl 90/ 80 W 0.3m white/pink qtz., gray/tan chal vn Multi-stage.	0.205	3.6
RK49	523788	4246236	Channel sampl 10 cm thick white/pink quartz/chal sheeted vns, N20W/v.	0.041	1.0
RK50	523780	4246269	Select sheeted white qtz vnlts 1-20 cm thick. Several orientations but N20W/ 75W dominant.	1.048	8.2
RK51	523758	4246309	Channel sampl 1.5 m thick white/pink quartz, gray/tan chal multi-stage sheeted vn, N10W/ 85E	0.452	4.8

RK52	523764	4246322	Channel sampl 0.3 m thick white/pink quartz, minor banded gray/tan chal. multi-stage sheeted vein N10W/v	0.575	4.6
RK53	523785	4246351	Grab 5 cm thick white/pink quartz, sheeted vein, N20W/ 70W	0.678	17.2
RK54	523788	4246303	N of RK15 same vein Channel sampl 180/ 80W 0.3m white/pink qt. vn Multi-stage.	0.051	0.8
RK55	523793	4246236	Grab N20W/ 75W 10 cm white qtz vn	0.380	4.6
RK56	523810	4246195	Semi-channel. 0.5 m thick white/purple/tan amethystine quartz multi-stage vn, N20W/ 80W large calcite replacement texture in part.	0.360	3.6
RK57	523835	4246115	Semi-channel. 0.8 m thick white/pink quartz, gray/tan chal. multi-stage sheeted vn, N20W/ 75 E	1.223	22.0
RK58	523859	4246047	Grab N20W/ 80E 10 cm banded white qtz vn	0.226	2.0
RK59	523863	4246073	Channel sampl 0.5 m thick white/pink quartz vn, N40W/ 60E	0.853	14.8
RK60	523899	4246028	Select. 10 cm thick white/pink sheeted qtz vns, N10W/ 80W several more in area.	0.298	5.4
RK61	523891	4246013	Channel sampl 0.5 m thick white/pink quartz vn, N20W/ 70W	0.072	2.4
RK62	523886	4245997	Channel sampl 0.3m thick gray/tan chal vn, N10W/ 70E	0.863	11.8
RK63	523911	4245948	Channel sampl 1.0 m thick white quartz, gray chal. multi-stage sheeted vein, N35W/ 75E Calcite replacement texture common.	0.267	3.0
RK64	523733	4246432	Grab 10 cm thick white/gray qtz. vn, N15W/ 70 E	2.548	14.2

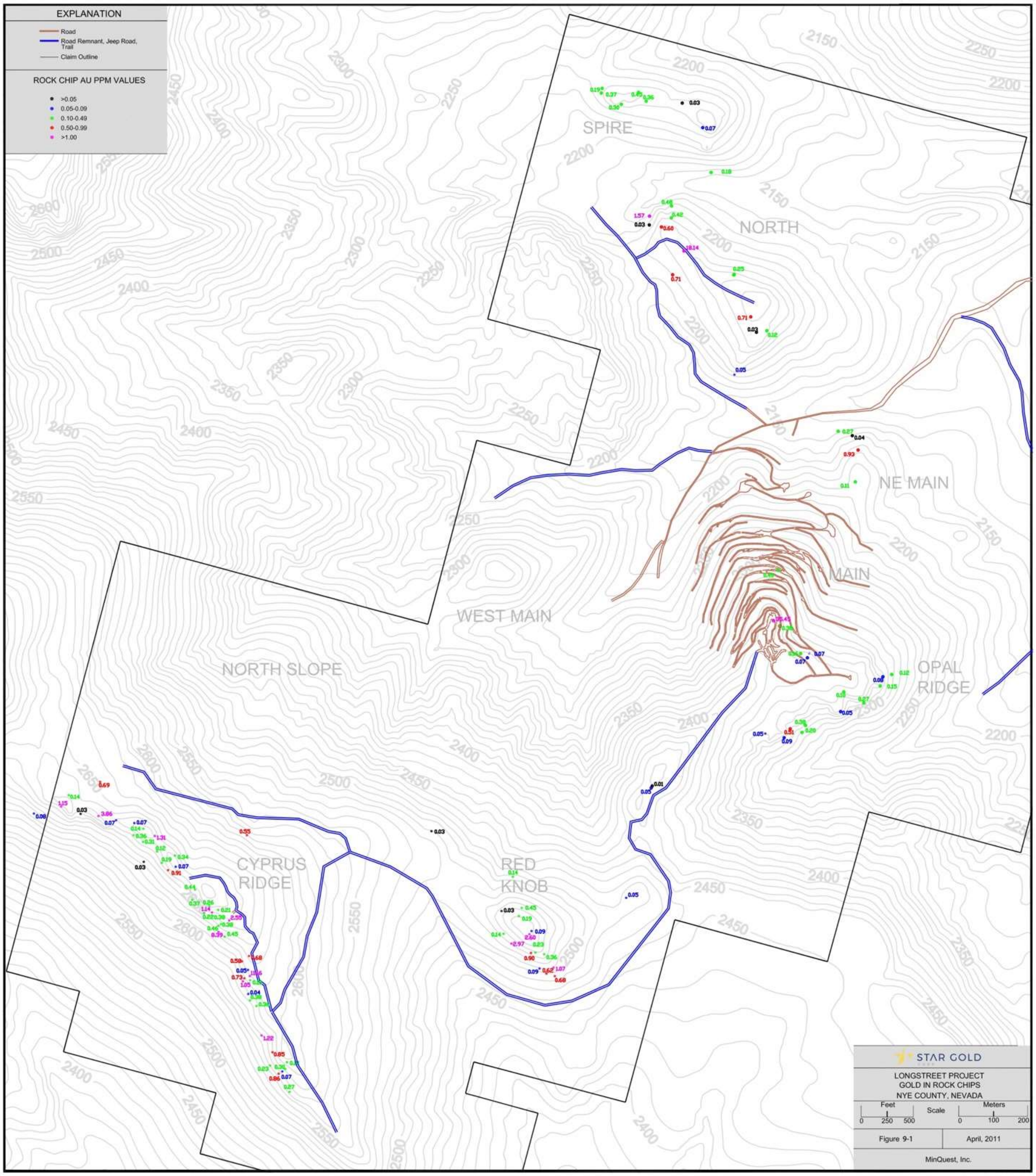
RK65	523703	4246410	Select 2-5 cm thick white/tan quartz, sheeted vns, N15W/v moderate lim, calcite replacement texture.	8.394	15.6
RK66	523703	4246432	Channel sampl footwall 2 m of 5 m thick white/gray quartz, tan chal. multi-stage vn, N35W/ 70E calcite replacement texture.	0.462	8.0
RK67	523703	4246432	Channel smpl HW 3 m of 5 m thick wh/gr qtz, tan chal. vn, N35W/ 70E large clasts in wall	0.565	9.4
RK68	523659	4246461	Cyprus. select. Several 3-5cm thick white/tan quartz, sheeted veins, N40W vert. Moderate limonite.	1.140	3.6
RK69	523636	4246506	Select several 3-5 cm thick white/gray quartz, gray chal. sheeted vns, N50W/v strong lim assoc. w/ vugs.	0.370	12.8
RK70	523632	4246544	Select several 2-10 cm thick white/gray quartz, gray chal. sheeted vns, N20W/ 60E moderate lim	0.442	4.0
RK71	523677	4246489	Chip sampl grab of 5 m thick white/gray quartz, tan chal. multi-stage vn, N35W/ 70E calcite replacement txt, silc. rock fragments.	0.257	5.2
RK72	525516	4247858	400 m NE of Main north of RK19 above road Select one 2 cm 90/ 65N gray/brown lim. stained chal vnlt in aft	0.267	4.8
RK73	525567	4247858	400m NE of Main north of RK19 above road Select several both 1-2 cm 90/ 60-80N & N35W/ N dip gray/brown lim stained chal vnlts in aft.	0.041	2.2
RK74	523710	4246472	Grab four 0.3-0.4m thick white-pink qtz/chal vns; 360-N10E/v to 75W dip	0.205	3.8
RK75	523579	4246589	Select 2-10 cm lt gray-tan chal sheeted vnlts. N40W/ 60-85E	0.914	15.2

RK76	523553	4246609	Select 2-5 cm lt gray-tan chal sheeted vnlts. N30W/ 80W.	0.185	3.0
RK77	523493	4246608	Select 2-4 cm lt gray-tan chal sheeted vnlts. N50W/ 85E	0.031	0.8
RK78	523538	4246641	0.5 m channel sampl lt gray-tan chal vin N80E/ 80S	0.123	4.2
RK79	523489	4246678	Grab.0.2 m lt gray-tan-pink chal vein. N30W/v	0.308	5.8
RK80	523471	4246692	Select 10 cm lt gray chal and red/green opal vein. 90/v	0.360	9.4
RK81	523460	4246723	0.6m Semi-channel lt gray-pink chal vn N40W/ 80NE	0.072	0.8
RK82	523531	4246690	Select 4-10 cm gray-tan chal sheeted vnlts N30W/ 75W	1.305	26.4
RK83	523582	4246630	Select 2-5 cm pink chal sheeted vnlts. N40W & N30E, vert.	0.339	4.6
RK84	523365	4246841	0.5m Semi-channel subcrop. White qtz and gray chal vn. No attitude Is in Ts unit NE end of zone.	0.688	7.2
RK85	523319	4246757	Grab 10 cm wh-gray chal vein. N60W/ 65NE	0.031	0.6
RK86	523354	4246744	Grab 10 cm gray chal vnlts 90/ 70N	3.863	47.0
RK87	523270	4246805	Grab subcrop 0.2-0.5m wh qtz/chal vns 90/ 70N; attitude unknown near Cyprus ddh.	0.144	3.6
RK88	523251	4246771	Select 5 cm wh-gray qtz/chal vnlts N20E/v	1.151	4.4
RK89	523178	4246747	Grab 5 cm lt gray chal/opal vein. 90/ 75N.	0.082	0.8
RK90	523779	4246693	N of Main ridge select. 2-5 cm gray/wh chal vnlts in rhy porph	0.545	2.8

Figure 6-6 Cyprus Ridge



K Figure 9-1 Lithogeochemical Sampling



9.2 RC Drilling

During the 2011 drilling campaign, Star Gold completed approximately 4,728 m of drilling in 39 RC drill holes. This work was carried out to further test the central part of the Main Zone target area. Results are discussed in Item 10, Drilling.

9.3 Diamond Drilling

During 1987, Cyprus completed seven diamond drill holes on the Cyprus Ridge target area. During the 2012 drilling campaign, Star Gold completed approximately 395 m of drilling in four diamond drill holes. This work was carried out to provide additional lithologic information regarding the RC holes of the Main Zone target area. Results are discussed in Section 10, Drilling.

9.4 Specific Gravity Determinations

In 2011, MinQuest carried out specific gravity determinations on eight surface samples from the Longstreet property for Star Gold, using the Archimedes' Principle, i.e.:
Specific gravity of rock=weight of rock/volume of rock (amount of water in graduated cylinder)
The statistics of the specific gravity determinations are as follows:

- Maximum: 2.49 g/cm3.
- Minimum: 2.16 g/cm3.
- Average: 2.29 g/cm3.

The author is of the opinion that while these values fall within expected specific gravity ranges for rock types at Longstreet, they do not likely represent mineralized material at depth.

In 2012, MinQuest carried out specific gravity determinations on eight drill core samples from the four diamond drill holes completed on the Longstreet property for Star Gold, again using the Archimedes' Principle, as summarized below and listed in Table 9-8.

- Maximum: 2.51 g/cm^3.
- Minimum: 2.19 g/cm^3.
- Average: 2.37 g/cm^3.

O Table 9-8 Statistics of Specific Gravity

Table 9-8 Statistics of Specific Gravity Determinations, Main Zone Drilling 2012				
Star Gold Corp. – Longstreet Au-Ag Project, Nevada				
DDH No.	**From (ft.)**	**To (ft.)**	**Interval (ft.)**	**Specific Gravity**
LS 1216C	85.0	89.0	4.0	2.48
LS 1216C	213.2	213.6	0.4	2.51
LS 1217C	65.3	65.8	0.5	2.44
LS 1217C	175.0	175.3	0.3	2.48
LS 1222C	74.2	76.0	1.8	2.22
LS 1222C	191.0	191.5	0.5	2.32
LS 1224C	109.0	109.3	0.3	2.19
LS 1224C	200.8	201.0	0.2	2.34

Source: Kern, 2012a.

The author recommends continued and systematic bulk density measurements in association with all future drilling campaigns.

10.0 Drilling

More than 403 RC holes (approximately 81,000 ft. or 24,700 m) and 4,295 ft. (1,310 m) of diamond drilling in 19 holes have been completed by Star Gold and previous operators in the general area of the Longstreet property during the since 1980. Most of the drilling was done on the Main Zone and includes 16 RC holes completed by Star Gold in 2011, 23 RC drill holes, and four diamond drill holes completed by Star Gold in 2012. Three of the 2012 RC holes tested the North Zone, and one RC hole tested the Opal Ridge Zone. For the 2011, 2012, and 2013 campaigns, the drilling contractor was O'Keefe Drilling Company, Inc. (O'Keefe) of Butte, Montana. During the historic and recent RC drilling campaigns, drill chips were retrieved and sent for assays. Figure 14-1 shows the drill hole collar locations.

Of the 19 diamond drill holes and 423 RC holes completed on the six target areas, the majority (402) of the holes intersected significant mineralization of more than 0.2 g/t Au and 1.0 g/t Ag over intervals ranging from more than 3 m to approximately 85 m, as shown in Figure 14-1 and Appendix 2.

10.1 RC Drilling

To date, approximately 364 RC holes by previous operators and 39 RC holes by Star Gold have been completed on the Longstreet property during the past 32 years. The drilling contractor, methodology, or procedures of sampling in previous campaigns are not available at this time.

During the 2011, 2012, and 2013 drilling programs, the RC drilling contractor was O'Keefe. Star Gold used similar truck-mounted mud rotary equipment (with hole diameters ranging from 4 ¾ in. to 5 ¾ in.) using local Reno, Nevada based drilling contractors. The procedures used during the RCD programs are provided below,and are summarized, as follows:

- The collar locations of all drill holes were surveyed and marked in the field. A Geographic Positioning System (GPS) instrument was used to mark the collar locations of drill holes. This survey was carried out by MinQuest.

- Lithologic logging of drill core and geotechnical observations were provided by Mr. David Eastwood, Star Gold contract geologist, on loan from MinQuest. Logging is done by depicting all down-hole data and assay values. All information is recorded on previously prepared logs using LOGPLOT software developed by RockWare, Inc. (RockWare) of Denver, Colorado. This includes marking:

- Lithologic contacts.
- Descriptive geology.
- Intensity of various alteration types.

The author is of the opinion that logging procedures for RC holes used by Star Gold are in keeping with industry standards. Results of recent drilling are provided in Appendix 2.

10.2 Diamond Drilling

To date, nineteen diamond drill holes have been completed on the Longstreet property; eight holes by Keradamex/E&B, seven holes by Cyprus on the Cyprus Ridge target area, and four holes by Star Gold on the Main Zone (Prenn, 1988, Noland 2012, and Kern, 2012a). The drilling contractor or the size of drill core recovered for Keradamex/E&B in 1980, and Cyprus during the 2003-2005 drilling program, are not available.

During the 2012 exploration program, diamond drilling was done by O'Keefe. The drilling crew worked two 12-hour shifts and recovered NQ core throughout the hole. Drill hole collar co-ordinates and collar elevations were determined using GPS instrument. For down-hole surveying the holes, Star Gold used the International Directional Services (IDS) system from Elko, Nevada, which is similar to the digital Maxibore instrument. Measurements of the hole inclination and azimuth were taken continuously down the hole, thus a complete record of down-hole measurements is available at intervals of five feet.

The procedures used during the diamond drilling programs are summarized as follows:

- The collar locations of all drill holes were surveyed and marked in the field using GPS.
- Lithologic logging of drill core and geotechnical observations was provided by Mr. Richard Kern, President of MinQuest. Logging was done by Mr. David Eastwood, contract geologist on loan from MinQuest. Logging was done by depicting all down-hole data including assay values. Similar to RC holes, drill holes are logged using LOGPLOT software. All information was recorded on handwritten logs. This includes marking:
    - o Lithologic contacts.
    - o Descriptive geology.
    - o Intensity of various alteration types.
    - o Structural features, such as foliation, fracture and brecciated zones
    - o Core angles.
    - o Core diameter.
    - o Downhole inclination.
    - o Percent core recovery record.
    - o Recording geotechnical data, such as RQD measurements.
    - o Down-hole survey using the IDS system survey tool.

The author examined drill products and reviewed drill logs during and subsequent to his site visits to the property. The author is of the opinion that lithologic logging procedures are in keeping with industry standards. The author recommends that density measurements be continued on future drilling, and digital core photographs be recorded regularly.

10.3 Historical Drilling Results

10.3.1 North Zone Drill Highlights

The North Zone is located at a mean elevation of 7350 ft about 3300 feet north-northwest of the Longstreet Mine (Figure 6-5) An east-northeast striking fault of unknown character separates this mineralization from the Longstreet Mine. Both northwest trending and east to northeast-trending vein systems and related limonitic fractures are present in outcrops. The gold mineralization is known over an area measuring 1800 ft by 1100 ft. MDA (1988) reports that 22 vertical RCs (3700 ft) were drilled at this location, with potentially economic mineralization found in four holes. Complete drill logs for these holes are not available for perusal. Since these holes were all vertical, and the veins are generally dipping at varying angles from moderate to steep, the intervals reported in Table 10-1 likely represent thicknesses greater than 'true widths' of veins.

P Table 10-1 North Zone Drill Intercepts and Analytical Results

RC #	Interval (m)	Au Assay (g/t)	Ag Assay (g/t)
383	15.24-24.38	1.09	9.59
385	44.19-54.86	1.54	10.97
393	1.52-4.57	4.01	25.71
393	4.57-10.67	0.79	22.63

10.3.2 Spire Zone Historical Drilling Summary

The Spire Zone is located at a mean elevation of 7425 ft approximately 4600 ft north-northwest of the Longstreet Mine (Figure 6-5). MDA (1988) reports that 24 vertical RCs (3400 feet) were drilled at this target area with the most significant results presented in the following table. Complete drill logs are not available for examination. Since these holes were all vertical, and the veins are generally dipping at varying angles from moderate to steep, the intervals reported in Table 10-2 likely represent thicknesses greater than 'true widths' of veins.

Q Table 10-2 Spire Zone Drill Intercepts and Analytical Results

RC #	Interval (m)	Au Assay (g/t)	Ag Assay (g/t)
320	51.82-60.96	0.99	62.06
402	45.72-68.58	1.30	44.57
403	27.43-39.62	2.09	31.88

10.3.3 Red Knob Historical Drilling Summary

MDA (1988) states that 66 vertical and inclined RCs totaling 9500 feet were drilled at Red Knob Zone. Potentially economic mineralization was located in two holes. Complete drill logs for these holes are not available for examination. Analytical results (Table 10-3) probably reflect the negative sampling bias associated with the sampling of vertical, or near vertical structures with vertical drill holes. Additionally, the vertical drill holes do not allow any representation of 'true width' of intersected veins. Consequently, the intervals reported in Table 10-3 likely represent thicknesses greater than true vein widths.

R Table 10-3 Red Knob Zone Drill Intercepts and Analytical Results

RC #	Interval (m)	Au Assay (g/t)
1002	13.76-21.34	0.99
1043	21.34-25.91	5.55

10.3.4 Cyprus Ridge Historical Drilling Summary

Cyprus Minerals Company completed a 3,000 foot DDH drill program in 1987 and the following table is a summary of the results obtained. Complete drill records are not available for examination.

S Table 10-4 Cyprus Ridge Zone Drill Intercepts and Analytical Results

DDH #	Interval (m)	Gold (g/t)	Azim°	Dip	Length (m)
LS-1	79.3-82.3	0.38	216	75	86.9
LS-2	94.5-97.5	0.45	215	83	105.2
LS-3	73.2-79.3	0.34	225	75	103.6
DDH #	Interval (m)	Gold (g/t)	Azim°	Dip	Length (m)
LS-4	30.5-36.6	0.41	255	70	88.4
And	70.1-79.3	0.34			
LS-5	91.4-94.5	1.19	185	70	109.7
Or	91.4-97.5	0.72			
Or	91.4-109.7	0.34			
LS-6	nil	nil	225	70	85.3
LS-7	nil	nil	0	90	83.8
LS-8	nil	nil	0	90	45.7
LS-9	67.1-70.1	0.31	0	90	100.6
LS-10	nil	nil	0	90	24.4
LS-11	nil	nil	0	90	30.5
LS-12	nil	nil	0	70	56.4

11.0 Sample Preparation, Analysis and Security

11.1 Work Prior to Star gold

Information on sampling procedures during geochemical sampling and RC drilling programs carried out by Keradamex/E & B, Minerva, Naneco, and REM/Harvest Gold in the 1980s and 1990s, is not available at this time. Sampling was done at 2 ft., 5 ft., and 10 ft. intervals. The bulk of the sampling, however, was done at 5 ft. intervals, and sampling was done throughout the entire hole. In general, samples from earlier drilling were assayed mainly for gold and silver. The exact methods of gold and silver determinations, however, are not available.

It is the author's opinion that data from these historical programs were collected using methods and safeguards common and prevalent at the time, and that no bias was likely introduced by the operators. The use of these drill holes in a resource estimation must be made on a 'case by case' basis and the determination of validity conducted by the QP based on availability of data, proximity to 'twin' drilling or validation by other geologic considerations.

11.2 Work Conducted by MinQuest and Star Gold

11.2.1 RC Drilling

During the most recent work by Star Gold (2010-2013) sampling of drill chips was done by MinQuest technical personnel contracted by Star Gold. Sampling procedures during the drilling programs included splitting the drill chips using a two-way wet sample splitter, at 5 ft. sample intervals, under the supervision of the Project Geologist. Material from one half of the sample (A sample) was put in securely sealed bags and sent to the ALS sample preparation laboratory in Reno, Nevada. Samples were numbered on the sample bags, according to the drill hole number and footage of the hole. The other half of the sample (B sample) was kept at the site for future reference. The chain of custody of logging and sampling was the responsibility of the Project Geologist. Details of sampling procedures for both RC and Diamond Drilling are provided below.

The author notes that sample numbers are assigned in accordance with the footage of the drill hole, e.g., for sample from 20 ft. to 25 ft. in Hole LS01205, the sample number is LS-1205 20-25. While this sample numbering system is widely used in exploration, the author suggests that a higher level of security is provided by utilizing sequential sample numbers which do not identify drill hole numbers or footage.

11.2.2 Reverse Circulation Drilling, Logging and Sampling Procedures

Sampling of RC chips is undertaken at the drill site under the direct supervision of a Star Gold contract geologist.

- At each drill site, an area for sample splitting and chip logging is established.

- The cyclone is cleaned prior to commencement of drilling by blowing compressed air through it. If a wet sample has been collected, the top of the cyclone is removed and the sample "cake" is removed from the walls of the cyclone.
- Reverse circulation samples are collected over five-foot intervals and are numbered in 10 kg plastic pails, which is held underneath the cyclone by the sampler. Little to no dust is allowed to escape.
- At the end of each five-foot run (marked on the drill string) and without stopping the drilling, the sample pails are quickly removed (taking a second or two) and replaced with a new pail.
- At the end of a twenty-foot run, the five-foot sample pail is removed, an extra 20-ft. length of drill rod is fitted and drilling re-commences – first with the blowing out of the hole. As soon as the hammer starts to "chatter", a new sample pail is placed beneath the cyclone and the sample collection procedure continues.
- Each five-foot sample is weighed on a spring balance with the weight recorded in a book as well as on the RC log sheet in order to determine approximate recoveries.
- Each five-foot sample is split by a 1:2 riffle splitter. Half of the sample (A Sample) is bagged in rice bags, numbered according to hole number and sample depth, and used for assays. The other half (B Sample or reject) is bagged, also numbered in sequential order according to hole number and sample depth, and packed into rice sacks for storage at Star Gold/MinQuest sample storage facility in Reno.

A 200 g sample of each five-foot run is collected, sieved, washed and laid out to dry in wooden chip trays. The chips are logged by the geologist and recorded in the RC log sheet. The samples once dried, are placed in plastic chip trays and numbered accordingly. At the end of the shift these boxes are sent to Tonopah, and eventually to the Reno storage facility for indexing and storage.

- Samples are arranged in batches of 20 samples and include one duplicate, one standard, and one blank sample.
- Sample numbers are assigned in accordance with the footage of the drill hole, eg., for sample from 20 ft. to 25 ft. in Hole LS01205, the sample number is LS-1205 20-25. Agnerian is of the opinion that the sample numbers unique (commonly those with the book of sample tags either purchased independently or provided by the laboratory) so that the hole number is not disclosed.
-

Samples that return values higher than 1 g/t Au are asayed again by the fire assay method with gravimetric finish. The higher grade samples are retained in storage at the Reno core shed.

11.2.3 Diamond Drilling , Logging and Sampling Procedures

During the diamond drilling program the Project Geologist carried out daily visits to the drill site. Geotechnical logging was undertaken on site during drilling operations and procedures of drill hole logging and sampling were as follows:

- Each 5-foot core run is separated from the following run by a piece of hard plastic "block" on which is written the depth of the hole.
- Once each run of core is packed and marked in the core box, geotechnical logging is carried out in which core recovery measurements are recorded. Furthermore, a brief lithologic description and joint distribution of fractures, based on the core axis, are also noted.
- Hole depths are periodically checked.
- On completion of diamond drill holes, down-the-hole survey is carried out using the survey tool by International Directional Services, which is similar to the digital Maxibore instrument.
- At the change of drilling shift, the core is carefully packed and transported to Tonopah for the logging of additional data

Diamond Logging procedures

- Geotechnical Log: usually completed at the drill site and finalized at the core shed.
- Descriptive Log – geological description of the core together with structural data, alteration, mineralization, sample numbers and assays are recorded.
- The depth of hole is written on the core box and on each block.

Diamond Sampling procedures

- Once all logging procedures are completed on the diamond drill core, the entire hole is sampled at no greater than 5-foot intervals. Sample breaks of less than 5 feet are made at geological boundaries at the logging geologist's discretion.
- The core is split vertically down the core axis.
- The remaining half core section is labelled to indicate the sample interval.
- Duplicate samples consists of quarter core.
- As with the RC samples, all DDH samples are arranged into batches of 20 samples and include one duplicate, one standard, and one blank. Barren volcanic is rock cut into pieces, and used as blank material.

During the 2011, 2012 and 2013 exploration programs by Star Gold, samples were sent to the ALS laboratory in Reno, Nevada, where samples were crushed and ground. Sample pulps were then assayed for gold and silver using the one assay-ton (30 g sample) fire assay method and the atomic absorption (AA) finish. Samples that contained more than 10 g/t Au were re-assayed by the fire assay method and gravimetric finish. In addition, at the discretion of the Project Geologist, samples adjacent to intervals with significant gold, were re-assayed.

ALS is an ISO 9001 recognised laboratory and the procedures used at ALS Chemex laboratories are similar to those used at many commercial laboratories in Canada. In particular, they include:

- Drying the split sample and preparing by particle size reduction to produce a homogeneous sub-sample, which is representative of the original sample.
- Crushing the split sample to 10 mesh and grinding it to 200 mesh, 85% passing <75μ.
- Cleaning the pulverizer after each sample using cleaner sand to avoid cross contamination of samples.
- Determinations of the gold and silver contents are carried out using the Aqua Regia Digestion Method, including sulphuric acid, nitric acid, and hydrochloric acid.
- Sample size is generally <250 g.

The author believes that the sample preparation and assay procedures at ALS are in keeping with industry standards.

12.0 Data Verification

All drilling data utilized in the resource estimation was verified by the author, including available historic QA/QC measures. Assay certificates for current and historic drilling were inspected by the author, compared to assay tables utilized in resource calculations, and thereby confirmed. The author also has inspected the assay certificates from surface and underground sampling conducted at Longstreet by MinQuest and can verify the results as presented in this report.

The 'preliminary feasibility study' completed by MDA (1988) provides details of assay verification as a prelude to calculating the historical 'measured resource'. The author notes here that neither the MDA 'preliminary feasibility study' completed in 1988 nor the reported 'measured resource' from that study meet current NI 43-101 or SK 1300 standards or definitions of 'resource'. Reference is given here for perspective only.

Further attempts at 'verification' of historical drilling were made by conducting 'twin drilling' programs whereby historical drill holes are duplicated as closely as possible with new drilling and the assay results compared. Two separate 'twin drilling' programs have been conducted at Longstreet as a way of verifying validity of historical drilling.

12.1 Naneco Twin Drilling Program

During its drilling campaigns from 1984 to 1987, Naneco carried out a program of twin drilling. This comprised of ten twinned holes, as shown in Figure 12-1 and Table 12-1.

T Table 12-1 Naneco Twin Drilling Results

Table 12-1 Naneco Twin Drilling Results, Main Zone Drilling 1987									
Star Gold Corp. – Longstreet Au-Ag Project, Nevada									
Original Drill Hole					**Twin Drill Hole**				
Hole ID	**Interval (ft.)**		**oz/ton Au**	**oz/ton Ag**	**Hole ID**	**Interval (ft.)**		**oz/ton Au**	**oz/ton Ag**
	From	**To**				**From**	**To**		
LRH-1	0	35	0.018	0.42	LRH-53	0	35	0.008	0.23
LRH-1	35	105	0.080	0.80	LRH-53	35	105	0.041	0.61
LRH-1	105	115	0.027	0.28	LRH-53	105	115	0.004	0.14
LRH-1	0	35	0.018	0.42	LRH-250*	0	35	0.026	0.49
LRH-1	35	105	0.080	0.80	LRH-250*	35	105	0.098	0.63
LRH-1	105	115	0.027	0.28	LRH-250*	105	115	0.008	0.14
LRH-3	0	30	0.021	0.36	LRH-248*	0	30	0.016	0.33
LRH-3	30	70	0.012	0.25	LRH-248*	30	70	0.004	0.10
LRH-3	70	180	0.035	0.69	LRH-248*	70	180	0.031	0.76
LRH-5	0	50	0.028	0.23	LRH-247*	0	50	0.020	0.21
LRH-5	50	65	0.007	0.27	LRH-247*	50	65	0.005	0.14
LRH-5	65	90	0.198	0.53	LRH-247*	65	90	0.029	0.18
LRH-5	90	120	0.021	0.75	LRH-247*	90	120	0.013	0.81
LRH-5	120	195	0.010	0.59	LRH-247*	120	162	0.004	0.56
LRH-7	0	130	0.026	0.46	LRH-246	0	100	0.046	0.29
LRH-8	0	135	0.021	0.39	LRH-243*	0	155	0.018	0.40
LRH-8	135	155	0.025	1.90	LRH-243*	155	175	0.022	1.87
LRH-8	155	190	0.015	0.66	LRH-243*	175	190	0.002	0.44
LRH-18	0	15	0.013	0.41	LRH-245	0	15	0.013	0.41
LRH-18	40	95	0.018	0.55	LRH-245	40	95	0.011	0.44
LRH-50	0	50	0.009	0.21	LRH-244	0	50	0.014	0.27
LRH-50	50	65	0.012	0.28	LRH-244	50	65	0.082	2.74
LRH-50	0	50	0.009	0.21	LRH-21	0	50	0.046	0.97
LRH-50	50	65	0.012	0.28	LRH-21	50	65	0.003	0.35
LRH-51	0	20	0.012	0.12	LRH-249*	0	20	0.025	0.29
LRH-51	20	80	0.018	0.27	LRH-249*	20	80	0.011	0.20
LRH-51	80	100	0.004	0.06	LRH-249*	80	100	0.010	0.13
LRH-51	100	135	0.062	0.91	LRH-249*	100	135	0.013	0.49
Total length		**1,260**	**0.031**	**0.49**	**Total length**		**1,197**	**0.027**	**0.49**

Source: Prenn, 1988.Taken from Agnerian, 2013.

Results of the twin drilling by Naneco indicate that except for one pair of values, the silver assays from twin holes were, in general, comparable to the ones from the original holes. The gold assays, on the other hand, show poor correlation. Historically, poor correlations suggest either poor sampling or irregular gold distribution in the host rocks. It is the author's opinion, based on review of drilling results and check assays performed by MinQuest and Star Gold, that irregular gold distribution, most likely associated with 'nugget effect' or coarse gold, is more likely than any poor sampling technique.

12.2 MinQuest – Star Gold Twin Drill Programs 2011 and 2012

In 2011, MinQuest conducted a twin drilling program in which nine historical RC holes which had been utilized in the 1988 MDA Resource estimation were twinned with identical drill equipment, and sampled in 1.5 m intervals. The following table shows the assay results generated by this verification program.

U Table 12-2 2011 Twin Drill Holes Comparison

Table 12-2: 2011 Twin Drill Holes Comparison			
	Original Drill Holes	Twin Drill Holes	% Difference
Total Depth (m)	384	364.8	
Average Au (g/t)	1.06	0.93	12.30%
Average Ag (g/t)	16.8	16.8	0%
Total Samples	252	239	

The difference in the gold assay values is 12.3%, and is well within acceptable limits for gold determinations at these low concentration levels. This suggests that all of the 10,640 assay results for Au and Ag from 338 RCHs are probably characterized by the same precision.

In 2012, a more focused study was performed, in which four historical RC holes were twinned with core holes. The locations of anomalous Au/Ag in these paired drill holes match well except the lower portion of LS-1101 which does not match well with LS-1216C. This is believed to be caused by two high angle sheeted veins in LS-1101 not intersecting LS-1216C. While average values for +0.005 oz/ton gold equivalent (AuEq) zones are occasionally skewed dramatically by high-grade assays, these are thought of as a nugget effect. Cutting these rare high-grade samples produces very similar average grades between all pairs except the 1101/1216C set. Further statistical analysis was performed on each pair, including a calculation of all intercepts above 0.005 ounces per ton AuEq, and a paired two sample t-test. A table summarizing the results follows:

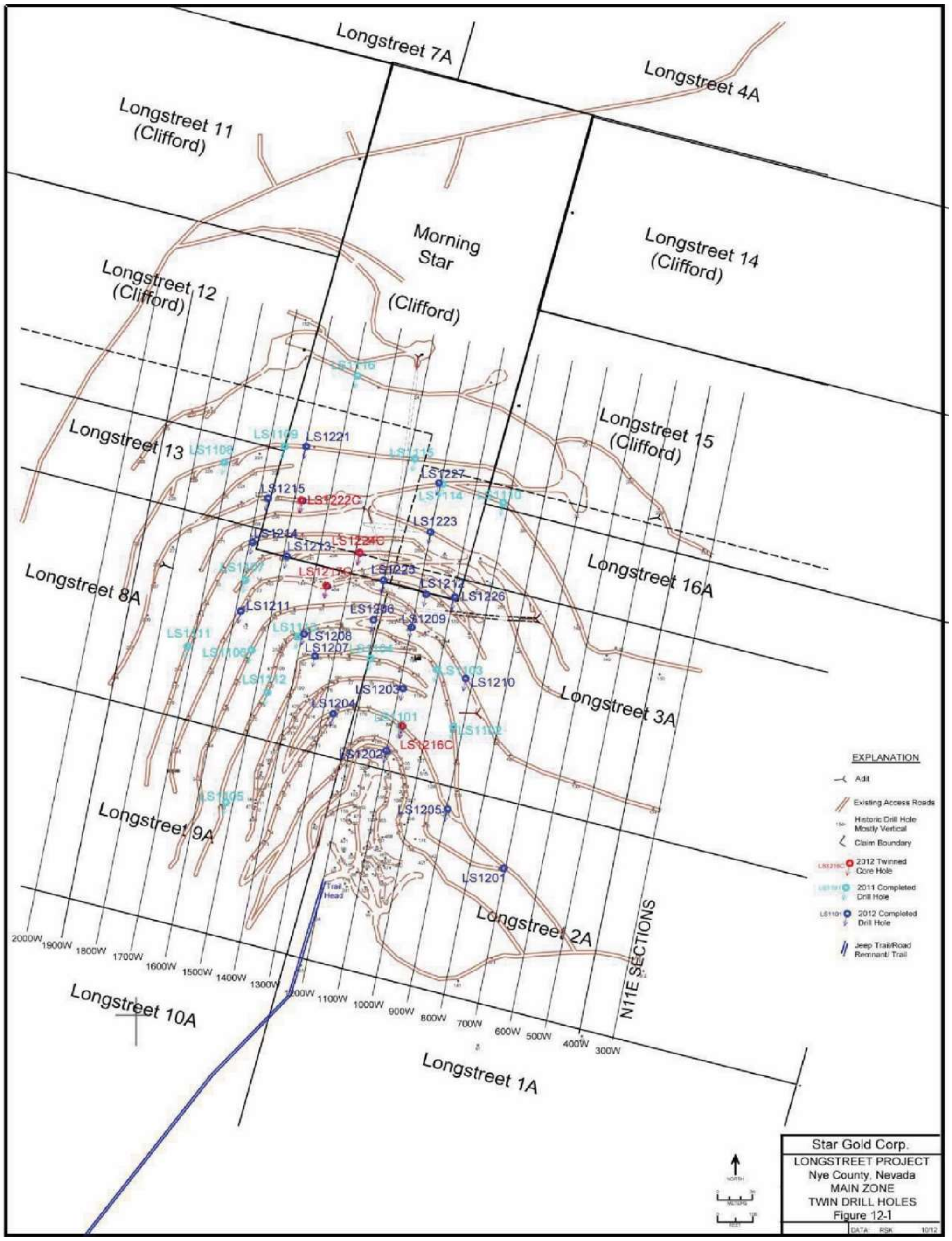
V Table 12-3 2012 Twin Drill Holes Comparison

Table 12-3: 2012 Twin Drill Holes Comparison					
DH No.	DH Type	Grade ≥0.005 oz/ton intercept (ft)	Grade ≥0.005 opt average (oz/ton)	Entire DH average (oz/ton)	P(T<=t)
LRH-242	RC	105	0.06	0.021	0.403
LS-1224C	Core	95	0.055	0.018	
PR-5	RC	170	0.026	0.015	0.329
LS-1217C	Core	185	0.026	0.017	

PR-9 LS-1222C	RC Core	125 130	0.039 0.02	0.017 0.01	0.075
LS-1101 LS-1216C	RC Core	305 240	0.021 0.016	0.018 0.011	0.022

Figure 12-1 shows the locations of the twinned core holes within the resource zone.

L Figure 12-1 Main Zone Twin Drill Holes



From Kern, 2012a.

Using a t-test, which rigorously tests the hypothesis that each assay pair, for the entirety of each drill hole, is sampling the same mineralized structures, two twin sets did very well (LRH-242/LS-1224C and PR-5/LS-1217C) and two sets failed the test (PR-9/LS-1222C and LS-1101/LS-1216C). This is thought to be caused by unacceptably wide drill hole separation, as much as 50 feet between LS-1101 and LS-1216C, and the occasional nugget effect high-grade. The twin sets which pass the t-test show less than 10% difference in average grade and intercept length, which implies that when drill hole separation is reasonably close, historical drilling data can be proven to be accurate. Additional twinned holes may be needed to increase the sample size and gain further statistical confidence.

The current author further inspected paper copies of drill assays from Harvest Gold drilling (PR-1 through PR-9) in order to verify the authenticity of the assays and Harvest's check sample program. The check samples included with the Harvest drilling involved re-submission of duplicate samples under blind sample numbers. The results of this check sampling program indicate reliable results and adequate methods.

Site visits by the author verifies the nature of the mineralization, the extent of the target zones, and the existence of drilling and underground workings.

It is the opinion of author that the data used in this report, including the drill assays from which the resource was calculated, are adequate and reliable.

13.0 Mineral Processing and Metallurgical Testing

Kappes, Cassiday and Associates (KCA) composited numerous oxide drill intercept cuttings and conducted bottle roll tests on 10 samples as requested by Naneco and reported by Harron (2003) and MDA (1988). Average results for -10 mesh samples were 85.4 percent gold and 37.9 percent silver recovery in 72 hours. Chemical consumption was normal. KCA then conducted column tests on three samples to test low, medium and high grade ore from underground. After crushing to -3/4 inch the samples averaged 82 percent gold and 29 percent silver recovery. Crushing to -6 mesh increased recovery to 93 percent for gold and 52 percent for silver. These are the currently expected recoveries for an open pit heap-leach operation at Longstreet.

KCA also conducted agitated cyanide tests on pulverized material and obtained 92 percent gold and 81 percent silver recovery. These are the recoveries expected in a conventional mill.

Column leach tests were also done by Bacon-Donaldson on -2 inch material. Recoveries varied from 85-90 percent for gold and 9-28 percent for silver, with underground samples being more susceptible to leaching than surface samples. It appears the oxide zone of the Main deposit has reasonable leaching characteristics although silver recovery is poor.

Although the Kappes, Cassiday and Associates results are somewhat dated, the methods used are essentially the same as would be utilized for current metallurgical testing of a gold-silver deposit with predominantly oxide material.

Star Gold commissioned an additional metallurgical testing program with McClelland Laboratories, Sparks Nevada in 2014. In summary, results of the bottle roll and column leach tests conducted by McClelland are in general agreement with the earlier tests conducted by KCA both for recoveries of gold and silver and response to crushing and grinding. A copy of the McClelland report is provided in Appendix 3.

Material for the McClelland testing consisted of composites of mineralized material collected from underground workings and from surface exposures. It is the author's opinion that future metallurgical testing be conducted on drill products (RC coarse rejects and core) for more representative results.

14.0 Mineral Resource Estimates

A mineral resource estimation has been prepared for the Longstreet Project. The resource estimate is confined to the Main Target Zone (Figure 6-3). Both an Indicated Mineral Resource and an additional Inferred Mineral Resource have been determined (see Table 14-1). The resource provided and described in this report was initially created and designed to meet the standards and definitions of CIM and NI 43-101 as part of an NI 43-101 Technical Report and Resource estimation on the Longstreet Project (Noland, 2014).

The definitions and standards utilized are described below:
"*In this Instrument, the terms "mineral resource", "inferred mineral resource", "indicated mineral resource" and "measured mineral resource" have the meanings ascribed to those terms by the Canadian Institute of Mining, Metallurgy and Petroleum, as the CIM Standards on Mineral Resources and Reserves Definitions and Guidelines adopted by CIM Council on August 20, 2000, as those definitions may be amended from time to time by the Canadian Institute of Mining, Metallurgy, and Petroleum."*

Further definitions and standards adhered to in this report are summarized here:

*"A **Mineral Resource** is a concentration or occurrence of natural, solid, inorganic or fossilized organic material in or on the Earth's crust in such form and quantity and of such a grade or quality that it has reasonable prospects for economic extraction. The location,*

quantity, grade, geological characteristics and continuity of a Mineral Resource are known, estimated or interpreted from specific geological evidence and knowledge."

The terms Measured, Indicated and Inferred as used in this report adhere to the following definitions:

"A ***'Measured Mineral Resource'*** *is that part of a Mineral Resource for which quantity, grade or quality, densities, shape, physical characteristics are so well established that they can be estimated with confidence sufficient to allow the appropriate application of technical and economic parameters, to support production planning and evaluation of the economic viability of the deposit. The estimate is based on detailed and reliable exploration, sampling and testing information gathered through appropriate techniques from locations such as outcrops, trenches, pits, workings and drill holes that are spaced closely enough to confirm both geological and grade continuity."*

*"An '***Indicated Mineral Resource***' is that part of a Mineral Resource for which quantity, grade or quality, densities, shape and physical characteristics, can be estimated with a level of confidence sufficient to allow the appropriate application of technical and economic parameters, to support mine planning and evaluation of the economic viability of the deposit. The estimate is based on detailed and reliable exploration and testing information gathered through appropriate techniques from locations such as outcrops, trenches, pits, workings and drill holes that are spaced closely enough for geological and grade continuity to be reasonably assumed."*

*"An '***Inferred Mineral Resource***' is that part of a Mineral Resource for which quantity and grade or quality can be estimated on the basis of geological evidence and limited sampling and reasonably assumed, but not verified, geological and grade continuity. The estimate is based on limited information and sampling gathered through appropriate techniques from locations such as outcrops, trenches, pits, workings and drill holes."*

Conventions used in the resource estimation are given here. All mineral grades are reported in gold- equivalent (AuEq) troy ounces per short ton (oz/ton). All gold-equivalent (AuEq) values are determined by adding the assayed gold value to 1/60 of the assayed silver value in the following manner: *AuEq = Au oz/ton + ((Ag oz/ton)/60).* All distances are recorded and calculated in feet, all mass calculations are made in short tons.

The 2014 resource is presented here unmodified. The author is aware that SK 1300 definitions vary slightly from those of NI 43-101. However, it is the author's opinion that the methods and data utilized are sufficient to meet current SK 1300 criteria for 'indicated' and 'inferred' resource.

The author further recognizes that current metals prices would certainly impact factors such as the gold-silver equivalency (AuEq) and cut off grades in a new resource calculation. However, the 2014 resource, as presented here, is considered to be a valid 'base line' resource until additional drilling, resource development and definition, metallurgical testing and economic analyses are completed for Longstreet.

The 2014 Longstreet resource is summarized in the table below:

W Table 14-1 Longstreet Resource Summary

Table 14-1: Longstreet Resource Summary							
Category	Tonnage	AuEq (opt)	Au (opt)	Ag (opt)	AuEq (oz)	Au (oz)	Ag (oz)
Indicated	8674951	0.0199	0.0131	0.4118	172944	113409	3571986
Inferred	2399648	0.0167	0.0079	0.5284	40138	19005	1267945
Total	11074599	0.0192	0.0120	0.4370	213082	132414	4839931
Pit	30263060	Lower cutoff grade: 0.005 opt AuEq					
Waste	19188460						
Strip Ratio	1.73						

14.1 Conventions and Methodology

Conventions used in the resource estimation are given here. All mineral grades are reported in gold- equivalent (AuEq) troy ounces per short ton (oz/ton). All gold-equivalent (AuEq) values are determined by adding the assayed gold value to 1/60 of the assayed silver value in the following manner: *AuEq = Au oz/ton + ((Ag oz/ton)/60).* All distances are recorded and calculated in feet, all mass calculations are made in short tons.

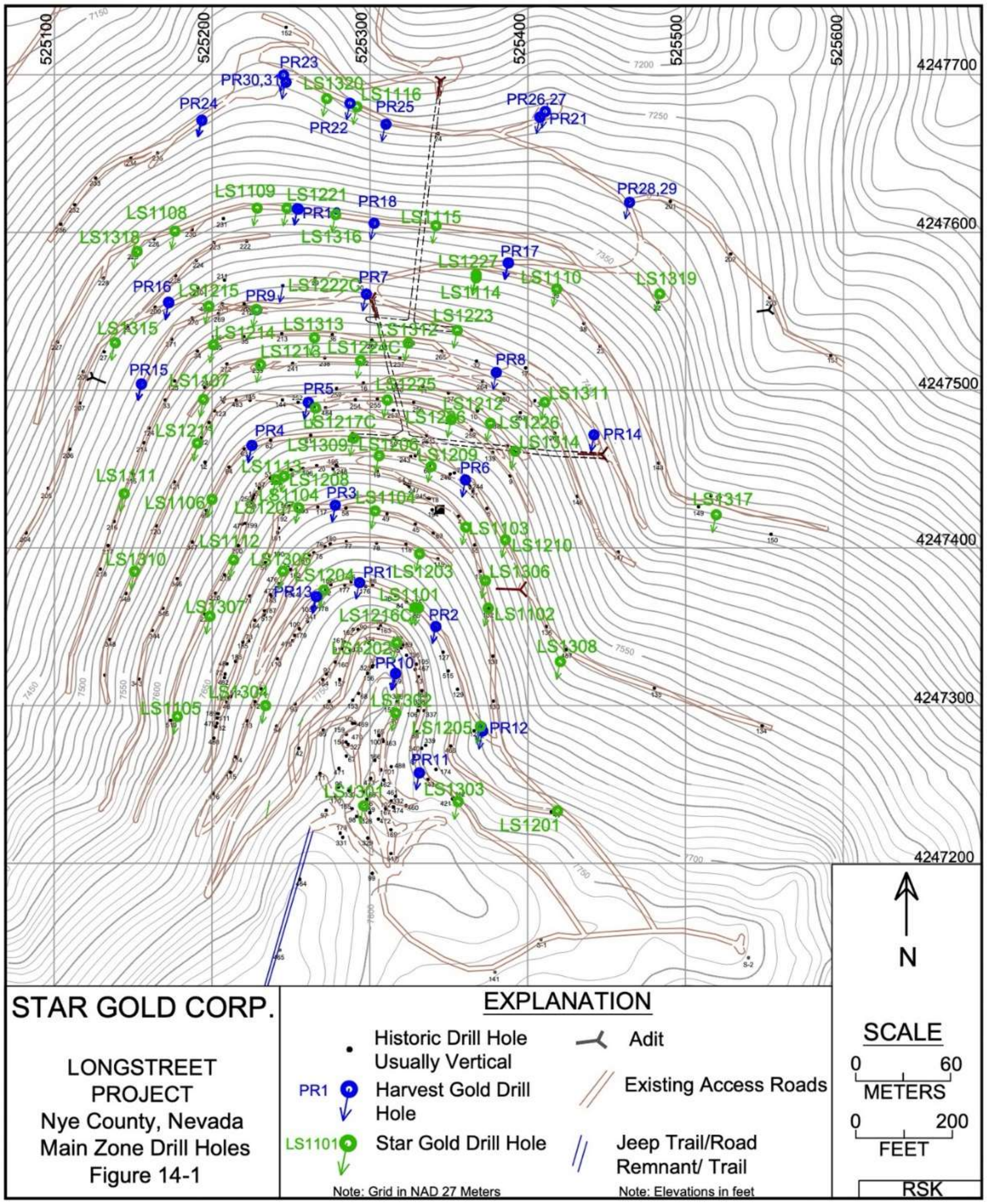
By loading a created Longstreet project drilling database into the Micromine software, and performing grade interpolation with the known density in the main zone, a resource estimate has been created. Using a nominal cut-off of 0.005 oz/ton AuEq, and focusing solely on areas of close drill spacing, the Indicated resource is calculated to be approximately 8.7 million tons at an average grade of 0.0199 AuEq, containing approximately 172,000 ounces of AuEq. An additional Inferred resource was calculated by extending the mineral interpretation beyond areas of closest drill spacing. This additional Inferred resource was calculated at approximately 2.4 million tons at an average grade of 0.0167 AuEq, for an additional contained AuEq of approximately 40,000 ounces (Table 14-1 Longstreet Resource Summary).,

14.3 Database and Wireframe Interpretation

These resource estimations were created by loading all relevant drilling and assay data into Micromine, then performing block modeling and an Inverse Distance Weighting (IDW) interpolation with the database. The loaded database consists of drill hole coordinates, surveys, and assay data for 427 drill holes, as shown in Figure 14-1. When assays were not available for drilling intervals, the AuEq value for the intercept was left blank, and Micromine was set to ignore that intercept. Other forms of validation were performed on the database before the estimation was created, and all of the following errors reported by the Micromine software were corrected:

- *Duplicate Drill (or underground sampling) ID;*
- *Missing collar coordinates;*
- *'From' or 'To' values missing in assay file';*
- *Non-contiguous or overlapping assay intervals;*
- *Multiple survey for same depth;*
- *Dip angle and azimuth fall into inappropriate ranges;*
- *Missing azimuth or dip angle in collar data;*
- *Total depth of hole less than depth to included assays.*

Figure 14-1 Drilling Plan View



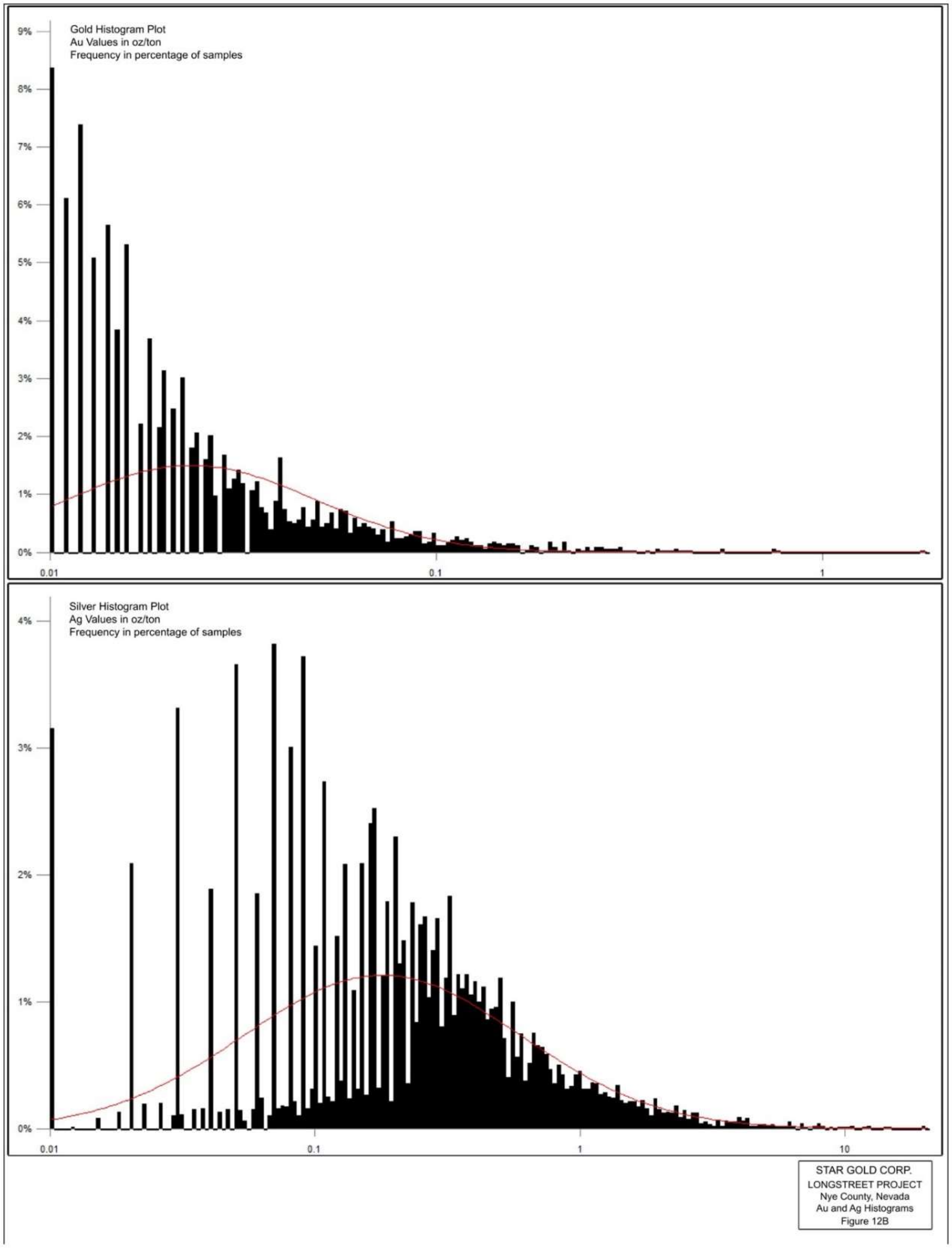
Holes that could not be appropriately corrected (for example, historical drilling with insufficient coordinate data) were thrown out, and no calculations were performed with them. Once all drill and underground sampling data were validated in this manner, they were loaded into

Micromine's interactive viewer and examined as a secondary validation to ensure drill holes and underground samplings fell within appropriate areas of the project. During this step, a visual validation insured that collars fell within accepted limits of the digital topographic surface utilized in the model. An additional validation step involved checking roads and drill sites as plotted on the digital model against air photo overlays to ensure correct placement.

In order to minimize the impact that rare outliers in assay data have on the overall accuracy of the project, all assay intervals above expected values are cut (capped) to a reasonable level. Termed the 'balancing cut,' this procedure is done to avoid the 'nugget' effect, where an unusually high assay will incorrectly raise the estimated values around it.

Histograms for raw gold and silver assay data were created and are included as Figure 14-2; statistical analysis was run for the assay data, the results of which are provided in Table 14-2 below. The value of the third deviation was chosen as the point at which to cut values, ensuring that any assays greater than 99.86% of all assays would not unfairly affect surrounding estimates.

M Figure 14-2 Histogram Plots Au and Ag



The specific grade cap was calculated to be 0.380 ounces per ton Au and 8.3 ounces per ton Ag; all values above these grades were cut to exactly 0.380 and 8.3 respectively. After the cut was applied to the assay data, compositing was run upon the drill data. A composite width of 5 feet was used to ensure the data was granular and would best fit to our chosen sub block size.

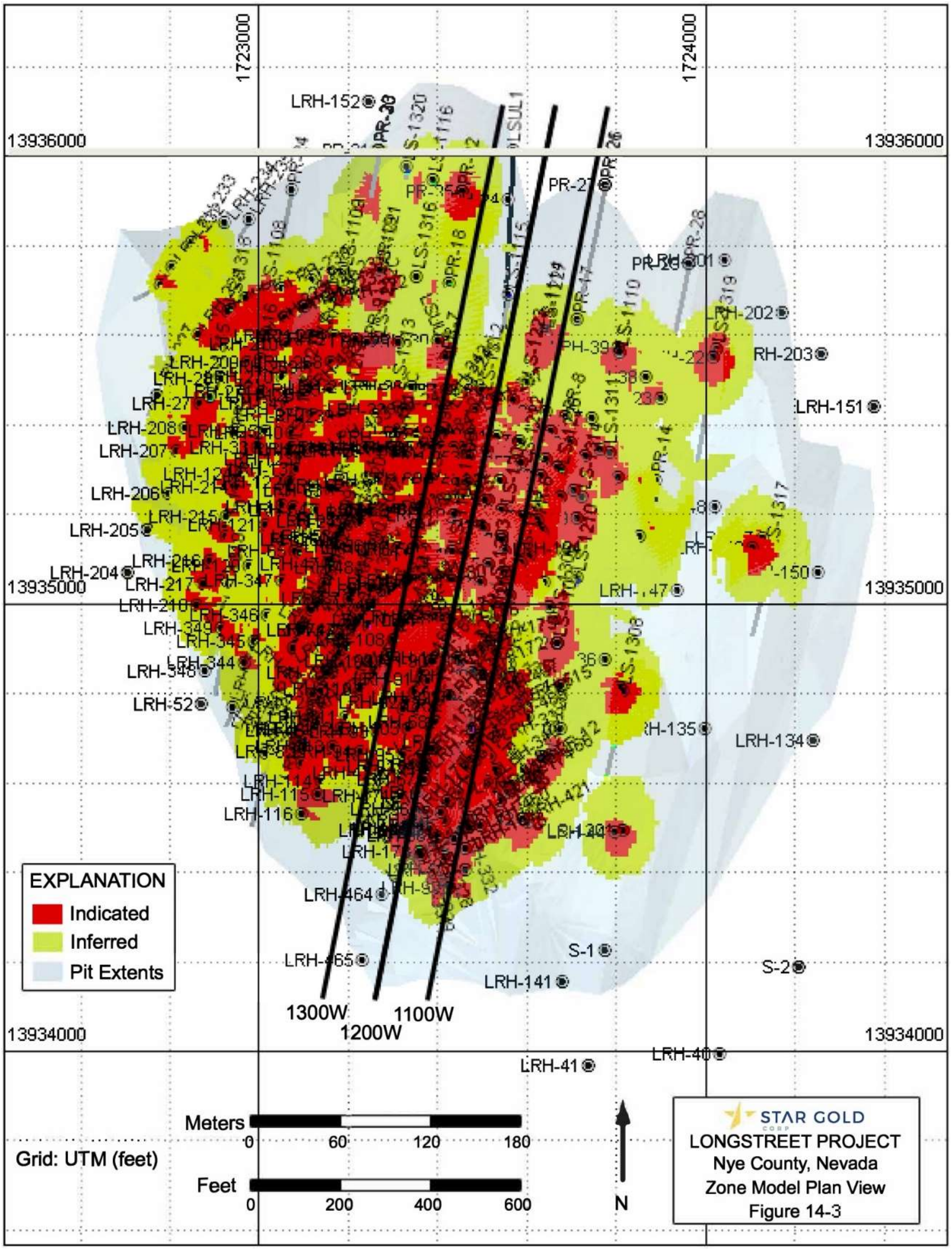
All calculations were performed within the Micromine program, and the compositing step was saved to a second version of the assay interval file. This balanced and composited version of the interval file was used for all subsequent calculations, and its statistics are included in the following table for comparison to the original.

X Table 14-2 Longstreet Assay Statistics

Table 14-2: Longstreet Assay Statistics				
	Pre-Composite		Post-Composite	
	Au	Ag	Au	Ag
Count	9461	9960	9242	9726
Median	0.0060	0.1900	0.0060	0.1900
Mean	0.0146	0.3745	0.0140	0.3653
Mode	0.0013	0.0900	0.0013	0.0900
Minimum	0.0010	0.0100	0.0008	0.0100
Maximum	1.8340	20.0020	0.3800	8.3000
Bin Size	0.0005	0.0200	0.0005	0.0200
Variance	0.0014	0.5773	0.0008	0.4339
Standard deviation	0.0373	0.7598	0.0287	0.6587
Coefficient of variation	2.5551	2.0291	2.0485	1.8030
84th percentile	0.0210	0.5400	0.0210	0.5400
97.7th percentile	0.0850	2.0000	0.0830	1.9800
99.86th percentile	0.3800	8.3000	0.3700	8.1700

After compositing was complete and verified, a wireframe interpretation for the Longstreet project was then created within Micromine. This was performed by a geologist familiar with the project, who created a three-dimensional wireframe interpretation of the mineralized zones within the Main Zone, based upon drill hole assays and known areas of permissive geology and structures. Three mineralized zones were defined which represent areas of grade and structural continuity. These zones are referred to in this report as the Upper, Middle, and Lower Zones. The final result of this wireframing is shown in the block model view in Figure 14-3.

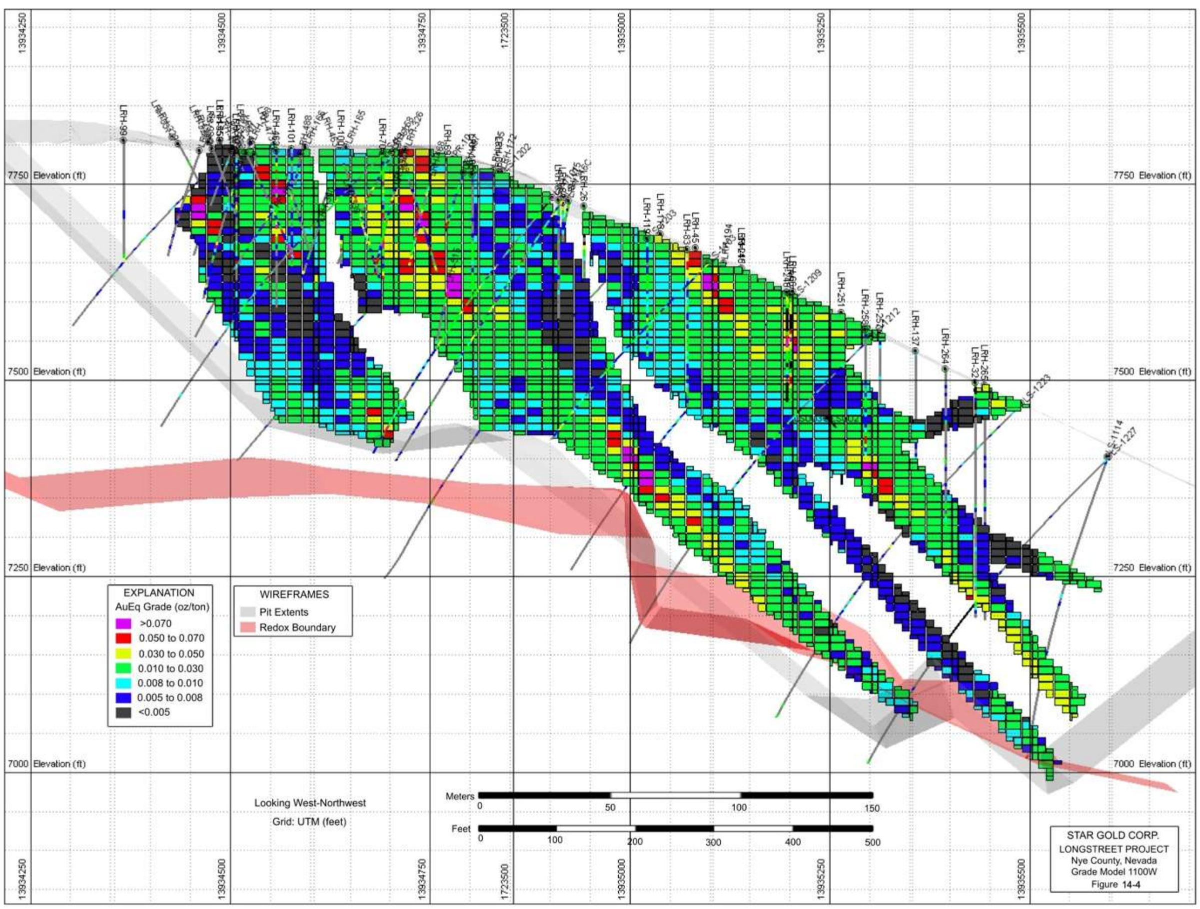
N Figure 14-3 Zone Model Plan View



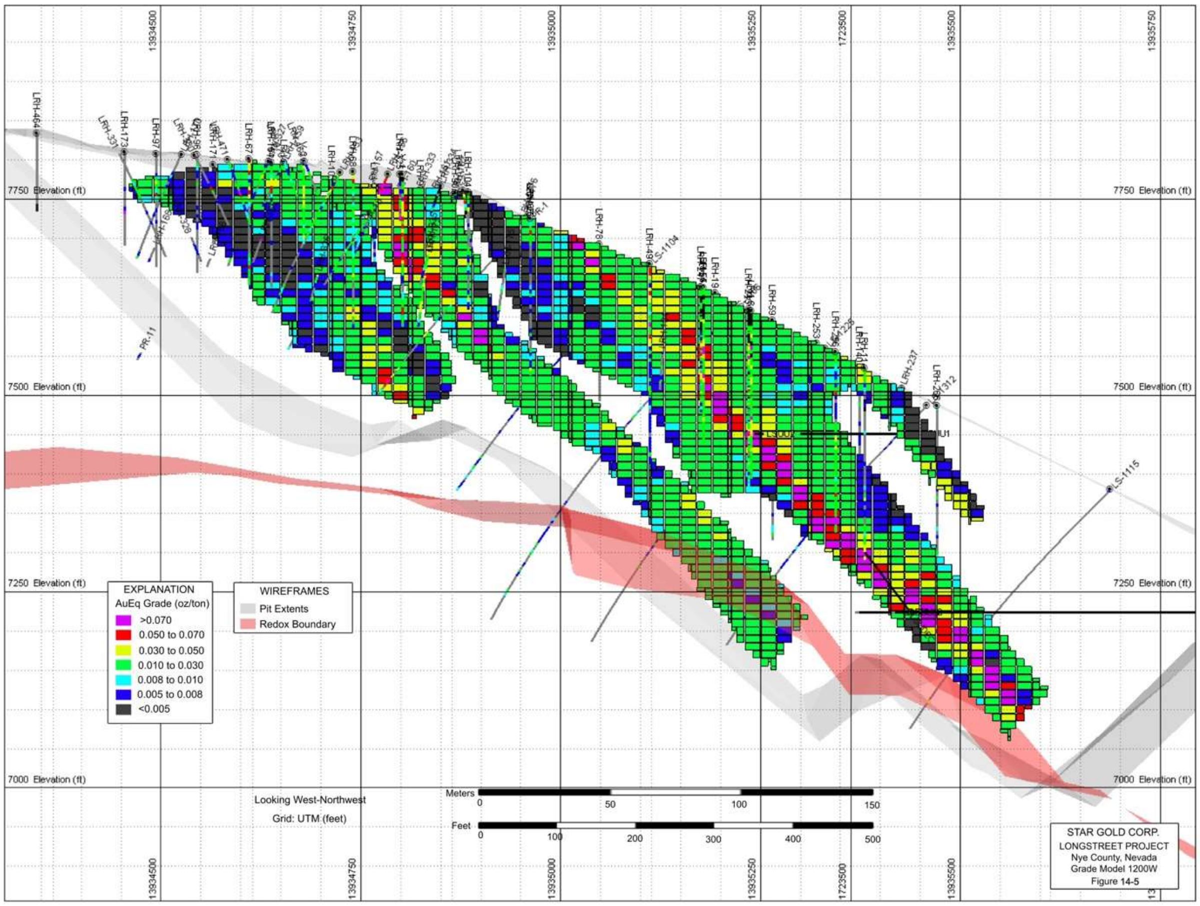
The mineralization wireframes define the maximum limits of the resource estimation. By restricting the volume to which subsequent calculations by the software can apply interpolated block grades, the shapes provide an upper limit for the mineralized tonnage which may be contained in the model. All samples and all volume beyond the limits of this wireframe interpretation are ignored by the IDW calculations. No volume or blocks beyond the limits have any defined tonnage or grade, and do not contribute to the final estimate.

The final step in interpretive wireframing was to model the redox boundary. The boundary between oxide material and sulfide material was determined from visual inspection of drill cuttings and the presence of sulfides as noted in drill logs for all Star Gold drilling. The modeler created a continuous digital terrain model (DTM) wireframe marking the interpreted redox boundary, which can be seen in Figures 14-4 through 14-9.

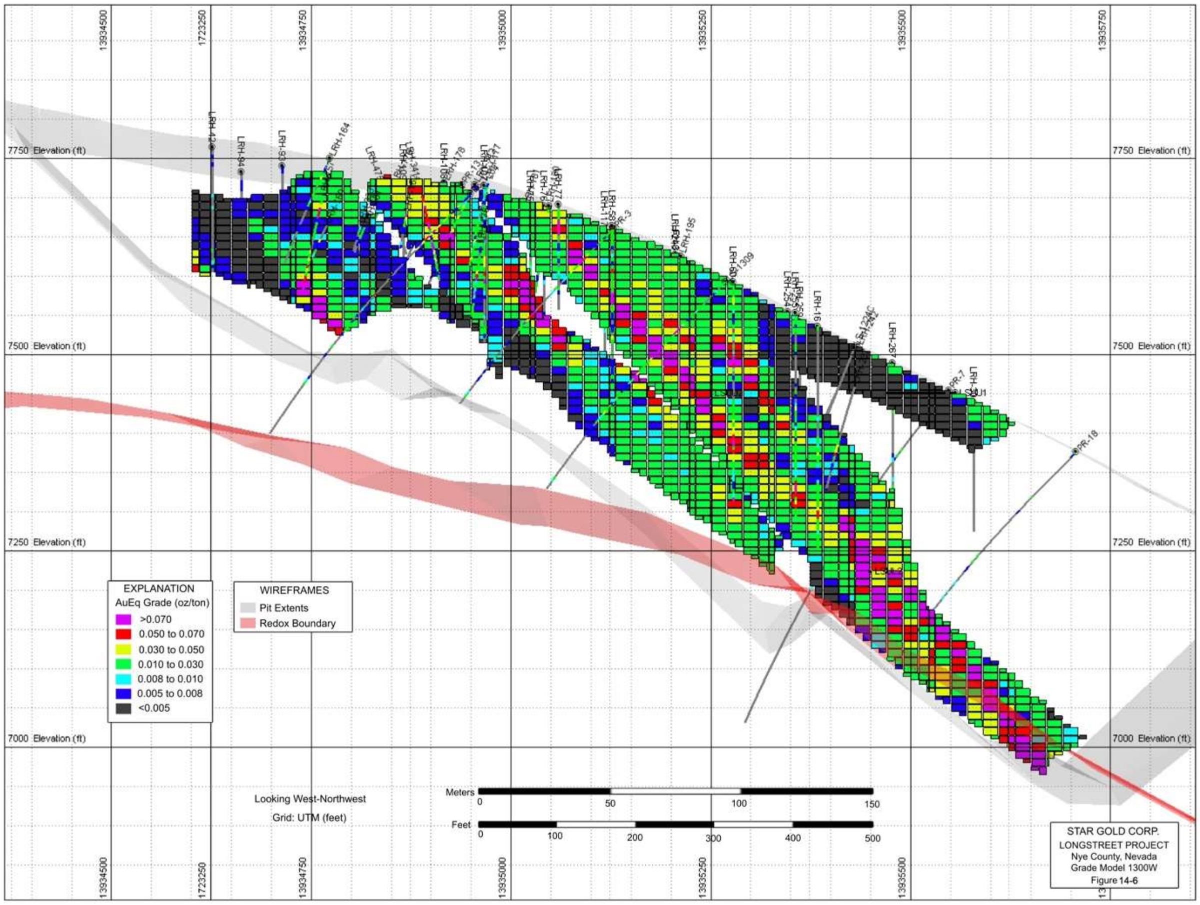
O Figure 14-4 Longstreet Grade Model Section 1100 W



P Figure 14-5 Longstreet Grade Model Section 1200 W

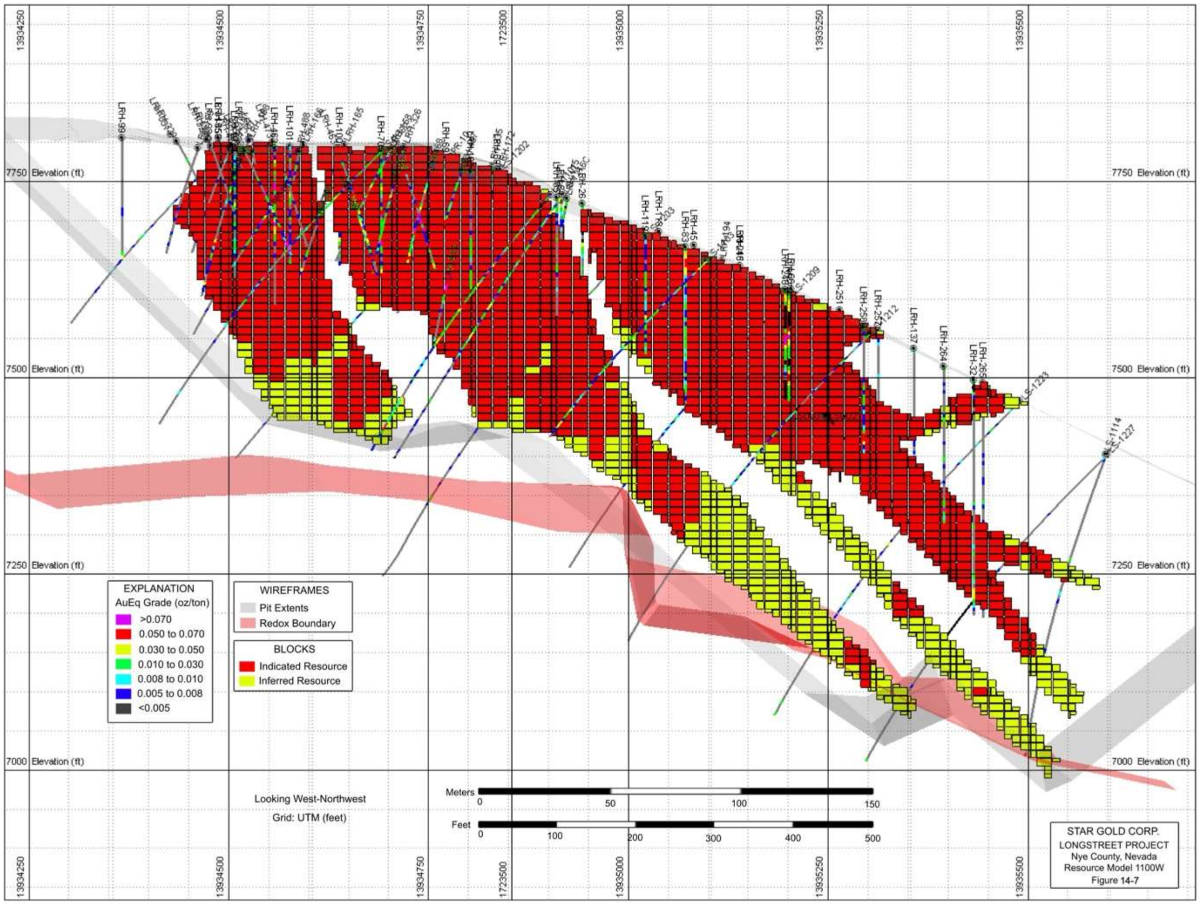


Q Figure 14-6 Longstreet Grade Model Section 1300 W

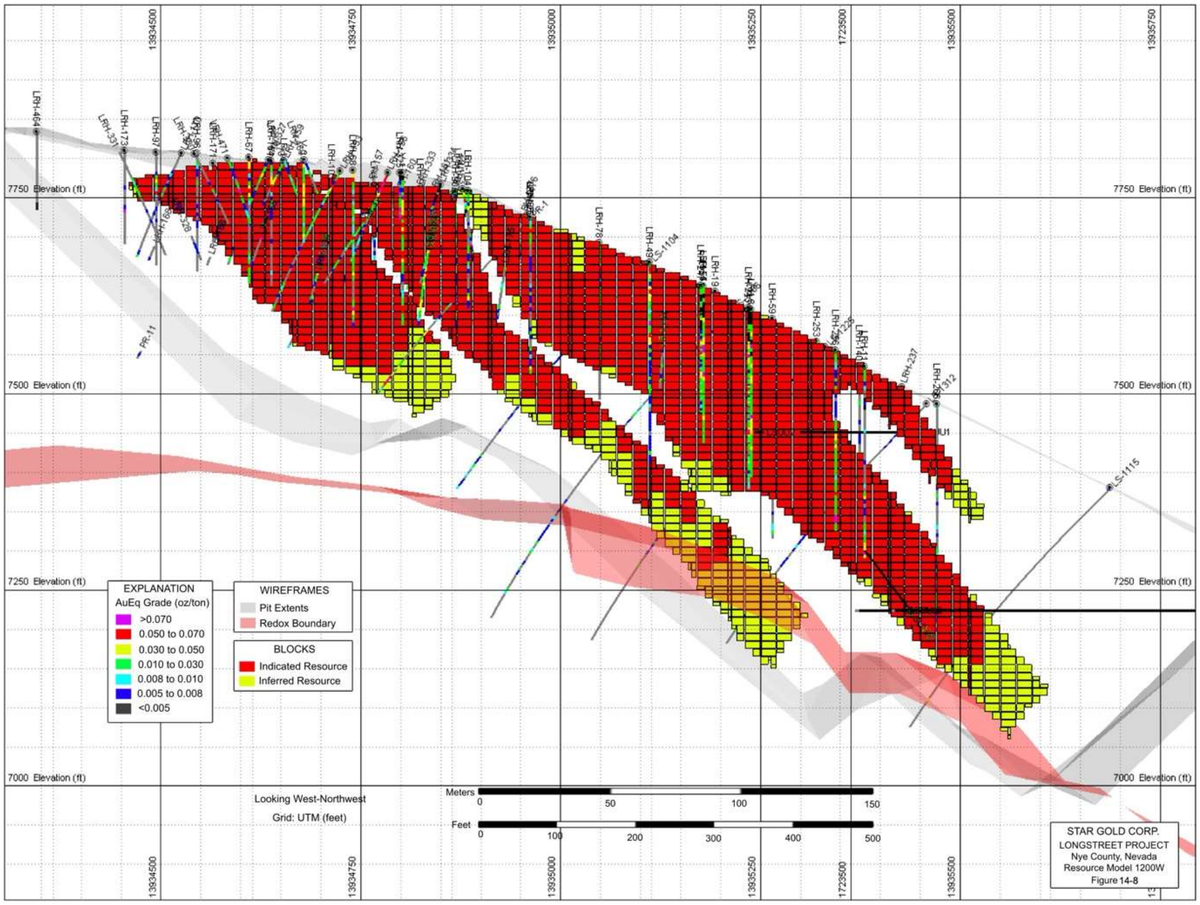


Once wireframing was completed, the database was flagged to designate the three primary mineral zones and to reflect the REDOX boundary. Composited samples which lay within the Upper, Middle, or Lower Zones were flagged with the respective name of the zone. Samples which lay above the redox boundary were flagged as Oxide, and samples that lay below the boundary were flagged as Sulfide. Ultimately in the creation of block model and resource calculations, these flags transfer to the individual blocks of the block model, such that the final reporting may be reported by zone, and blocks below the redox boundary can be ignored and discarded.

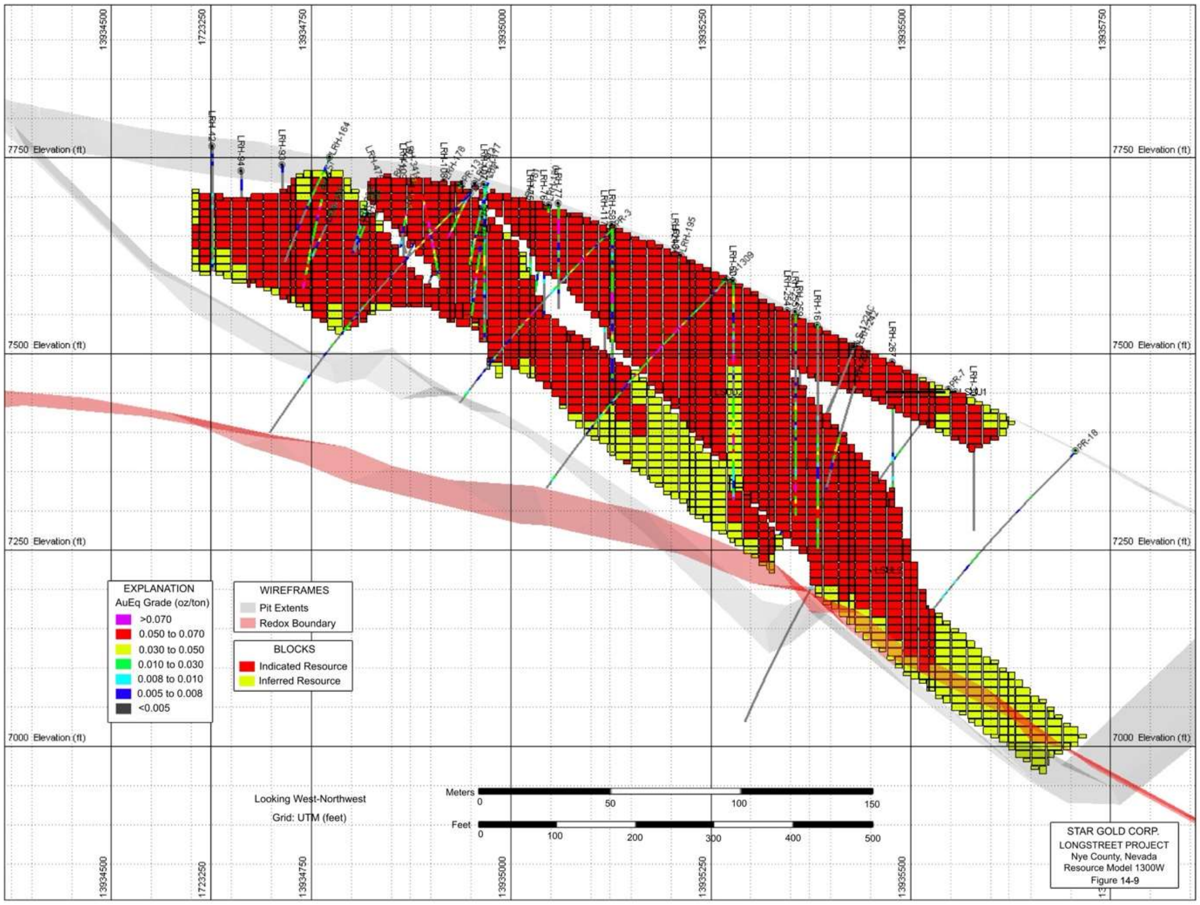
R Figure 14-7 Longstreet Resource Model Section 1100 W



S Figure 14-8 Longstreet Resource Model Section 1200 W



T Figure 14-9 Longstreet Resource Model Section 1300 W



14.4 Specific Gravity

Volumes calculated in cubic feet were converted to short tons by using a conversion factor (tonnage factor) of 13.358 cubic feet per ton. This conversion was derived by the following formula: *cubic feet/short ton = 0.9072 (short tons/metric tons) / (specific gravity * 0.02832 (cubic feet/cubic meters)).* The specific gravity (SG) value was the weighted mean value of 8 representative core samples collected from the width of the main zone of the Longstreet project. The specific gravity determinations were conducted by ALS Chemex. The specific gravity results are presented below in Table 14-3:

Y Table 14-3 Specific Gravity Results

Table 143Specific Gravity Results	
Sample ID	Specific Gravity
LS 1216C 85-89	2.48
LS 1216C 213.2-213.6	2.51
LS 1217C 65.3-65.8	2.44
LS 1217C 175-175.3	2.48
LS 1222C 74.2-76	2.22
LS 1222C 191.2-191.5	2.32
LS 1224C 109-109.3	2.19
LS 1224C 200.8-201	2.34
Weighted mean	2.39
Final density	13.358 cubic feet/short ton

All tonnage calculations of wireframe and block volumes within the Micromine program were assigned a value of 13.358.

14.5 Cut Off Grade

A cut-off grade of 0.005 oz/ton AuEq was selected for all estimations and pit designs on the Longstreet project. Firstly, an examination of drill sections such as Figures 14-4 through 14-6 with the color coded assay brackets shows a good correlation between the dipping mineralized veins and the assay bracket of 0.010 to 0.0299 oz/ton AuEq. In most cases throughout the resource area, the mineralization drops abruptly and sharply outside the mineralized shapes. Further examination of drill assay tables supports this conclusion. Statistical analysis was applied to the Longstreet drill data, as seen in Figure 14-2, and visual inspection of assays throughout the mineralized area reveal a clustering of mineralized intercepts around a cut-off grade of 0.005 to 0.010 oz/ton AuEq. Outside of the mineralized areas, the Au and Ag values drop significantly, and rarely have 'kicks' or isolated higher values.

Based upon precious metals price forecasts and expected operating and processing costs, Agnerian and Routledge (2013) calculated a cut-off grade for the main zone of 0.004 oz/ton Au without mining costs included, and 0.007 oz/ton Au with mining costs. Final reporting cut-off grade for Agnerian's 2013 report was 0.005 oz/ton Au.

This cutoff is supported by similar or even lower cut-off grades from mines and announced resources in Nevada, taken from 2003-2012 (appropriate for the time frame the current resource was calculated) as seen in Table 14-4:

Z Table 14-4 Published Cut Off Grades for Selected Nevada Mines and Resources 2003-2012

Table 14-4: Published Cut-off Grades for Selected Nevada Mines and Resources	
Barrick Pipeline-Cortez Mine.	Cut-off = 0.003 oz/ton Au (Noland, 2008)
Barrick-Kinross Round Mountain	Oxide cut-off = 0.006-0.018 oz/ton Au Sulfide cut-off = 0.010-0.018 oz/ton Au (Kinross Annual Reports, 2003-2008)
Allied Nevada Gold Corp.	Oxide Cut-off = 0.004 oz/ton Au
Hycroft Mine	Sulfide Cut-off = 0.010 oz/ton Au (Wilson, S. E., 2012)
Corvus Gold Inc. – Bull Frog	Cut-off = 0.003 opt Au (Corvus Gold, 2012)
Midway Gold Inc. – Pan	Cut-off = 0.006-0.008 oz/ton Au (Midway Gold, 2012)
Comstock Mining - Comstock	Cut-off = 0.007 (Comstock Mining, 2011)

An AuEq cut-off at or below 0.010 is also supported by the MDA (1988) study of Longstreet conducted for Naneco. Although this study utilized fewer drill holes than are available now, it did consider essentially the same 'Main Zone' resource area reported on here. In a detailed study, MDA concluded an economic open pit with heap leach recovery of Au and Ag at Longstreet would have a strip ratio of 0.95 at a cut-off grade of 0.010 Au (note that no Ag value was included in the MDA cut-off). With both 2014 and current metals prices much greater than those at the time of the MDA report, it is suggested that a strip ratio of 3 or 4 to one at Longstreet would remain economically viable, with the initial pit design (visible in Figures 14-4 through 14-9) keeping a conservative ratio of 1.73 to one.

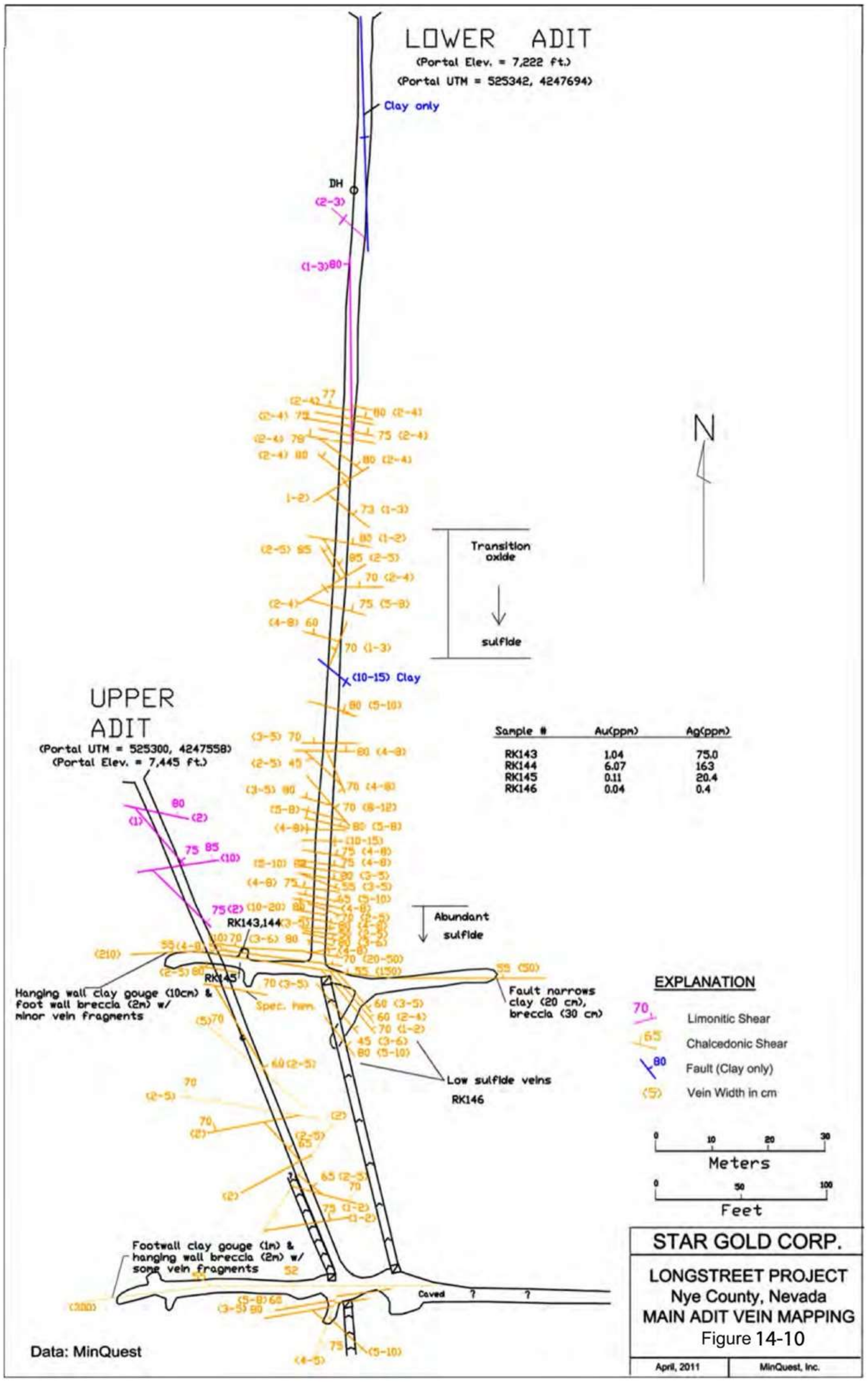
14.6 Block Model and Search Routine

A blank block model was created in Micromine, bounded by the limits of the project's mineralization as defined by the wireframes of the Upper, Middle, and Lower Zones. All blocks in the model were 20 feet north to south, 20 feet east to west, and 10 feet vertical, except where a block would straddle the boundary of the mineralization, in which case the program may halve any or all dimensions to best fit the boundaries. The result of this is a three-dimensional model of the mineralized zones, made entirely of blocks. Each block is blank at this stage, but in later steps may be assigned AuEq values. A flag may also be set on each block, for being either Indicated or Inferred (never both), or it may be left blank to denote an area of no confidence. The blank model is visually verified as lying entirely within the three interpreted zones, as visible in Figure 14-3.

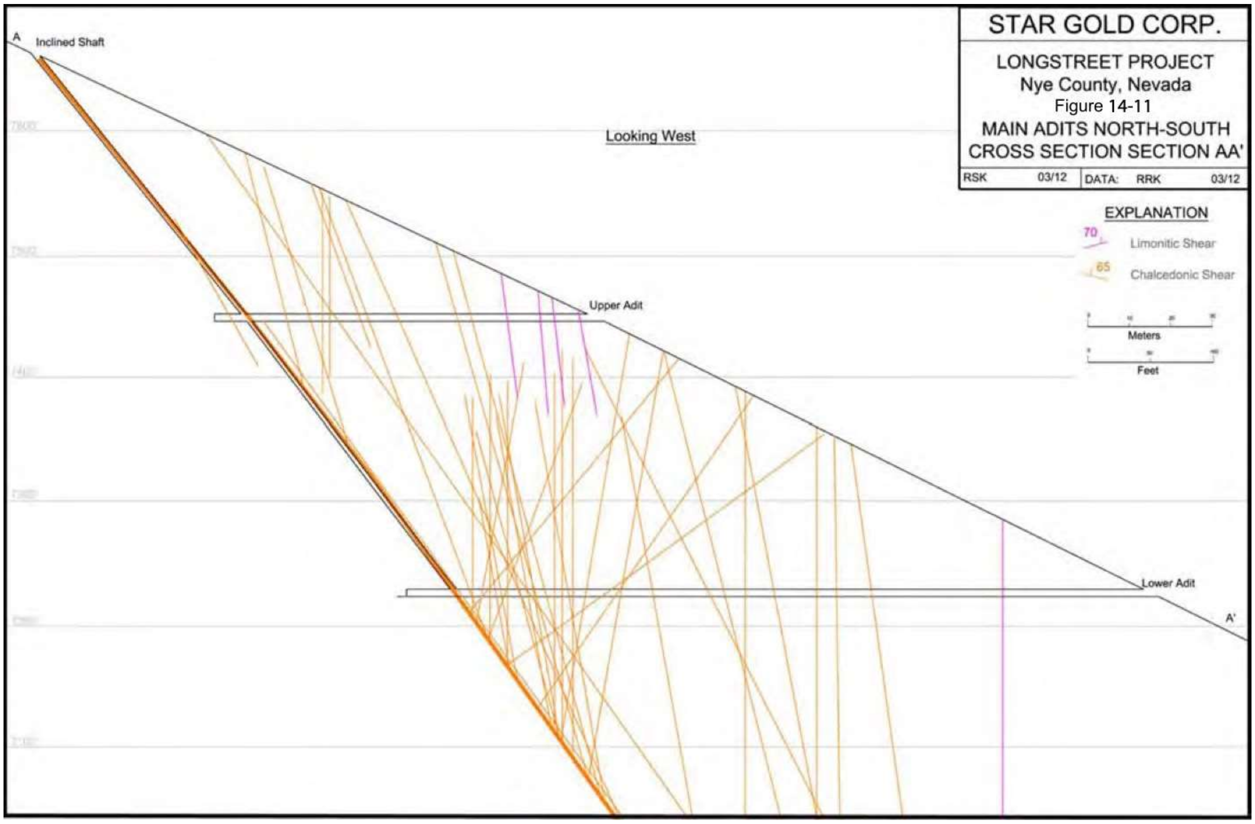
An Inverse Distance Weighting (IDW) search algorithm was then defined. The selected IDW search pattern uses an ellipsoid, the longest axis of which is biased to the trend of the veins and structures evident on the property. The search will look farther along this trend, and restrict its view to a shorter distance perpendicular to the trend. The search strike and dip were determined from the trend of geologic continuity at the Longstreet property, which was determined by a geologist familiar with the project using drill data and historical structures.

The dip direction and angle are reflected in the direction of the line of intersection of the two principal vein orientations mapped in the lower and upper adits shown in Figure 14-10, which are known to be N11E (011 degrees). The search dip was taken from the dip of the Adit Fault and of its associated decline, shown in Figure 14-11, known to be 53 degrees below horizontal. As a result the specified search strike was set perpendicular to N11E (011), therefore 281 degrees, and the dip was set to 53 degrees. The specific dimensions of the IDW search ellipsoids were determined by drill spacing and confidence in trend continuity. As the continuity down the dip is excellent, the long axis of the search ellipsoid is set in this direction. Appropriate search radii in the down-dip direction were determined to be 100 feet for the initial Indicated pass and 200 feet for the secondary Inferred pass. Continuity along strike is good, but not as reliable as that down dip. Consequently, search radii of 60 feet for the Indicated pass and 120 feet for the Inferred were selected for this dimension. Most drilling performed by Star Gold is angled along the third semi-axis, allowing for a high confidence level in true widths of the intercepts and overall continuity is. The search in this direction is set to match these demonstrated true widths, thus 20 feet for the Indicated pass and 40 for the inferred.

U Figure 14-10 Main Adit Vein Mapping Results



V Figure 14-11 Main Adit Cross Section



The final chosen Indicated search ellipsoid is shown in Figure 14-12 arbitrarily placed next to the historical decline to best show the relation. Table 14-5 below shows the final radius of each semi-axis.

AA Table 14-5 IDW Search Parameters

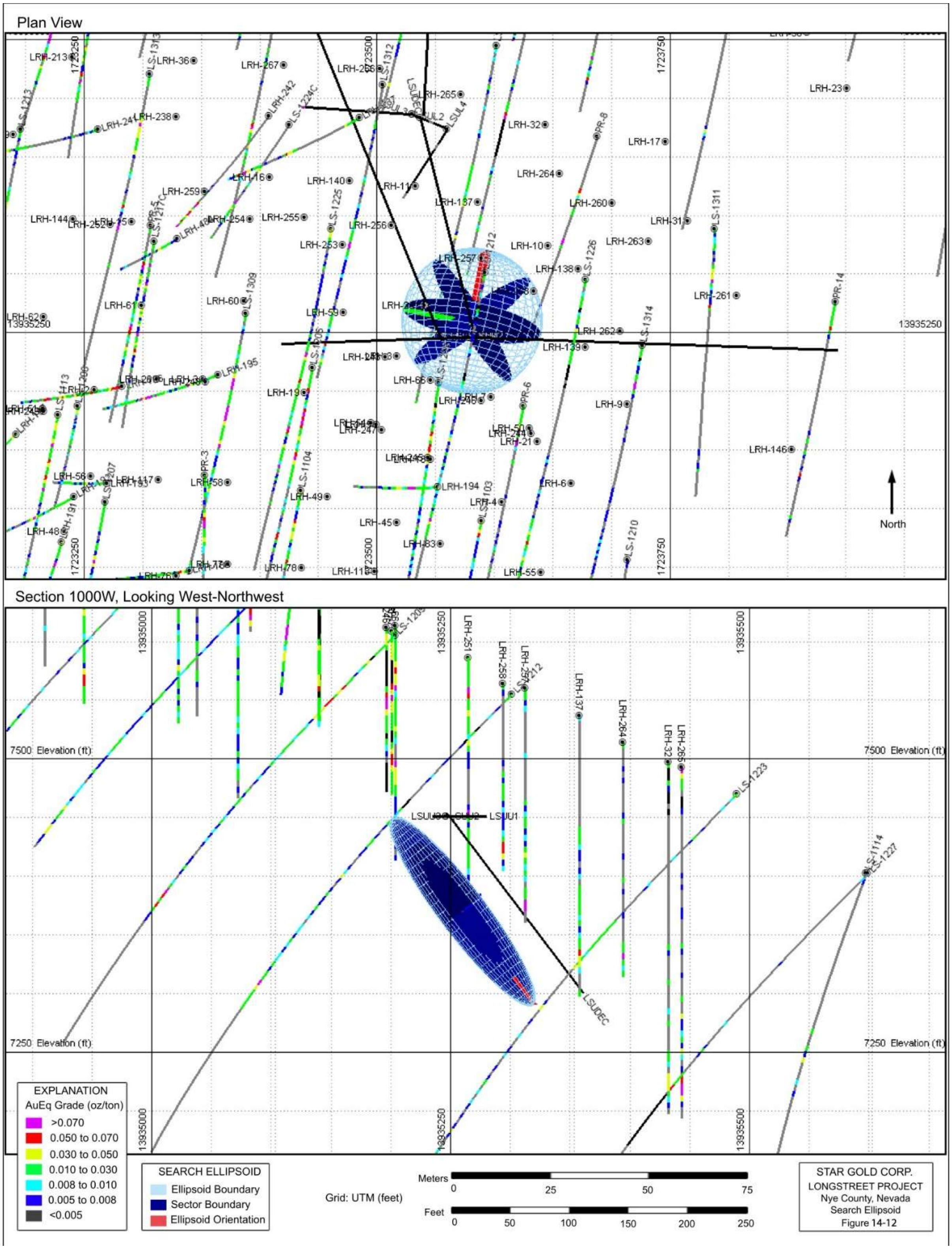
Table 14-5: IDW Search Parameters				
	Azimuth	Dip	Radius (Indicated)	Radius (Inferred)
Along dip Semi-axis 1	11°	53°	100 feet	200 feet
Along strike Semi-axis 2	281°	0°	60 feet	120 feet
Thickness Semi-axis 3	169°	37°	20 feet	40 feet

In the final step before interpolation is run, a declustering method is applied to the search ellipsoid. In order to prevent our selective interest in high grades from unfairly raising the calculated grade of the block model, the ellipse is divided into sectors, and a limit on the number of samples selected per sector is applied.

After selecting the nearest samples up to the maximum number allowed per sector, the search routine must choose samples in another sector, thereby ensuring the search makes its calculations on samples in all directions, rather than solely a high grade cluster in any one direction. Iterative testing determined that eight sectors, with a maximum of four samples per sector, reduced the clustering effect without excessively decreasing the grade and overall resource.

The sectors are best displayed in the plan view of Figure 14-12 Search Ellipsoid.

W Figure 14-12 Search Ellipsoid



Interpolation was then performed on the blank block model. The Indicated search ellipsoid was placed on each block in the model, and if at least two drill holes with four valid samples were found within the radii of the ellipsoid, that block was assigned a gold and silver value by IDW, and flagged as 'Indicated'. In the case that a block failed this search, it was left blank.

Once all blocks within the flagged model were checked in this initial, 'Indicated pass', Micromine then performed a second IDW procedure on remaining, unpopulated blocks utilizing the larger, Inferred search dimensions, and the minimum number of holes was reduced from 2 to 1. When this search was successful, the block was assigned values by IDW and flagged all blocks meeting the defined criteria as 'Inferred'.

IDW, by definition, reduces the weight of a sample by a power of its distance from the block, such that more distant samples contribute less to the grade of the block. A power of 3 was chosen to *most accurately and conservatively* interpolate the narrow-vein gold bearing structures at the Longstreet property.

The results of these searches are displayed in the figures reference earlier. A plan view showing the surface of the blank block model, colored by interpreted zone (Upper/Middle/Lower), is shown in Figure 14-3. Figures 14-4, 14-5, and 14-6 show the fully interpolated block model in cross section form, will drill holes and blocks colored by AuEq grade. Figures 14-7, 14-8 and 14-9 show the same blocks colored by Indicated/Inferred status.

Finally, all blocks below the redox boundary (visible in Figures 14-4 through 14-9) were then flagged as Sulfide, and all above were flagged Oxide. Only 953 blocks out of the model-wide total of 64,661 blocks fell below the REDOX boundary.

14.7 Validation, Pit Model, and Final Results

From the model views as provided above, another validation was performed. It is apparent that grade continuity is good along the known strike and dip of the veins, and that areas of best confidence coincide with areas of greatest drilling density. Areas with fewer drill holes, particularly toward the north end of the Upper Zone, and most areas deeper than 400 feet, are considered by our search algorithm to be either 'Inferred' resource or no resource at all, as little confidence can be made from the data available. The cross section views for AuEq grade clearly displays the main vein which is further defined by historical underground workings. Other displayed bands of high grades follow the predicted trends of gold bearing mineralization, therefore the model succeeds visual validation against both recent and historical drill orientation and spacing, as well as current geologic interpretations.

In order to calculate the volume and tonnage of a pit, and therefore calculate waste rock and strip ratio, an initial pit design was then added to the model. The area of this pit is shown in Figure 14-3. The outlines of this pit in cross section are visible in Figures 14-4 through 14-9 . The walls of the pit are restricted to angles 45 degrees or shallower, and the floor is low enough to envelop the majority of the resource. Some portions of the resource considered too deep for economic recovery are omitted from the pit's volume. The ceiling of the pit is the topo layer, therefore the pit model is an enclosed volume, and its tonnage can be calculated from the known density of the local rock.

After the pit wireframe was created and trimmed to topography, all blocks within the volume of the wireframe were flagged as parts of the pit. The resource is now strictly limited to the volumes of the three zones of mineralization, which fall within the pit, and above the redox boundary. At this point, the model is considered complete.

After a final validation, a final resource can be calculated. Each block which has been flagged as 'Indicated', has been flagged as a part of the pit, has been flagged as Oxide, and bears an AuEq value above or equal to 0.005 ounces per ton, is added to the Indicated grade tonnage calculation. The process is repeated for Inferred blocks. The results of this process are summarized in Table 146below:

BB Table 14-6 Longstreet Resource by Zone and Category

Table 14-6: Longstreet Resource by Zone and Category							
Upper Zone	Tonnage	AuEq (opt)	Au (opt)	Ag (opt)	AuEq (oz)	Au (oz)	Ag (oz)
Indicated	5404552	0.0220	0.0148	0.4315	119024	80153	2332127
Inferred	925775	0.0187	0.0102	0.5079	17275	9438	470229
Total	6330326	0.0215	0.0142	0.4427	136299	89590	2802356
Middle Zone							
Indicated	2163947	0.0177	0.0105	0.4376	38404	22622	946882
Inferred	1022084	0.0154	0.0053	0.6056	15745	5429	618964
Total	3186031	0.0170	0.0088	0.4915	54149	28051	1565846
Lower Zone							
Indicated	1106453	0.0140	0.0096	0.2648	15516	10633	292977
Inferred	451789	0.0158	0.0092	0.3957	7118	4139	178752

Total	1558242	0.0145	0.0095	0.3027	22634	14772	471729
All Zones							
Indicated	8674951	0.0199	0.0131	0.4118	172944	113409	3571986
Inferred	2399648	0.0167	0.0079	0.5284	40138	19005	1267945
Total	11074599	0.0192	0.0120	0.4370	213082	132414	4839931

The entirety of the resource calculated in this report is within the oxidized zone, above the redox boundary. By comparison, the Noland report of 2012 found that only 8 of its 230 resource polygons (3.5%) fell entirely below the modeled redox boundary. Preliminary metallurgical testing suggests moderate Au and Ag recoveries may be achieved from some of the sulfide material, especially in a zone of mixed oxide and sulfide. However, to provide a conservative estimate, no known sulfide zones are included in the current resource summary. All tonnage reported here belongs to the oxidized zone.

Although there are historic underground workings within the Main Resource zone at Longstreet, there are no production records available. Underground inspection reveals very small stopes. The mill at the bottom of the canyon has a tailings pile estimated at no more than a few tons to a few tens of tons. Consequently, no 'subtraction' of the historic mining is made to the current resource.

It is the author's opinion that the resource stated here, although originally created at different metals prices and cost parameters, remains valid. The author is not aware of any additional environmental, permitting, legal, title, taxation, socio-economic, marketing, political or other relevant issues which are likely to negatively affect the economic value of the Longstreet project other than the issues already described in this report.

It is the author's understanding that Star Gold intends to commission more detailed economic analyses in the coming months, including a Preliminary Economic Assessment (PEA). Those analyses should either validate the resource presented here or provide an updated resource with current metals prices and costs.

15.0 Mineral Reserve Estimates

Star Gold has not yet completed any mineral reserve estimates for the Longstreet Project.

16.0 Mining Methods

Star Gold has not completed any formal or final mining plans beyond the pit design shown in the resource calculation. However, preliminary planning calls for an open pit mine, with contract mining, and a heap leach recovery, with or without crushing.

17.0 Processing and Recovery Methods

No formal processing or recovery methods have been determined. This section is not applicable.

18.0 Infrastructure

There is currently no established infrastructure at the Longstreet Project. This section is not applicable.

19.0 Market Studies

Star Gold has not completed any formal market studies for Longstreet. This section is not applicable.

20.0 Environmental Studies, Permitting, Plans and Agreements

Star Gold has operated to date under a 'Categorical Exclusion' permit and agreement with the USFS for exploration activities. This permit allows for up to 5 acres of total disturbance. Star has recently submitted an application to the USFS for an Exploration Plan of Operation (PoO), which allows significantly more disturbance. Star intends to expand exploration drilling to new targets, complete production water wells and monitoring water wells, as well as conduct some pre-production activities under this new application. Approval of the PoO is expected in the 4th quarter of 2025.

21.0 Capital and Operating Costs

Star has not completed any formal economic studies or established final operating costs. This section is not applicable.

22.0 Economic Analysis

Star has not completed a formal Preliminary Economic Analysis (PEA) or other economic analyses on the property. This section is not applicable.

23.0 Adjacent Properties

The author is not aware of any adjacent active mining properties within a 15 mile radius of the property. The nearest producing mine is the Round Mountain Mine, some 25 miles to the northwest. Nearby (less than 30 miles) active exploration projects include the Midway (Midway Gold Corp.) in Ralston Valley. There are several recently announced exploration projects in the historic Manhattan and Belmont districts, including Scorpio Gold's programs at Gold Wedge in Manhattan.

24.0 Other Relevant Data and Information

The author is not aware of any other data or information which would add materially to the understanding or authenticity of this report.

25.0 Interpretations and Conclusions

The Longstreet Project and the Round Mountain Mine are located peripherally to the Walker Lane Zone in a region of Tertiary calc-alkalic magmatism and associated epithermal gold /silver mineralization. The property is mainly underlain by rhyolitic welded ash-flow tuffs of the same character and age as are found at the Round Mountain Mine, located approximately 25 miles northwest of the Longstreet Project. Detailed mapping by MinQuest also identified zones of volcaniclastic sediments overlying the tuffs and quartz feldspar intrusions within the tuff.

Hydrothermal alteration resulted in the development of sheeted quartz vein systems and the deposition of gold / silver mineralization along preferred northwest and easterly trends, which is apparent on both the Longstreet Project and at the Round Mountain Mine. On the Longstreet Project limonite, geothite, hematite, manganese oxides, and adularia in quartz veins and in fractures accompany potentially economic oxidized mineralization. Native gold is fine grained and is occasionally noted in limonite pseudomorphs after pyrite

An 'indicated resource' is calculated in this report at 7.7 million tons at an average grade of 0.021 oz/ton AuEq (0.012 oz/ton Au and 0.48 oz/ton Ag), for a contained resource of approximately 165,000 ounces of AuEq (108,000 ounces Au and 3.3 million ounces Ag). These resources were calculated with a cut-off grade of 0.005 opt AuEq. The resource calculation database contains over 300 reverse-circulation-rotary (RC) drill holes plus the 59 completed by Star in 2011-2013. An additional 'inferred resource' containing 4.9 million tons at an average grade of 0.019 oz/ton AuEq has been calculated for this report. The 'inferred resource' contains approximately 92,000 ounces of AuEq metal in addition to the 'indicated resource' This inferred resource is estimated to contain approximately 47,000 ounces of gold and 2.7 million ounces of silver. The author notes that fewer than half of the drill holes within the resource penetrated the entire thickness of oxidized mineralization and bedrock. This sampling bias indicates to the author that the calculated resource reported here very likely underestimates the size and grade of the deposit.

The gold mineralized vein systems trend both northwest and east and both sets dip steeply to vertical and are difficult to intersect with vertical drilling. An optimal drill pattern, as employed by Star uses an azimuth of 191° and a dip of 45-50° to achieve a ‘more’ perpendicular intersection of both vein sets in the same RC hole. Continued implementation of this type of drilling should enhance the grade of the deposit by providing unbiased sampling of the mineralization.

The indicated and inferred resources reported in this report, plus probable extensions of the Main Zone mineralization on the Longstreet Project, represent the foundation for identifying an economic heap leachable gold/ silver deposit. Sufficient preliminary metallurgical test work has been undertaken to indicate that the gold mineralization is recoverable and presents no special problems. Additional potential resides in the other eight gold zones located within 1.25 miles of the Main Zone. All Longstreet target areas (Main, NE Main, West Main, north Slope, North, Spire, Opal Ridge, Red Knob and Cyprus Ridge) have surface sample results that indicate the presence of potentially economic gold / silver mineralization (see Figure 9-1), and as such warrant further exploration. There are also large tracts of unexplored lands located peripheral to the known zones, which should be examined in detail.

The author is of the opinion, in light of the gold / silver discoveries made to date, that further discoveries of potentially economic gold / silver mineralization on the Longstreet Project are possible.

The author is of the further opinion that the resource calculations included in this report, when scrutinized and enhanced with updated costs estimates and metals prices, will support a positive Economic Analysis and remain the basis for an economically viable operation.

26.0 Recommendations

The next phase(s) of work at Longstreet should be designed to push the project toward production. Once the PoO currently under review is approved by the USFS, work can begin on completion of a production water well, and at least one water monitoring well.

A minimal drilling program should be completed to test high priority targets and attempt to enhance the current resource for a subsequent updated resource estimation. Additional drilling within the current resource should target converting 'inferred' to 'indicated' resource, and ultimately lead to calculated 'reserves'.

Engineering studies should be initiated which will guide Star through design of operational parameters and selection of a Contract Miner. These studies may or may not initially take the form of a Preliminary Economic Assessment (PEA) but should be aimed at determining profitability of the project under current costs and metals prices. An updated resource estimation will be a necessary part of these studies.

Once the project is deemed to be economically viable for production, additional permits should be initiated with the USFS, BLM and Nevada Department of Environmental Protection (NDEP) to allow for open pit, heap leach mining on site. The proposed operation and subsequent permit application may or may not trigger the need for an Environmental Impact Statement (EIS). That determination will be made by the BLM and USFS.

27.0 References

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28.0 Reliance on Information provided by the Registrant

The author relied upon a data packet provided by Star Gold and by the previous owner, MinQuest for much of the historical information in this report. Sample results and drilling data were confirmed by examining original assay certificates or reports whenever available.

Drill logs, drill assays and all other parameters utilized for the resource estimations were verified independently by examination of original data whenever possible.

The author believes that all information available and utilized for this report is reliable and valid.

29.0 Date and Signature Page

I, Paul D. Noland, 118 Spring Creek Parkway, Spring Creek, NV, U.S.A., hereby certify:

1. I am a graduate of Lamar University (1971) with a B.Sc. degree in geology, and am a Certified Professional Geologist with certification through AIPG (#11293).

2. I am presently employed as a consulting geologist, independent of Star, MinQuest or any of their subsidiaries.

3. I have been employed in my profession by various mining companies since 1974, and an independent consultant for over 17 years in total Employment with exploration and mining companies has involved positions of Senior Geologist with Inspiration, Noranda, Independence Mining (Jerritt Canyon mine), Barrick Gold (Cortez, NV mine) and Chief Geologist for Yukon-Nevada at their Jerritt Canyon mine. I held the position of VP Exploration for Fiore Gold and Calibre Mining Corp. I have been intimately involved with several precious and base metal discoveries, and at least partly responsible for several others. My consulting practice specializes in project management, project evaluation, exploration planning and targeting, and resource estimation. The majority of my work has involved precious metals deposits, both vein and bulk tonnage types.

4. I have read the definitions of "Qualified Person" set out in NI 43-101 and in SK1300, and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101), (Certified Professional Geologist, #11293 from AIPG, member of Geological Society of Nevada) and past relevant work experience, I fulfill the requirements to be a "Qualified Person" for the purposes of this report.

5. I am responsible for all sections of this report, utilizing in part the data summarized in the References section of this report and provided by Star Gold and previous owners.

6. This certificate applies to the technical report titled *Technical Report and Resource Estimation for the Longstreet Property, Nye County, Nevada,* dated December 8, 2025.

7. I visited Longstreet property on May 17, 2011, May 31, 2011, and February 10 and 11, 2012. I had no prior involvement with the Longstreet Property before these dates. The initial resource estimate was created February 16, 2014, and was reviewed in the weeks prior to the effective date of this report. It is my understanding that no significant or material change to the property has occurred since my last visit to the site.

8. I hold no office with Star Gold Corp. and am therefore independent of all ownership in the Longstreet Project and all its subsidiaries and I am in no position to receive any financial gain nor any other benefit from any success of Star Gold and am employed only as an independent consultant.

9. To the best of my knowledge, information and belief, this report contains all the scientific and technical information that is required to be disclosed to make this technical report not misleading.

10. I consent to the filing of this technical report with any stock exchange and other regulatory authority and any publication by them for regulatory purposes, including

electronic publication in the public company files on their websites accessible by the public. The contents of this report may be summarized in Press Releases.

Paul D. Noland

Dated at Spring Creek, Nevada this 8th day of December 2025

AMERICAN INSTITUTE OF PROFESSIONAL GEOLOGISTS
CERTIFICATE NUMBER
11293
AIPG
PAUL D. NOLAND
CERTIFIED PROFESSIONAL GEOLOGIST

30.0 Appendices

Appendix 1. Claims List

TonopahOffice
101RadarRoad
POBox1111
Tonopah,NV89049
Phone(775)482-8116
Fax(775)482-8111

Office Of Nye County Recorder
Deborah Beatty - Recorder

PahrumpOffice
170NFloydStSte1
Pahrump,NV89060
Phone(775)751-6340
Fax(775)751-6341

Receipt2025-07845

Product	Name	Extended
NOI	Notice of Intent to Hold	$1,716.00
Document # 1056349, Document Info: GREAT BASIN RESOURCES, Document Info: GREAT BASIN RESOURCES, Claims 142		
Total		$1,716.00
Tender (Check)		$1,716.00
Name GREAT BASIN RESOURCES, Check # 1496, Name GREAT BASIN RESOURCES		

8/26/25,1:53PMPSTvwalker

I hereby affirm that this document submitted for recording does not contain a social security number.

Signed
Richard R. Kern, Agent

DOC # 1056349
Official Records Nye County Nevada
Deborah Beatty - Recorder
08/26/2025 01:53:37 PM
Requested By: GREAT BASIN RESOURCES
Recorded By: vw RPTT:$0.00
Recording Fee: $1,716.00
Page 1 of 5

AFTER FILING/RECORDING,
PLEASE RETURN TO:
Great Basin Resources Inc.
5560 Rue St Tropez
Reno, NV 89511

Nye County Recorder
101 Radar Road
P.O. Box 1111
Tonopah, NV 89049

AFFIDAVIT OF PAYMENT OF CLAIM MAINTENANCE AND NOTICE OF INTENTION TO HOLD UNPATENTED MINING CLAIMS

The undersigned being first duly sworn deposes and says:

Great Basin Resources Inc., a Nevada corporation, with offices located at 5560 Rue St Tropez, Reno, NV, 89511, is the owner or authorized agent on behalf of the owner of each of the claims described on Exhibit A attached hereto and incorporated herein ("the Claims").

Great Basin Resources Inc., as owner or as the authorized agent on behalf of the owner of the Claims, intends to hold said Claims from September 2, 2025 until September 2, 2026.

Great Basin Resources Inc., as owner or as the authorized agent on behalf of the owner of the Claims, has paid to the U.S. Department of the Interior - Bureau of Land Management, on or before September 1st, 2025, the annual maintenance fees for the assessment year beginning September 2, 2025 as prescribed in the 1993 Omnibus Budget Reconciliation Act of 1993, Public Law 103-66, for the Claims.

This Affidavit of Payment of Claim Maintenance Fees and Notice of Intention to Hold Unpatented Mining Claims is made and recorded pursuant to NRS 517.230(3).

The recording fee due the Nye County Recorder has been calculated by multiplying each of the 142 claims by $12.00 plus $12.00 per document for a total amount due the Nye County Recorder, enclosed herewith, of $1,716.00.

EXHIBIT A

NYE COUNTY

CLAIM NAME			CLAIMANT'S NAME	NMC NUMBER
Morning Star			Roy Clifford et al	96719
Longstreet	11		Roy Clifford et al	164002
Longstreet	12		Roy Clifford et al	164003
Longstreet	14		Roy Clifford et al	164005
Longstreet	15		Roy Clifford et al	164006
Longstreet	1	A	MinQuest Inc.	799562
Longstreet	2	A	MinQuest Inc.	799563
Longstreet	3	A	MinQuest Inc.	799564
Longstreet	4	A	MinQuest Inc.	836168
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Longstreet	6	A	MinQuest Inc.	799565
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Longstreet	8	A	MinQuest Inc.	799567
Longstreet	8		MinQuest Inc.	836170
Longstreet	9	A	MinQuest Inc.	799568
Longstreet	10		MinQuest Inc.	836171
Longstreet	10	A	MinQuest Inc.	836172
Longstreet	12		MinQuest Inc.	843867
Longstreet	13		MinQuest Inc.	799570
Longstreet	14		MinQuest Inc.	843868
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Longstreet	314	MinQuest Inc.	1116075
Longstreet	315	MinQuest Inc.	1116076
Longstreet	316	MinQuest Inc.	1116077
Longstreet	317	MinQuest Inc.	1116078
		Total Claims	**142**

Dated and signed this 4 day of August, 2025
For Great Basin Resources Inc.

Richard R. Kern, Agent

STATE OF NEVADA)
) SS.
COUNTY OF WASHOE)

Signed and sworn to before me this 4 day of August, 2025, by Richard R. Kern, as agent for Great Basin Resources Inc.

NOTARY PUBLIC

My Commission Expires: 04/01/2026 [SEAL]
Notary Public in and for Washoe Country, Nevada

RAJANDRAKUMAR T PATEL
Notary Public, State of Nevada
Appointment No. 22-2721-02
My Appt. Expires Apr 1, 2026

Appendix 2. Drill Hole Collars and Assay Highlights

STAR GOLD CORP

Summary of Significant Mineralized Intersections in Reverse Circulation Drill Holes

Table 30-1 Reverse Circulation Drilling Record (1984-1997, and 2011-2013)

Star Gold Corp. – Longstreet Au-Ag Project, Nevada

Hole ID	Year	UTM Coordinates		Elevation (ft.)	Azimuth (⁰)	Inclination (⁰)	Length (ft.)	Intersection (ft.) From	Intersection (ft.) To	Interval (ft.)	oz/ton Au	oz/ton Ag
LRH-1	1984	525225E	4247433N	7,613	0	-90	115	0	115	115	0.055	0.62
LRH-2	1984	525249E	4247449N	7,620	0	-90	170	10	170	160	0.058	0.81
LRH-3	1984	525278E	4247452N	7,626	0	-90	180	0	180	180	0.027	0.54
LRH-4	1984	525355E	4247420E	7,638	0	-90	75	0	75	75	0.035	0.90
LRH-5	1984	525323E	4247440N	7,637	0	-90	200	0	200	200	0.035	0.46
LRH-6	1984	525373E	4247425N	7,612	0	-90	40	0	40	40	0.032	0.62
LRH-7	1984	525353E	4247447N	7,609	0	-90	140	0	140	140	0.019	0.35
LRH-8	1984	525328E	4247458N	7,608	0	-90	215	0	215	215	0.016	0.52
LRH-9	1984	525388E	4247446N	7,575	0	-90	70	0	70	70	0.024	0.75
LRH-10	1984	525367E	4247487N	7,545	0	-90	200	0	200	200	0.017	0.64
LRH-11	1984	525333E	4247502N	7,535	0	-90	245	0	30	30	0.010	0.10
LRH-11	1984	525333E	4247502N	7,535	0	-90	245	160	245	85	0.013	0.42
LRH-12	1984	525195E	4247454N	7,543	0	-90	100	0	100	100	0.020	0.15
LRH-13	1984	525197E	4247479N	7,526	0	-90	105	15	105	90	0.019	0.54
LRH-14	1984	525206E	4247492N	7,526	0	-90	180	10	70	60	0.015	0.31
LRH-14	1984	525206E	4247492N	7,526	0	-90	180	110	165	55	0.019	0.34
LRH-15	1984	525259E	4247493E	7,554	0	-90	235	0	225	225	0.020	0.33
LRH-16	1984	525295E	4247504N	7,736	0	-90	285	0	10	10	0.006	0.07
LRH-16	1984	525295E	4247504N	7,736	0	-90	285	135	285	150	0.012	0.52
LRH-17	1984	525398E	4247514N	7,484	0	-90	240	5	50	45	0.005	0.20
LRH-17	1984	525398E	4247514N	7,484	0	-90	204	120	190	70	0.006	0.48
LRH-17	1984	525398E	4247514N	7,484	0	-90	240	205	225	20	0.010	0.81
LRH-18	1984	525337E	4247431N	7,642	0	-90	115	0	115	115	0.011	0.34
LRH-19	1984	525304E	4247449N	7,630	0	-90	115	0	115	115	0.033	0.77

Table 30-1 Reverse Circulation Drilling Record (1984-1997, and 2011-2013)

Star Gold Corp. – Longstreet Au-Ag Project, Nevada

Hole ID	Year	UTM Coordinates		Elevation (ft.)	Azimuth (°)	Inclination (°)	Length (ft.)	Intersection (ft.)		Interval (ft.)	oz/ton Au	oz/ton Ag
								From	To			
LRH-20	1984	525265E	4247452N	7,623	0	-90	200	0	200	200	0.024	0.41
LRH-21	1984	525364E	4247436N	7,612	0	-90	100	0	55	55	0.028	0.62
LRH-22	1984	525481E	4247555N	7,359	0	-90	280	0	35	35	0.014	0.09
LRH-22	1984	525481E	4247555N	7,359	0	-90	280	240	250	10	0.011	1.74
LRH-23	1984	525445E	4247528N	7,427	0	-90	245	No significant values				
LRH-24	1984	525341E	4247663N	7,274	0	-90	105	0	15	15	0,011	0.38
LRH-25	1984	525287E	4247378N	7,721	0	-90	145	0	145	145	0.007	0.18
LRH-26	1984	525315E	4247373N	7,722	0	-90	175	0	15	15	0.009	0.30
LRH-26	1984	525315E	4247373N	7,722	0	-90	175	50	175	125	0.008	0.58
LRH-27	1984	525131E	4247524N	7,395	0	-90	185	0	155	155	0.008	0.09
LRH-28	1984	525146E	4247541N	7,403	0	-90	145	0	105	105	0.009	0.25
LRH-28	1984	525146E	4247541N	7,403	0	-90	145	115	130	15	0.006	0.11
LRH-29	1984	525266E	4247565N	7,446	0	-90	365	0	85	85	0.006	0.14
LRH-29	1984	525266E	4247565N	7,446	0	-90	365	210	315	105	0.020	0.49
LRH-30	1984	525293E	4247567N	7,439	0	-90	165	0	30	30	0.013	0.25
LRH-31	1984	525404E	4247493N	7,504	0	-90	180	100	165	65	0.012	0.45
LRH-32	1984	525367E	4247518N	7,497	0	-90	300	0	20	20	0.007	0.18
LRH-32	1984	525367E	4247518N	7,497	0	-90	300	185	195	10	0.011	0.17
LRH-33	1984	525170E	4247494N	7,474	0	-90	200	0	130	130	0.011	0.24
LRH-33	1984	525170E	4247494N	7,474	0	-90	200	180	200	20	0.007	0.07
LRH-34	1984	525190E	4247525N	7,471	0	-90	245	0	215	215	0.016	0.27
LRH-35	1984	525220E	4247534N	7,483	0	-90	245	20	95	75	0.006	0.20
LRH-35	1984	525220E	4247534N	7,483	0	-90	245	110	120	10	0.006	0.04
LRH-35	1984	525220E	4247534N	7,483	0	-90	245	135	245	110	0.023	0.37
LRH-36	1984	525275E	4247535N	7,489	0	-90	165	0	20	20	0.019	0.43
LRH-37	1984	525515E	4247433N	7,401	0	-90	180	0	20	20	0.008	0.26
LRH-37	1984	525515E	4247433N	7,401	0	-90	180	50	110	55	0.007	0.19
LRH-38	1984	525435E	4247542N	7,422	0	-90	100	No significant values				
LRH-39	1984	525417E	4247562N	7,410	0	-90	165	No significant values				

Table 30-1 Reverse Circulation Drilling Record (1984-1997, and 2011-2013)

Star Gold Corp. – Longstreet Au-Ag Project, Nevada

Hole ID	Year	UTM Coordinates		Elevation (ft.)	Azimuth (°)	Inclination (°)	Length (ft.)	Intersection (ft.) From	To	Interval (ft.)	oz/ton Au	oz/ton Ag
LRH-40	1984	525486E	4247081N	7,710	0	-90	250	No significant values				
LRH-41	1984	525396E	4247073N	7,718	0	-90	250	20	80	60	0.005	0.01
LRH-41	1984	525396E	4247073N	7,718	0	-90	250	130	160	30	0.005	0.07
LRH-41	1984	525396E	4247073N	7,718	0	-90	250	190	220	30	0.005	0.03
LRH-42	1984	525254E	4247273N	7,765	0	-90	160	60	80	20	0.005	0.06
LRH-42	1984	525254E	4247273N	7,765	0	-90	160	130	155	25	0.006	0.10
LRH-43	1984	525330E	4247318N	7,763	0	-90	160	25	140	115	0.010	0.21
LRH-44	1984	525414E	4247232N	7,727	0	-90	100	15	30	15	0.004	0.007
LRH-44	1984	525414E	4247232N	7,727	0	-90	100	85	95	10	0.007	0.01
LRH-45	1984	525328E	4247415N	7,668	0	-90	60	0	60	60	0.023	0.71
LRH-46	1984	525208E	4247302N	7,681	0	-90	155	0	20	20	0.007	0.20
LRH-46	1984	525208E	4247302N	7,681	0	-90	155	90	140	50	0.023	0.17
LRH-47	1984	525218E	4247415N	7,618	0	-90	250	0	115	115	0.011	0.17
LRH-47	1984	525218E	4247415N	7,618	0	-90	250	195	230	35	0.007	0.36
LRH-48	1984	525241E	4247412N	7,651	0	-90	235	0	95	95	0.020	0.36
LRH-48	1984	525241E	4247412N	7,651	0	-90	235	155	200	45	0.009	0.19
LRH-49	1984	525310E	4247421N	7,667	0	-90	255	0	175	175	0.016	0.52
LRH-49	1984	525310E	4247421N	7,667	0	-90	255	240	255	15	0.005	0.19
LRH-50	1984	525362E	4247439N	7,610	0	-90	150	0	65	65	0.009	2.64
LRH-51	1984	525236E	4247444N	7,615	0	-90	300	0	250	250	0.018	0.29
LRH-52	1984	525131E	4247319N	7,531	0	-90	150	No significant values				
LRH-53	1984	525226E	4247433N	7,614	0	-90	200	0	120	120	0.027	0.44
LRH-53	1984	525226E	4247433N	7,614	0	-90	200	175	185	10	0.005	0.31
LRH-54	1984	525321E	4247441N	7,637	0	-90	`180	0	125	125	0.011	0.58
LRH-55	1984	525366E	4247402N	7,641	0	-90	150	0	20	20	0.007	0.34
LRH-56	1984	525248E	4247427N	7,644	0	-90	200	5	30	25	0.010	0.18
LRH-56	1984	525248E	4247427N	7,644	0	-90	200	65	120	55	0.029	0.41
LRH-57	1984	525233E	4247391N	7,660	0	-90	150	0	105	105	0.012	0.15
LRH-57	1984	525233E	4247391N	7,660	0	-90	150	135	150	15	0.013	0.24

Table 30-1 Reverse Circulation Drilling Record (1984-1997, and 2011-2013)

Star Gold Corp. – Longstreet Au-Ag Project, Nevada

Hole ID	Year	UTM Coordinates		Elevation (ft.)	Azimuth (°)	Inclination (°)	Length (ft.)	Intersection (ft.)		Interval (ft.)	oz/ton Au	oz/ton Ag
								From	To			
LRH-83	1984	525339E	4247409N	7,666	0	-90	200	0	180	180	0.010	0.41
LRH-84	1984	525328E	4247362N	7,726	0	-90	50	0	40	40	0.009	0.16
LRH-85	1984	525328E	4247360N	7,729	0	-90	150	0	20	20	0.012	0.28
LRH-85	1984	525328E	4247360N	7,729	0	-90	150	50	60	10	0.007	0.35
LRH-85	1984	525328E	4247360N	7,729	0	-90	150	85	100	15	0.008	0.49
LRH-86	1984	525301E	4247376N	7,725	0	-90	200	0	35	35	0.011	0.68
LRH-86	1984	525301E	4247376N	7,725	0	-90	200	90	100	10	0.005	0.41
LRH-86	1984	525301E	4247376N	7,725	0	-90	200	165	200	35	0.006	0.46
LRH-87	1984	525327E	4247267N	7,771	0	-90	100	10	55	45	0.013	0.28
LRH-88	1984	525329E	4247283N	7,766	0	-90	100	20	100	80	0.028	0.54
LRH-89	1984	525320E	4247338N	7,765	0	-90	150	0	90	80	0.004	0.18
LRH-89	1984	525320E	4247338N	7,765	0	-90	150	140	150	10	0.004	0.20
LRH-90	1984	525292E	4247348N	7,758	0	-90	180	0	105	105	0.019	0.29
LRH-90	1984	525292E	4247348N	7,758	0	-90	180	140	170	30	0.052	0.85
LRH-91	1984	525281E	4247336N	7,754	0	-90	150	0	150	150	0.025	0.75
LRH-92	1984	525272E	4247320N	7,751	0	-90	150	0	110	110	0.010	0.31
LRH-93	1984	525252E	4247301N	7,741	0	-90	150	40	55	15	0.006	0.09
LRH-93	1984	525252E	4247301N	7,741	0	-90	150	100	130	30	0.015	0.24
LRH-94	1984	525240E	4247287N	7,733	0	-90	100	35	50	15	0.024	0.07
LRH-95	1984	525270E	4247284N	7,780	0	-90	140	0	15	15	0.004	0.11
LRH-95	1984	525270E	4247284N	7,780	0	-90	140	55	70	15	0.010	0.15
LRH-95	1984	525270E	4247284N	7,780	0	-90	140	100	115	15	0.005	0.47
LRH-96	1984	525279E	4247248N	7,806	0	-90	150	10	40	30	0.006	0.09
LRH-97	1984	525271E	4247233N	7,808	0	-90	145	30	60	30	0.02	0.32
LRH-98	1984	525291E	4247230N	7,804	0	-90	160	50	70	20	0.043	0.42
LRH-98	1984	525291E	4247230N	7,804	0	-90	160	110	125	15	0.013	0.04
LRH-99	1984	525301E	4247194N	7,806	0	-90	150	90	100	10	0.006	0.04
LRH-99	1984	525301E	4247194N	7,806	0	-90	150	140	150	10	0.005	0.02
LRH-100	1984	525307E	4247278N	7,793	0	-90	150	0	150	150	0.009	0.18

Table 30-1 Reverse Circulation Drilling Record (1984-1997, and 2011-2013)

Star Gold Corp. – Longstreet Au-Ag Project, Nevada

Hole ID	Year	UTM Coordinates		Elevation (ft.)	Azimuth (°)	Inclination (°)	Length (ft.)	Intersection (ft.) From	Intersection (ft.) To	Interval (ft.)	oz/ton Au	oz/ton Ag
LRH-101	1984	525306E	4247259N	7,795	0	-90	150	0	150	150	0.006	0.19
LRH-102	1984	525314E	4247235N	7,788	0	-90	160	0	160	160	0.008	0.29
LRH-103	1984	525273E	4247303N	7,766	0	-90	150	0	150	150	0.005	0.28
LRH-104	1984	525306E	4247350N	7,759	0	-90	150	0	25	25	0.010	0.31
LRH-104	1984	525306E	4247350N	7,759	0	-90	150	70	80	10	0.006	0.67
LRH-104	1984	525306E	4247350N	7,759	0	-90	150	90	105	15	0.005	0.29
LRH-104	1984	525306E	4247350N	7,759	0	-90	150	130	150	20	0.006	0.70
LRH-105	1984	525329E	4247326N	7,762	0	-90	150	85	150	65	0.003	0.15
LRH-106	1984	525330E	4247297N	7,766	0	-90	150	15	150	135	0.024	0.57
LRH-107	1984	525274E	4247376N	7,716	0	-90	200	0	200	200	0.009	0.32
LRH-108	1984	525263E	4247363N	7,718	0	-90	150	0	130	130	0.033	0.25
LRH-109	1984	525254E	4247348N	7,717	0	-90	150	0	45	45	0.013	0.34
LRH-110	1984	525241E	4247330N	7,710	0	-90	160	0	80	80	0.008	0.22
LRH-111	1984	525230E	4247310N	7,706	0	-90	150	No significant values				
LRH-112	1984	525226E	4247302N	7,705	0	-90	60	0	35	35	0.004	0.67
LRH-113	1984	525221E	4247290N	7,706	0	-90	100	0	75	75	0.008	0.20
LRH-114	1984	525214E	4247267N	7,711	0	-90	100	65	85	20	0.018	0.06
LRH-115	1984	525211E	4247258N	7,714	0	-90	100	75	100	25	0.012	0.06
LRH-116	1984	525200E	4247244N	7,709	0	-90	60	45	55	10	0.006	0.06
LRH-117	1984	525266E	4247426N	7,657	0	-90	200	0	130	130	0.012	0.35
LRH-118	1984	525322E	4247402N	7,686	0	-90	150	0	55	55	0.017	0.71
LRH-119	1984	525342E	4247393N	7,680	0	-90	150	45	65	20	0.007	0.38
LRH-119	1984	525342E	4247393N	7,680	0	-90	150	100	120	20	0.005	0.85
LRH-120	1984	525164E	4247414N	7,524	0	-90	150	0	15	15	0.010	0.17
LRH-120	1984	525164E	4247414N	7,524	0	-90	150	60	70	10	0.007	0.13
LRH-121	1984	525175E	4247442N	7,521	0	-90	150	0	80	80	0.008	0.12
LRH-121	1984	525175E	4247442N	7,521	0	-90	150	130	150	20	0.009	0.78
LRH-122	1984	525193E	4247470N	7,526	0	-90	150	0	150	150	0.011	0.33
LRH-123	1984	525201E	4247487N	7,524	0	-90	200	0	200	200	0.018	0.23

Table 30-1 Reverse Circulation Drilling Record (1984-1997, and 2011-2013)

Star Gold Corp. – Longstreet Au-Ag Project, Nevada

Hole ID	Year	UTM Coordinates		Elevation (ft.)	Azimuth (°)	Inclination (°)	Length (ft.)	Intersection (ft.) From	To	Interval (ft.)	oz/ton Au	oz/ton Ag
LRH-124	1984	525159E	4247476N	7,472	0	-90	200	0	160	160	0.008	0,61
LRH-125	1984	525175E	4247506N	7,472	0	-90	260	0	155	155	0.007	0.65
LRH-126	1984	525202E	4247530N	7,476	0	-90	260	60	205	145	0.053	0.70
LRH-127	1984	525346E	4247334N	7,725	0	-90	160	145	160	15	0.007	0.26
LRH-128	1984	525365E	4247284N	7,715	0	-90	160	No significant values				
LRH-129	1984	525355E	4247310N	7,720	0	-90	240	65	100	35	0.007	0.17
LRH-129	1984	525355E	4247310N	7,720	0	-90	240	170	210	40	0.009	0.55
LRH-130	1984	525377E	4247303N	7,688	0	-90	360	185	240	55	0.006	1.03
LRH-131	1984	525377E	4247331N	7,674	0	-90	260	165	180	15	0.008	0.19
LRH-131	1984	525377E	4247331N	7,674	0	-90	260	245	260	15	0.011	2.29
LRH-132	1984	525374E	4247361N	7,657	0	-90	260	No significant values				
LRH-133	1984	525369E	4247385N	7,649	0	-90	200	0	20	20	0.006	0.24
LRH-133	1984	525369E	4247385N	7,649	0	-90	200	190	200	10	0.013	0.24
LRH-134	1984	525550E	4247295N	7,560	0	-90	125	No significant values				
LRH-135	1984	525476E	4247303N	7,592	0	-90	50	No significant values				
LRH-136	1984	525407E	4247349N	7,605	0	-90	200	No significant values				
LRH-137	1984	525349E	4247498N	7,537	0	-90	240	95	215	120	0.008	0.46
LRH-138	1984	525375E	4247481N	7,548	0	-90	180	0	15	15	0.006	0.12
LRH-138	1984	525375E	4247481N	7,548	0	-90	180	95	160	55	0.012	0.93
LRH-139	1984	525377E	4247460N	7,573	0	-90	150	0	85	85	0.011	0.37
LRH-140	1984	525316E	4247503N	7,536	0	-90	280	0	30	30	0.025	0.85
LRH-140	1984	525316E	4247503N	7,536	0	-90	280	110	165	55	0.005	0.80
LRH-140	1984	525316E	4247503N	7,536	0	-90	280	190	270	80	0.027	2.00
LRH-141	1984	525378E	4247131N	7,774	0	-90	140	60	75	15	0.004	0.03
LRH-141	1984	525378E	4247131N	7,774	0	-90	140	90	115	25	0.009	0.09
LRH-141	1984	525378E	4247131N	7,774	0	-90	140	130	140	10	0.005	0.06
LRH-142	1984	525352E	4247241N	7,764	0	-90	150	135	150	15	0.029	0.17
LRH-143	1984	525336E	4247253N	7,767	0	-90	150	115	145	30	0.020	0.05
LRH-144	1984	525244E	4247494N	7,550	0	-90	270	0	25	25	0.009	0.18

Table 30-1 Reverse Circulation Drilling Record (1984-1997, and 2011-2013)

Star Gold Corp. – Longstreet Au-Ag Project, Nevada

Hole ID	Year	UTM Coordinates		Elevation (ft.)	Azimuth (°)	Inclination (°)	Length (ft.)	Intersection (ft.) From	To	Interval (ft.)	oz/ton Au	oz/ton Ag
LRH-144	1984	525244E	4247494N	7,550	0	-90	270	115	210	95	0.019	0.30
LRH-145	1984	525223E	4247493N	7,540	0	-90	220	0	185	185	0.022	0.42
LRH-145	1984	525223E	4247493N	7,540	0	-90	220	210	220	10	0.016	0.16
LRH-146	1984	525431E	4247434N	7,514	0	-90	100	No significant values				
LRH-147	1984	525457E	4247397N	7,494	0	-90	100	No significant values				
LRH-148	1984	525482E	4247454N	7,415	0	-90	100	No significant values				
LRH-149	1984	525507E	4247426N	7,414	0	-90	100	No significant values				
LRH-150	1984	525553E	4247409N	7,426	0	-90	100	No significant values				
LRH-151	1984	525591E	4247522N	7,276	0	-90	100	No significant values				
LRH-152	1984	525246E	4247730N	7,250	0	-90	100	No significant values				
LRH-153	1984	525288E	4247303N	7,784	195	-60	200	0	95	95	0.014	0.64
LRH-153	1984	525288E	4247303N	7,784	195	-60	200	160	200	40	0.009	0.11
LRH-154	1984	525284E	4247277N	7,797	0	-90	160	0	60	60	0.014	0.74
LRH-155	1984	525288E	4247234N	7,806	0	-90	100	5	35	30	0.020	0.24
LRH-156	1984	525298E	4247320N	7,782	225	-60	200	0	200	200	0.030	0.44
LRH-157	1984	525280E	4247316N	7,762	250	-60	200	0	200	200	0.028	0.49
LRH-158	1984	525316E	4247297N	7,790	202	-60	160	0	145	145	0.013	0.23
LRH-159	1984	525284E	4247282N	7,797	225	-60	150	0	40	40	0.011	0.68
LRH-159	1984	525284E	4247282N	7,797	225	-60	150	60	75	15	0.004	0.07
LRH-160	1984	525277E	4247327N	7,754	207	-60	150	0	35	35	0.014	0.40
LRH-160	1984	525277E	4247327N	7,754	207	-60	150	75	140	65	0.006	0.32
LRH-161	1984	525283E	4247340N	7,754	220	-60	140	0	120	120	0.025	0.31
LRH-162	1984	525289E	4247348N	7,755	255	-60	135	0	135	135	0.040	0.45
LRH-163	1984	525305E	4247349N	7,761	296	-60	150	0	30	30	0.019	0.27
LRH-163	1984	525305E	4247349N	7,761	296	-60	150	65	135	70	0.016	0.18
LRH-164	1984	525269E	4247316N	7,750	220	-60	150	0	55	55	0.008	0.49
LRH-164	1984	525269E	4247316N	7,750	220	-60	150	95	130	35	0.004	0.16
LRH-165	1984	525305E	4247281N	7,797	228	-60	150	15	115	100	0.015	0.30
LRH-166	1984	525302E	4247265N	7,797	222	-60	150	0	55	55	0.011	0.38

Table 30-1 Reverse Circulation Drilling Record (1984-1997, and 2011-2013)

Star Gold Corp. – Longstreet Au-Ag Project, Nevada

Hole ID	Year	UTM Coordinates		Elevation (ft.)	Azimuth (°)	Inclination (°)	Length (ft.)	Intersection (ft.)		Interval (ft.)	oz/ton Au	oz/ton Ag
								From	To			
LRH-166	1984	525302E	4247265N	7,797	222	-60	150	95	130	35	0.008	0.15
LRH-167	1984	525309E	4247235N	7,792	233	-60	150	80	110	30	0.116	0.85
LRH-168	1984	525295E	4247245N	7,803	213	-60	150	50	65	15	0.006	0.10
LRH-168	1984	525295E	4247245N	7,803	213	-60	150	115	130	15	0.018	0.05
LRH-169	1984	525312E	4247221N	7,792	242	-60	150	90	100	10	0.052	0.56
LRH-170	1984	525277E	4247242N	7,807	222	-60	150	45	65	20	0.008	0.15
LRH-170	1984	525277E	4247242N	7,807	222	-60	150	140	150	10	0.006	0.25
LRH-171	1984	525268E	4247257N	7,793	0	-90	100	60	90	30	0.009	0.06
LRH-172	1984	525318E	4247340N	7,765	245	-60	140	0	30	30	0.014	0.37
LRH-172	1984	525318E	4247340N	7,765	245	-60	140	60	120	60	0.010	0.35
LRH-173	1984	525280E	4247219N	7,810	0	-90	120	70	85	15	0.046	0.08
LRH-174	1984	525341E	4247259N	7,759	237	-60	150	35	150	115	0.013	0.15
LRH-175	1984	525322E	4247366N	7,728	259	-60	150	0	35	35	0.008	0.15
LRH-176	1984	525296E	4247375N	7,727	260	-60	200	75	200	125	0.012	0.29
LRH-177	1984	525283E	4247376N	7,722	254	-60	150	0	150	150	0.009	0.21
LRH-178	1984	525264E	4247363N	7,719	210	-60	160	0	75	75	0.025	0.30
LRH-178	1984	525264E	4247363N	7,719	210	-60	160	150	160	10	0.006	0.34
LRH-179	1984	525251E	4247344N	7,716	214	-60	160	0	60	60	0.018	0.34
LRH-179	1984	525251E	4247344N	7,716	214	-60	160	75	85	10	0.008	0.24
LRH-179	1984	525251E	4247344N	7,716	214	-60	160	135	145	10	0.009	0.19
LRH-180	1984	525274E	4247402N	7,690	261	-60	160	0	160	160	0.015	0.39
LRH-181	1984	525261E	4247395N	7,688	238	-60	140	0	100	100	0.007	0.26
LRH-182	1984	525246E	4247384N	7,683	228	-60	160	0	160	160	0.008	0.14
LRH-183	1984	525237E	4247369N	7,682	217	-60	160	0	105	105	0.014	0.15
LRH-184	1984	525226E	4247354N	7,677	203	-60	160	0	15	15	0.006	0.12
LRH-184	1984	525226E	4247354N	7,677	203	-60	160	85	100	15	0.013	0.11
LRH-184	1984	525226E	4247354N	7,677	203	-60	160	150	160	10	0.010	0.17
LRH-185	1984	525219E	4247340N	7,673	205	-60	160	15	65	50	0.007	0.26
LRH-185	1984	525219E	4247340N	7,673	205	-60	160	140	160	20	0.009	0.06

Table 30-1 Reverse Circulation Drilling Record (1984-1997, and 2011-2013)

Star Gold Corp. – Longstreet Au-Ag Project, Nevada

Hole ID	Year	UTM Coordinates		Elevation (ft.)	Azimuth (°)	Inclination (°)	Length (ft.)	Intersection (ft.)		Interval (ft.)	oz/ton Au	oz/ton Ag
								From	To			
LRH-186	1984	525214E	4247328N	7,674	199	-60	100	0	60	60	0.007	0.18
LRH-187	1984	525232E	4247360N	7,681	207	-60	100	0	50	50	0.006	0.09
LRH-188	1984	525210E	4247305N	7,682	199	-60	100	0	25	25	0.007	0.44
LRH-188	1984	525210E	4247305N	2,682	199	-60	100	60	80	20	0.005	0.07
LRH-189	1984	525203E	4247295N	7,677	190	-60	100	20	100	80	0.024	0.11
LRH-190	1984	525236E	4247395N	7,660	200	-60	100	0	60	60	0.010	0.19
LRH-191	1984	525241E	4247410N	7,653	197	-60	160	0	105	105	0.018	0.42
LRH-191	1984	525241E	4247410N	7,653	197	-60	160	130	140	10	0.006	0.03
LRH-192	1984	525244E	4247421N	7,646	241	-60	150	0	150	150	0.014	0.34
LRH-193	1984	525253E	4247425N	7,649	270	-60	100	0	90	90	0.008	0.17
LRH-194	1984	525339E	4247424N	7,649	268	-60	160	0	95	95	0.049	1.23
LRH-195	1984	525282E	4247453N	7,625	250	-60	240	0	240	240	0.025	0.33
LRH-196	1984	525257E	4247450N	7,622	258	-60	200	0	200	200	0.020	0.31
LRH-197	1984	525229E	4247438N	7,613	227	-60	160	0	100	100	0.043	0.60
LRH-197	1984	525229E	4247438N	7,613	227	-60	160	135	150	15	0.008	0.19
LRH-198	1984	525224E	4247429N	7,616	205	-60	160	0	115	115	0.011	0.27
LRH-199	1984	525220E	4247415N	7,621	195	-60	100	0	90	90	0.012	0.14
LRH-200	1984	525216E	4247401N	7,626	200	-60	100	0	100	100	0.009	0.17
LRH-201	1984	525489E	4247621N	7,304	0	-90	105	No significant values				
LRH-202	1984	525528E	4247586N	7,295	0	-90	150	No significant values				
LRH-203	1984	525554E	4247558N	7,268	0	-90	140	No significant values				
LRH-204	1984	525081E	4247409N	7,394	0	-90	150	No significant values				
LRH-205	1984	525095E	4247438N	7,395	0	-90	105	0	25	25	0.009	0.17
LRH-206	1984	525109E	4247462N	7,403	0	-90	105	No significant values				
LRH-207	1984	525115E	4247492N	7,392	0	-90	105	0	10	10	0.007	0.21
LRH-208	1984	525121E	4247507N	7,391	0	-90	105	No significant values				
LRH-209	1984	525163E	4247552N	7,411	0	-90	305	0	10	10	0.006	0.16
LRH-209	1984	525163E	4247552N	7,411	0	-90	305	20	30	10	0.007	0.33
LRH-209	1984	525163E	4247552N	7,411	0	-90	305	60	70	10	0.009	0.13

Table 30-1 Reverse Circulation Drilling Record (1984-1997, and 2011-2013)

Star Gold Corp. – Longstreet Au-Ag Project, Nevada

Hole ID	Year	UTM Coordinates		Elevation (ft.)	Azimuth (°)	Inclination (°)	Length (ft.)	Intersection (ft.) From	To	Interval (ft.)	oz/ton Au	oz/ton Ag
LRH-209	1984	525163E	4247552N	7,411	0	-90	305	95	115	20	0.007	0.07
LRH-209	1984	525163E	4247552N	7,411	0	-90	305	155	185	30	0.011	0.21
LRH-210	1984	525190E	4247565N	7,423	0	-90	345	0	110	110	0.009	0.22
LRH-210	1984	525190E	4247565N	7,427	0	-90	345	200	220	20	0.012	0.12
LRH-210	1984	525190E	4247565N	7,423	0	-90	345	240	345	105	0.007	0.09
LRH-211	1984	525207E	4247570N	7,429	0	-90	355	0	175	175	0.025	0.26
LRH-211	1984	525207E	4247570N	7,429	0	-90	355	215	295	80	0.012	0.15
LRH-211	1984	525207E	4247570N	7,429	0	-90	355	340	355	15	0.007	0.09
LRH-212	1984	525237E	4247568N	7,441	0	-90	215	0	95	95	0.010	0.16
LRH-213	1984	525243E	4247536N	7,486	0	-90	205	0	205	205	0.008	0.24
LRH-214	1984	525156E	4247467N	7,473	0	-90	165	0	15	15	0.011	0.20
LRH-214	1984	525156E	4247467N	7,473	0	-90	165	40	60	20	0.019	0.50
LRH-214	1984	525156E	4247467N	7,473	0	-90	165	145	165	20	0.011	0.53
LRH-215	1984	525149E	4247447N	7,475	0	-90	105	55	65	10	0.031	0.69
LRH-216	1984	525137E	4247417N	7,476	0	-90	105	0	35	35	0.007	0.19
LRH-217	1984	525133E	4247401N	7,479	0	-90	105	0	30	30	0.023	0.28
LRH-218	1984	525128E	4247386N	7,480	0	-90	80	0	15	15	0.006	0.20
LRH-219	1984	525207E	4247383N	7,630	210	-60	100	0	55	55	0.011	0.18
LRH-220	1984	525201E	4247371N	7,630	210	-60	100	0	45	45	0.036	0.19
LRH-220	1984	525201E	4247371N	7,630	210	-60	100	85	95	10	0.018	0.22
LRH-221	1984	525195E	4247358N	7,628	210	-60	100	0	15	15	0.008	0.11
LRH-221	1984	525195E	4247358N	7,628	210	-60	100	65	100	35	0.008	0.19
LRH-222	1984	525221E	4247594N	7,398	255	-60	160	0	35	35	0.009	0.11
LRH-222	1984	525221E	4247594N	7,398	255	-60	160	120	140	20	0.007	0.20
LRH-223	1984	525203E	4247590N	7,398	246	-60	215	0	25	25	0.011	0.22
LRH-223	1984	525203E	4247590N	7,398	246	-60	215	90	215	125	0.010	0.09
LRH-224	1984	525189E	4247582N	7,399	235	-60	160	0	110	110	0.009	0.18
LRH-225	1984	525176E	4247572N	7,401	230	-60	155	0	120	120	0.006	0.15
LRH-226	1984	525163E	4247596N	7,358	246	-60	135	10	30	20	0.008	0.11

Table 30-1 Reverse Circulation Drilling Record (1984-1997, and 2011-2013)

Star Gold Corp. – Longstreet Au-Ag Project, Nevada

Hole ID	Year	UTM Coordinates		Elevation (ft.)	Azimuth (°)	Inclination (°)	Length (ft.)	Intersection (ft.)		Interval (ft.)	oz/ton Au	oz/ton Ag
								From	To			
LRH-226	1984	525163E	4247596N	7,358	246	-60	135	70	135	65	0.009	0.08
LRH-227	1984	525101E	4247530N	7,337	205	-60	120	0	10	10	0.005	0.09
LRH-228	1984	525130E	4247571N	7,348	214	-60	140	No significant values				
LRH-229	1984	525150E	4247587N	7,355	242	-60	130	0	95	95	0.007	0.19
LRH-230	1984	525187E	4247602N	7,368	241	-60	200	0	130	130	0.012	0.17
LRH-230	1984	525187E	4247602N	7,368	241	-60	200	170	180	10	0.006	0.05
LRH-231	1984	525206E	4247609N	7,372	255	-60	200	140	200	60	0.016	0.10
LRH-232	1984	525112E	4247617N	7,274	218	-60	90	0	10	10	0.009	0.18
LRH-233	1984	525125E	4247634N	7,271	210	-60	155	5	15	10	0.005	0.12
LRH-234	1984	525148E	4247647N	7,277	218	-60	200	0	15	15	0.008	0.12
LRH-235	1984	525165E	4247650N	7,286	210	-60	100	No significant values				
LRH-236	1984	525103E	525103N	7,277	240	-60	160	0	20	20	0.007	0.20
LRH-237	1984	525318E	4247520N	7,509	241	-60	300	0	30	30	0.016	0.51
LRH-237	1984	525318E	4247520N	7,509	241	-60	300	130	175	45	0.014	0.34
LRH-237	1984	525318E	4247520N	7,509	241	-60	300	215	280	65	0.018	1.29
LRH-238	1984	525271E	4247520N	7,510	0	-90	300	95	120	25	0.040	0.90
LRH-238	1984	525271E	4247520N	7,510	0	-90	300	185	270	85	0.009	0.51
LRH-239	1984	525228E	4247516N	7,512	0	-90	260	0	50	50	0.007	0.08
LRH-239	1984	525228E	4247516N	7,512	0	-90	260	90	200	110	0.021	0.47
LRH-240	1984	525194E	4247504N	7,498	0	-90	140	45	130	85	0.012	1.51
LRH-241	1984	525250E	4247517N	7,514	254	-60	240	0	50	50	0.005	0.13
LRH-241	1984	525250E	4247517N	7,514	254	-60	240	125	235	110	0.017	0.49
LRH-242	1984	525295E	4247521N	7,509	216	-60	300	185	300	115	0.032	1.36
LRH-243	1984	525325E	4247458N	7,610	0	-90	232	22	176	152	0.015	0.54
LRH-243	1984	525325E	4247458N	7,610	0	-90	232	190	228	38	0.006	0.36
LRH-244	1984	525363E	4247438N	7,611	0	-90	78	0	64	64	0.029	0.84
LRH-245	1984	525336E	4247431	7,642	0	-90	110	0	110	110	0.008	0.32
LRH-246	1984	525350E	4247447N	7,612	0	-90	115	0	100	100	0.030	0.19
LRH-247	1984	525324E	4247439N	7,638	0	-90	162	0	42	42	0.013	0.14

Table 30-1 Reverse Circulation Drilling Record (1984-1997, and 2011-2013)

Star Gold Corp. – Longstreet Au-Ag Project, Nevada

Hole ID	Year	UTM Coordinates		Elevation (ft.)	Azimuth (°)	Inclination (°)	Length (ft.)	Intersection (ft.) From	Intersection (ft.) To	Interval (ft.)	oz/ton Au	oz/ton Ag
LRH-247	1984	525324E	4247439N	7,638	0	-90	162	62	136	74	0.017	0.57
LRH-248	1984	525278E	4247451N	7,627	0	-90	182	0	182	182	0.022	0.54
LRH-249	1984	525236E	4247444N	7,615	0	-90	162	0	132	132	0.018	0.26
LRH-250	1984	525225E	4247431N	7,615	0	-90	120	0	112	112	0.072	0.59
LRH-251	1984	525335E	4247471N	7,586	0	-90	200	0	85	85	0.018	0.51
LRH-251	1984	525335E	4247471N	7,586	0	-90	200	125	175	50	0.014	0.39
LRH-252	1984	525254E	4247492N	7,555	0	-90	200	0	190	190	0.017	0.33
LRH-253	1984	525314E	4247487N	7,566	0	-90	250	0	235	235	0.007	0.63
LRH-254	1984	525290E	4247494N	7,555	0	-90	250	0	30	30	0.009	0.30
LRH-254	1984	525290E	4247494N	7,555	0	-90	250	130	250	120	0.01	0.36
LRH-255	1984	525304E	4247494N	7,554	0	-90	260	0	55	55	0.007	0.12
LRH-255	1984	525304E	4247494N	7,554	0	-90	260	100	260	160	0.012	0.74
LRH-256	1984	525327E	4247492N	7,555	0	-90	230	0	55	55	0.008	0.41
LRH-256	1984	525327E	4247492N	7,555	0	-90	230	90	230	140	0.022	0.97
LRH-257	1984	525350E	4247483N	7,560	0	-90	200	0	20	20	0.009	0.15
LRH-257	1984	525350E	4247483N	7,560	0	-90	200	95	190	95	0.014	0.86
LRH-258	1984	525364E	4247475N	7,564	0	-90	160	0	10	10	0.008	0.14
LRH-258	1984	525364E	4247475N	7,564	0	-90	160	75	150	75	0.008	0.61
LRH-259	1984	525278E	4247501N	7,542	0	-90	280	5	60	55	0.007	0.08
LRH-259	1984	525278E	4247501N	7,542	0	-90	280	175	235	60	0.033	1.00
LRH-259	1984	525278E	4247501N	7,542	0	-90	280	270	280	10	0.033	2.00
LRH-260	1984	525384E	4247498N	7,516	0	-90	260	75	125	50	0.004	0.17
LRH-260	1984	525384E	4247498N	7,516	0	-90	260	150	180	30	0.008	0.81
LRH-261	1984	525416E	4247474N	7,506	0	-90	120	0	65	65	0.010	0.38
LRH-262	1984	525386E	4247464N	7,558	0	-90	140	0	100	100	0.020	0.66
LRH-263	1984	525393E	4247488N	7,521	0	-90	220	0	40	40	0.004	0.25
LRH-263	1984	525393E	4247488N	7,521	0	-90	220	70	120	50	0.006	0.65
LRH-264	1984	525370E	4247505N	7,514	0	-90	200	0	10	10	0.006	0.12
LRH-264	1984	525370E	4247505N	7,514	0	-90	200	170	190	20	0.012	1.41

Table 30-1 Reverse Circulation Drilling Record (1984-1997, and 2011-2013)

Star Gold Corp. – Longstreet Au-Ag Project, Nevada

Hole ID	Year	UTM Coordinates		Elevation (ft.)	Azimuth (⁰)	Inclination (⁰)	Length (ft.)	Intersection (ft.)		Interval (ft.)	oz/ton Au	oz/ton Ag
								From	To			
LRH-265	1984	525345E	4247526N	7,493	0	-90	300	0	20	20	0.048	0.48
LRH-265	1984	525345E	4247526N	7,493	0	-90	300	150	160	10	0.017	0.04
LRH-265	1984	525345E	4247526N	7,493	0	-90	300	195	205	10	0.011	0.05
LRH-265	1984	525345E	4247526N	7,493	0	-90	300	225	285	60	0.027	1.96
LRH-266	1984	525324E	4247533N	7,487	0	-90	290	80	120	40	0.020	0.21
LRH-266	1984	525324E	4247533N	7,487	0	-90	290	185	290	105	0.020	1.40
LRH-267	1984	525299E	4247534N	7,489	0	-90	320	0	10	10	0.015	0.29
LRH-267	1984	525299E	4247534N	7,489	0	-90	320	115	320	105	0.020	0.81
LRH-268	1984	525220E	4247552Nn	7,459	0	-90	320	0	10	10	0.022	0.45
LRH-268	1984	525220E	4247552N	7,459	0	-90	320	105	165	60	0.014	0.19
LRH-268	1984	525220E	4247552N	7,459	0	-90	320	220	240	20	0.024	0.57
LRH-269	1984	525203E	4247548N	7,454	0	-90	320	45	175	130	0.037	0.44
LRH-269	1984	525203E	4247548N	7,454	0	-90	320	200	225	25	0.007	0.13
LRH-270	1984	525187E	4247542N	7,449	0	-90	300	0	80	80	0.013	0.13
LRH-270	1984	525187E	4247542N	7,449	0	-90	300	130	195	65	0.015	0.23
LRH-271	1984	525174E	4247532N	7,444	0	-90	200	0	40	40	0.016	0.35
LRH-271	1984	525174E	4247532N	7,444	0	-90	200	90	160	70	0.013	0.22
LRH-272	1984	525208E	4247516N	7,499	0	-90	280	0	20	20	0.007	0.14
LRH-272	1984	525208E	4247516N	7,499	0	-90	280	75	200	125	0.037	0.43
LRH-274	1984	525222E	4247570E	7,436	0	-90	280	0	85	85	0.008	0.10
LRH-274	1984	525222E	4247570E	7,436	0	-90	280	245	200	55	0.020	0.28
LRH-274	1984	525222E	4247570E	7,436	0	-90	280	255	280	25	0.037	0.33
LRH-325	1984	525301E	4247324N	7,782	0	-90	60	0	60	60	0.026	0.22
LRH-326	1984	525316E	4247302N	7,794	240	-60	200	0	200	200	0.026	0.37
LRH-327	1984	525285E	4247275N	7,798	230	-60	150	0	150	150	0.006	0.68
LRH-328	1984	525293E	4247229N	7,803	337	-60	150	60	120	60	0.009	0.13
LRH-328	1984	525293E	4247229N	7,803	337	-60	150	130	140	10	0.005	0.10
LRH-329	1984	525298E	4247216N	7,801	357	-60	100	25	35	10	0.008	N/A
LRH-330	1984	525286E	4247246N	7,805	345	-60	100	45	70	25	0.017	0.10

Table 30-1 Reverse Circulation Drilling Record (1984-1997, and 2011-2013)

Star Gold Corp. – Longstreet Au-Ag Project, Nevada

Hole ID	Year	UTM Coordinates		Elevation (ft.)	Azimuth (⁰)	Inclination (⁰)	Length (ft.)	Intersection (ft.) From	Intersection (ft.) To	Interval (ft.)	oz/ton Au	oz/ton Ag
LRH-331	1984	525282E	4247216N	7,810	340	-60	150	40	90	50	0.008	0.17
LRH-332	1984	525313E	4247239N	7,789	340	-60	150	40	150	110	0.034	0.28
LRH-333	1984	525287E	4247335N	7,761	240	-60	150	35	120	85	0.010	0.25
LRH-334	1984	525296E	4247341N	7,766	240	-60	150	25	150	125	0.060	1.26
LRH-335	1984	525319E	4247336N	7,767	260	-60	200	0	10	10	0.006	0.17
LRH-335	1984	525319E	4247336N	7,767	260	-60	200	30	200	170	0.015	0.34
LRH-336	1984	525322E	4247332N	7,767	154	-60	100	25	45	20	0.009	0.11
LRH-337	1984	525332E	4247297N	7,763	250	-58	180	0	160	160	0.014	0.21
LRH-338	1984	525330E	4247300N	7,765	315	-58	150	0	10	10	0.005	0.19
LRH-338	1984	525330E	4247300N	7,765	315	-58	150	50	150	100	0.045	0.68
LRH-339	1984	525332E	4247275N	7,763	320	-57	150	0	105	105	0.011	0.17
LRH-340	1984	525332E	4247273N	7,764	234	-60	150	0	25	25	0.012	0.19
LRH-340	1984	525332E	4247273N	7,764	234	-60	150	65	80	15	0.005	0.16
LRH-340	1984	525332E	4247273N	7,764	234	-60	150	115	150	35	0.009	0.19
LRH-341	1984	525260E	4247353N	7,721	075	-60	160	0	160	160	0.039	0.73
LRH-342	1984	525271E	4247373N	7,717	214	-60	160	15	160	145	0.025	0.25
LRH-343	1984	525153E	4247317N	7,576	200	-60	100	15	25	10	0.006	0.01
LRH-343	1984	525153E	4247317N	7,576	200	-60	100	65	75	10	0.008	N/A
LRH-344	1984	525161E	4247348N	7,576	0	-90	100	80	90	10	0.006	N/A
LRH-345	1984	525168E	4247362N	7,577	0	-90	100	No significant values				
LRH-346	1984	525177E	4247380N	7,579	0	-90	100	0	40	40	0.015	0.39
LRH-347	1984	525187E	4247404N	7,576	0	-90	100	0	100	100	0.010	0.19
LRH-348	1984	525134E	4247342N	7,527	0	-90	100	0	25	25	0.005	0.08
LRH-349	1984	525145E	4247371N	7,521	0	-90	100	No significant values				
LRH-421	1984	525351E	4247241N	7,764	242	-60	200	125	200	75	0.008	0.32
LRH-459	1984	525299E	4247232N	7,798	0	-90	150	110	125	15	0.010	0.46
LRH-460	1984	525322E	4247236N	7,783	243	-60	200	40	70	30	0.008	0.15
LRH-460	1984	525322E	4247236N	7,783	243	-60	200	120	135	15	0.022	0.77
LRH-460	1984	525322E	4247236N	7,783	243	-60	200	180	195	15	0.010	0.27

Table 30-1 Reverse Circulation Drilling Record (1984-1997, and 2011-2013)

Star Gold Corp. – Longstreet Au-Ag Project, Nevada

Hole ID	Year	UTM Coordinates		Elevation (ft.)	Azimuth (°)	Inclination (°)	Length (ft.)	Intersection (ft.) From	To	Interval (ft.)	oz/ton Au	oz/ton Ag
LRH-461	1984	525315E	4247242N	7,787	081	-60	160	60	90	30	0.009	0.06
LRH-462	1984	525308E	4247253N	7,793	0	-90	200	10	120	110	0.044	0.64
LRH-463	1984	525308E	4247277N	7,792	060	-60	200	45	200	155	0.029	0.17
LRH-464	1984	525255E	4247190N	7,834	0	-90	90	No significant values				
LRH-465	1984	525242E	4247145N	7,844	0	-90	100	No significant values				
LRH-466	1984	525350E	4247274N	7,739	245	-60	200	10	65	55	0.009	0.07
LRH-466	1984	525350E	4247274N	7,739	245	-60	200	110	200	90	0.014	0.32
LRH-467	1984	525328E	4247323N	7,764	243	-60	200	0	200	200	0.026	0.46
LRH-468	1984	525332E	4247309N	7,761	250	-60	200	0	175	175	0,020	0.28
LRH-469	1984	525290E	4247289N	7,798	060	-60	50	5	50	45	0.006	0.13
LRH-470	1984	525284E	4247282N	7,797	060	-60	50	0	50	50	0.007	0.30
LRH-471	1984	525280E	4247260N	7,800	060	-60	150	0	150	150	0.021	0.52
LRH-472	1984	525305E	4247228N	7,795	060	-60	100	70	85	15	0.005	0.11
LRH-473	1984	525300E	4247254N	7,800	060	-60	150	0	55	55	0.007	0.16
LRH-474	1984	525314E	4247236N	7,788	060	-60	100	20	35	15	0.007	0.12
LRH-475	1984	525250E	4247341N	7,716	060	-60	100	0	45	45	0.009	0.28
LRH-476	1984	525241E	4247377N	7,682	060	-60	50	0	50	50	0.042	0.40
LRH-477	1984	525236E	4247370N	7,680	0	-90	50	0	35	35	0.011	0.19
LRH-479	1984	525202E	4247289N	7,679	120	-60	30	20	30	10	0.218	0.56
LRH-480	1984	525200E	4247279N	7,681	160	-60	100	0	20	20	0.005	0.10
LRH-480	1984	525200E	4247279N	7,681	160	-60	100	60	90	30	0.005	0.09
LRH-481	1984	525209E	4247326N	7,667	130	-60	100	20	45	25	0.017	0.40
LRH-481	1984	525209E	4247326N	7,661	130	-60	100	85	100	15	0.004	0.30
LRH-482	1984	525207E	4247318N	7,670	020	-60	100	25	80	55	0.065	0.37
LRH-483	1984	525214E	4247493N	7,533	240	-60	140	0	140	140	0.018	0.40
LRH-484	1984	525271E	4247489N	7,563	240	-60	120	10	65	55	0.010	0.27
LRH-484	1984	525271E	4247489N	7,563	240	-60	120	105	120	15	0.004	0.09
LRH-485	1984	525202E	4247530N	7,477	225	-60	100	0	20	20	0.010	0.14
LRH-485	1984	525202E	4247530N	7,477	225	-60	100	40	90	50	0.010	0.24

Table 30-1 Reverse Circulation Drilling Record (1984-1997, and 2011-2013)

Star Gold Corp. – Longstreet Au-Ag Project, Nevada

Hole ID	Year	UTM Coordinates		Elevation (ft.)	Azimuth (°)	Inclination (°)	Length (ft.)	Intersection (ft.) From	To	Interval (ft.)	oz/ton Au	oz/ton Ag
LRH-486	1984	525211E	4247569N	7,432	210	-60	100	0	15	15	0.026	0.27
LRH-486	1984	525211E	4247569N	7,432	210	-60	100	45	100	55	0.005	0.09
LRH-487	1984	525417E	4247331N	7,601	0	-90	200	0	10	10	0.005	0.16
LRH-488	1984	525313E	4247261N	7,688	260	-60	100	15	85	70	0.007	0.24
LRH-510	1984	525173E	4247290N	7,624	106	-60	100	5	20	15	0.005	0.08
LRH-510	1984	525173E	4247290N	7,624	106	-60	100	80	95	15	0.004	0.06
LRH-511	1984	525202E	4247292N	7,677	108	-60	100	40	95	55	0.006	0.10
LRH-512	1984	525211E	4247306N	7,683	108	-60	100	0	30	30	0.011	0.77
LRH-512	1984	525211E	4247306N	7,683	108	-60	100	70	85	15	0.011	0.19
LRH-513	1984	525232E	4247358N	7,682	120	-60	100	60	70	10	0.004	0.10
LRH-513	1984	525232E	4247358N	7,682	120	-60	100	90	100	10	0.004	0.08
LRH-514	1984	525246E	4247372N	7,692	117	-60	150	0	80	80	0.024	0.21
LRH-514	1984	525246E	4247372N	7,692	117	-60	150	110	130	20	0.009	0.11
LRH-515	1984	525349E	4247322N	7,725	247	-60	200	0	20	20	0.004	0.12
LRH-515	1984	525349E	4247322N	7,725	247	-60	200	45	55	10	0.007	0.17
LRH-515	1984	525349E	4247322N	7,725	247	-60	200	75	145	70	0.018	0.48
LRH-516	1984	525297E	4247240N	7,800	0	-90	150	45	90	45	0.011	0.11
LRH-516	1984	525297E	4247240N	7,800	0	-90	150	105	130	25	0.004	0.14
LRH-517	1984	525313E	4247206N	7,799	0	-90	150	No significant values				
V-1	1987	525301E	4247325N	7,782	0	-90	195	0	130	130	0.026	0.36
V-1	1987	525301E	4247325N	7,782	0	-90	195	150	195	45	0.017	0.29
V-2	1987	525288E	4247288N	7,798	0	-90	105	0	100	100	0.016	0.47
PR-1	1987	525293E	4247378N	7,723	180	-45	300	0	15	15	0.003	0.07
PR-1	1987	525293E	4247378N	7,723	180	-45	300	50	70	20	0.005	0.04
PR-1	1987	525293E	4247378N	7,723	180	-45	300	115	215	100	0.012	0.37
PR-1	1987	525293E	4247378N	7,723	180	-45	300	245	295	50	0.013	1.24
PR-2	1987	525342E	4247346N	7,722	191	-45	300	15	25	10	0.004	0.39
PR-2	1987	525342E	4247346N	7,722	191	-45	300	65	75	10	0.005	0.51
PR-2	1987	525342E	4247346N	7,722	191	-45	300	95	145	50	0.013	0.30

Table 30-1 Reverse Circulation Drilling Record (1984-1997, and 2011-2013)

Star Gold Corp. – Longstreet Au-Ag Project, Nevada

Hole ID	Year	UTM Coordinates		Elevation (ft.)	Azimuth (°)	Inclination (°)	Length (ft.)	Intersection (ft.)		Interval (ft.)	oz/ton Au	oz/ton Ag
								From	To			
PR-2	1987	525342E	4247346N	7,722	191	-45	300	165	200	35	0.014	0.48
PR-3	1987	525278E	4247427N	7,661	180	-45	300	0	120	120	0.018	0.53
PR-3	1987	525278E	4247427N	7,661	180	-45	300	140	180	40	0.028	1.99
PR-3	1987	525278E	4247427N	7,661	180	-45	300	195	205	10	0.005	0.09
PR-3	1987	525278E	4247427N	7,661	180	-45	300	220	290	70	0.004	0.08
PR-4	1987	525225E	4247465N	7,577	191	-50	300	0	120	120	0.019	0.22
PR-4	1987	525225E	4247465N	7,577	191	-50	300	150	165	15	0.004	N/A
PR-4	1987	525225E	4247465N	7,577	191	-50	300	195	235	40	0.006	0.31
PR-5	1987	525264E	4247492N	7,563	191	-50	300	30	205	175	0.017	0.24
PR-5	1987	525264E	4247492N	7,563	191	-50	300	230	245	15	0.024	1.67
PR-6	1987	525361E	4247445N	7,605	191	-50	300	0	60	60	0.023	0.38
PR-6	1987	525361E	4247445N	7,605	191	-50	300	120	130	10	0.006	N/A
PR-6	1987	525361E	4247445N	7,605	191	-50	300	165	190	25	0.005	N/A
PR-6	1987	525361E	4247445N	7,605	191	-50	300	285	300	15	0.008	0.89
PR-7	1987	525298E	4247556N	7,455	191	-50	500	5	15	10	0.006	N/A
PR-7	1987	525298E	4247556N	7,455	191	-50	500	95	120	25	0.006	0.19
PR-7	1987	525298E	4247556N	7,455	191	-50	500	205	265	60	0.030	1.90
PR-7	1987	525298E	4247556N	7,455	191	-50	500	295	305	10	0.005	0.23
PR-8	1987	525380E	4247515N	7,494	198	-50	300	70	145	75	0.014	0.41
PR-8	1987	525380E	4247515N	7,494	198	-50	300	145	170	25	0.310	1.73
PR-9	1987	525245E	4247566N	7,445	196	-50	300	0	30	30	0.009	0.06
PR-9	1987	525245E	4247566N	7,445	196	-50	300	115	220	105	0.039	0.28
PR-10	1987	525316E	4247321N	7,782	234	-45	300	0	235	235	0.021	0.35
PR-10	1987	525316E	4247321N	7,782	235	-45	300	265	285	20	0.004	0.18
PR-11	1987	525332E	4247258N	7,768	235	-45	300	25	45	20	0.007	0.11
PR-11	1987	525332E	4247258N	7,768	235	-45	300	65	150	85	0.011	0.28
PR-12	1987	525371E	4247284N	7,707	235	-45	300	55	75	20	0.005	0.18
PR-12	1987	525371E	4247284N	7,707	235	-45	300	85	95	10	0.006	0.49
PR-12	1987	525371E	4247284N	7,707	235	-45	300	105	150	45	0.007	0.17

Table 30-1 Reverse Circulation Drilling Record (1984-1997, and 2011-2013)

Star Gold Corp. – Longstreet Au-Ag Project, Nevada

Hole ID	Year	UTM Coordinates		Elevation (ft.)	Azimuth (°)	Inclination (°)	Length (ft.)	Intersection (ft.)		Interval (ft.)	oz/ton Au	oz/ton Ag
								From	To			
PR-12	1987	525371E	4247284N	7,707	235	-45	300	290	300	10	0.009	1.81
PR-13	1987	525267E	4247369N	7,717	235	-45	195	0	120	120	0.015	0.41
PR-13	1987	525267E	4247369N	7,717	235	-45	195	150	195	45	0.005	0.18
PR-14	1987	525442E	4247472N	7,469	191	-45	300	0	45	45	0.010	0.58
PR-14	1987	525442E	4247472N	7,469	191	-45	300	215	225	10	0.004	1.51
PR-15	1987	525155E	4247504N	7,444	191	-45	300	0	10	10	0.007	0.46
PR-15	1987	525155E	4247504N	7,444	191	-45	300	75	85	10	0.007	0.12
PR-16	1987	525172E	4247555N	7,418	191	-45	300	10	20	10	0.005	0.05
PR-16	1987	525172E	4247555N	7,418	191	-45	300	40	190	150	0.013	0.22
PR-17	1987	525388E	4247581N	7,396	191	-45	300	20	30	10	0.005	0.03
PR-17	1987	525388E	4247581N	7,396	191	-45	300	220	255	35	0.034	4.85
PR-18	1987	525301E	4247606N	7,376	191	-45	350	0	15	15	0.005	0.15
PR-18	1987	525301E	4247606N	7,376	191	-45	350	80	90	10	0.005	0.45
PR-18	1987	525301E	4247606N	7,376	191	-45	350	180	195	15	0.007	0.25
PR-18	1987	525301E	4247606N	7,376	191	-45	350	240	255	15	0.004	0.17
PR-18	1987	525301E	4247606N	7,376	191	-45	350	280	295	15	0.091	1.20
PR-18	1987	525301E	4247606N	7,376	191	-45	350	325	335	10	0.011	0.05
PR-19	1987	525254E	4247615N	7,371	191	-45	240	0	65	65	0.007	0.20
PR-21	1987	525407E	4247673N	7,274	191	-45	300	No significant values				
PR-22	1987	525310E	4247668N	7,269	191	-45	400	0	10	10	0.007	0.24
PR-22	1987	525310E	4247668N	7,269	191	-45	400	340	390	50	0.008	3.37
PR-23	1987	525253E	4247697N	7,269	191	-45	350	No significant values				
PR-24	1987	525193E	4247670N	7,283	191	-45	400	No significant values				
PR-25	1987	525310E	4247668N	7,269	0	-90	600	0	20	20	0.005	0.21
PR-26	1987	525407E	4247673	7,274	191	-45	450	No significant values				
PR-27	1987	525407E	4247673N	7,274	0	-90	600	No significant values				
PR-28	1987	525464E	4247619N	7,314	191	-45	450	No significant values				
PR-29	1987	525464E	4247619N	7,314	0	-90	600	410	420	10	0.006	0.15
PR-30	1987	525253E	4247697N	7,269	191	-45	450	No significant values				

Table 30-1 Reverse Circulation Drilling Record (1984-1997, and 2011-2013)

Star Gold Corp. – Longstreet Au-Ag Project, Nevada

Hole ID	Year	UTM Coordinates		Elevation (ft.)	Azimuth (°)	Inclination (°)	Length (ft.)	Intersection (ft.) From	To	Interval (ft.)	oz/ton Au	oz/ton Ag
PR-31	1987	525253E	4247697N	7,269	0	-90	600	No significant values				
LS-1101	2011	525327E	4247358N	7,733	191	-50	400	0	40	40	0.024	0.34
LS-1101	2011	525327E	4247358N	7,733	191	-50	400	80	245	165	0.009	0.61
LS-1101	2011	525327E	4247358N	7,733	191	-50	400	290	325	35	0.007	0.32
LS-1101	2011	525327E	4247358N	7,733	191	-50	400	360	375	15	0.013	2.77
LS-1102	2011	525375E	4247361N	7,669	191	-70	350	210	225	15	0.008	0.99
LS-1103	2011	525350E	4247415N	7,648	191	-45	300	0	50	50	0.013	0.47
LS-1103	2011	525350E	4247415N	7,648	191	-45	300	180	195	15	0.004	0.57
LS-1103	2011	525350E	4247415N	7,648	191	-45	300	255	285	30	0.007	1.06
LS-1104	2011	525303E	4247423N	7,667	191	-45	380	0	95	95	0.014	0.92
LS-1104	2011	525303E	4247423N	7,667	191	-45	380	130	200	70	0.005	0.34
LS-1104	2011	525303E	4247423N	7,667	191	-45	380	235	250	15	0.008	0.39
LS-1104	2011	525303E	4247423N	7,667	191	-45	380	325	335	10	0.005	0.17
LS-1105	2011	525176E	4247286N	7,663	191	-45	250	No significant values				
LS-1106	2011	525199E	4247422N	7,581	191	-45	250	0	90	90	0.011	0.32
LS-1106	2011	525199E	4247422N	7,581	191	-45	250	145	160	15	0.007	0.90
LS-1107	2011	525194E	4247494N	7,509	191	-45	300	0	135	135	0.006	0.31
LS-1107	2011	525194E	4247494N	7,509	191	-45	300	155	165	10	0.005	0.16
LS-1107	2011	525194E	4247494N	7,509	191	-45	300	200	270	70	0.014	0.95
LS-1108	2011	525176E	4247599N	7,356	191	-45	300	0	55	55	0.011	0.21
LS-1108	2011	525176E	4247599N	7,356	191	-45	300	85	120	35	0.021	0.24
LS-1108	2011	525176E	4247599N	7,356	191	-45	300	165	180	15	0.016	0.18
LS-1109	2011	525229E	4247614N	7,371	191	-70	300	0	40	40	0.008	0.26
LS-1110	2011	525417E	4247559N	7,415	191	-45	350	205	215	10	0.004	0.88
LS-1111	2011	525148E	4247434N	7,482	191	-45	300	0	50	50	0.015	0.34
LS-1112	2011	525213E	4247392N	7,631	191	-45	300	0	35	35	0.013	0.22
LS-1112	2011	525213E	4247392N	7,631	191	-45	300	170	180	10	0.004	0.07
LS-1113	2011	525240E	4247443N	7,620	191	-45	290	0	145	145	0.023	0.39
LS-1113	2011	525240E	4247443N	7,620	191	-45	290	185	195	10	0.003	0.30

Table 30-1 Reverse Circulation Drilling Record (1984-1997, and 2011-2013)

Star Gold Corp. – Longstreet Au-Ag Project, Nevada

Hole ID	Year	UTM Coordinates		Elevation (ft.)	Azimuth (⁰)	Inclination (⁰)	Length (ft.)	Intersection (ft.) From	Intersection (ft.) To	Interval (ft.)	oz/ton Au	oz/ton Ag
LS-1113	2011	525240E	4247443N	7,620	191	-45	290	240	285	45	0.006	0.79
LS-1114	2011	525365E	4247571N	7,402	191	-70	400	155	170	15	0.009	0.70
LS-1114	2011	525365E	4247571N	7,402	191	-70	400	265	310	45	0.008	1.88
LS-1115	2011	525341E	4247598N	7,380	191	-45	400	235	295	60	0.016	1.26
LS-1116	2011	525290E	4247677N	7,265	191	-45	400	0	30	30	0.008	0..20
LS-1116	2011	525290E	4247677N	7,265	191	-45	400	250	265	15	0.006	0.12
LS-1116	2011	525290E	4247677N	7,265	191	-45	400	310	325	15	0.027	0.11
LS-1201	2012	525419E	4247233N	7,725	0	-90	480	50	70	20	0.005	0.02
LS-1201	2012	525419E	4247233N	7,725	0	-90	480	225	240	15	0.004	0.04
LS-1201	2012	525419E	4247233N	7,725	0	-90	480	390	405	15	0.007	1.13
LS-1202	2012	525317E	4247340N	7,765	191	-45	500	0	255	255	0.018	0.53
LS-1202	2012	525317E	4247340N	7,765	191	-45	500	355	365	10	0.005	0.20
LS-1203	2012	525331E	4247395N	7,680	187	-45	550	0	40	40	0.008	0.43
LS-1203	2012	525331E	4247395N	7,680	187	-45	550	190	230	40	0.004	0.79
LS-1203	2012	525331E	4247395N	7,680	187	-45	550	285	325	40	0.006	0.62
LS-1203	2012	525331E	4247395N	7,680	187	-45	550	430	445	15	0.008	0.19
LS-1204	2012	525275E	4247371N	7,705	191	-45	400	15	100	85	0.028	0.51
LS-1204	2012	525275E	4247371N	7,705	191	-45	400	170	180	10	0.005	1.48
LS-1204	2012	525275E	4247371N	7,705	191	-45	400	220	240	20	0.011	0.29
LS-1204	2012	525275E	4247371N	7,705	191	-45	400	260	270	10	0.004	0.21
LS-1205	2012	525369E	4247285N	7,700	191	-65	320	95	285	190	0.065	0.37
LS-1206	2012	525306E	4247455N	7,605	191	-45	500	0	140	140	0.026	0.70
LS-1206	2012	525306E	4247455N	7,605	191	-45	500	210	235	25	0.015	1.00
LS-1206	2012	525306E	4247455N	7,605	191	-45	500	335	355	20	0.004	0.14
LS-1206	2012	525306E	4247455N	7,605	191	-45	500	380	395	15	0.005	0.49
LS-1207	2012	525252E	4247420N	7,635	191	-45	400	0	125	125	0.010	0.42
LS-1207	2012	525252E	4247420N	7,635	191	-45	400	200	215	15	0.021	0.33
LS-1208	2012	525245E	4247445N	7,615	191	-70	320	0	135	135	0.018	0.38
LS-1208	2012	525245E	4247445N	7,615	191	-70	320	180	195	15	0.034	0.45

Table 30-1 Reverse Circulation Drilling Record (1984-1997, and 2011-2013)
Star Gold Corp. – Longstreet Au-Ag Project, Nevada

Hole ID	Year	UTM Coordinates		Elevation (ft.)	Azimuth (°)	Inclination (°)	Length (ft.)	Intersection (ft.) From	To	Interval (ft.)	oz/ton Au	oz/ton Ag
LS-1209	2012	525339E	4247451N	7,605	191	-45	450	0	120	120	0.015	0.50
LS-1209	2012	525339E	4247451N	7,605	191	-45	450	180	190	10	0.005	0.13
LS-1209	2012	525339E	4247451N	7,605	191	-45	450	285	315	30	0.018	2.39
LS-1210	2012	525388E	4247405N	7,600	191	-45	400	235	245	10	0.006	1.48
LS-1210	2012	525388E	4247405N	7,600	191	-45	400	275	295	20	0.004	1.19
LS-1210	2012	525388E	4247405N	7,600	191	-45	400	390	400	10	0.006	0.34
LS-1211	2012	525187E	4247455N	7,528	191	-45	330	0	110	110	0.009	0.25
LS-1211	2012	525187E	4247455N	7,528	191	-45	330	130	180	50	0.004	0.44
LS-1212	2012	525351E	4247480N	7,555	191	-45	500	0	15	15	0.010	0.25
LS-1212	2012	525351E	4247480N	7,555	191	-45	500	210	235	25	0.005	0.47
LS-1212	2012	525351E	4247480N	7,555	191	-45	500	320	345	25	0.010	1.69
LS-1213	2012	525230E	4247517N	7,505	191	-45	430	0	220	220	0.015	0.29
LS-1213	2012	525230E	4247517N	7,505	191	-45	430	380	390	10	0.034	0.03
LS-1214	2012	525200E	4247525N	7,470	191	-45	450	20	165	145	0.013	0.35
LS-1215	2012	525214E	4247567N	7,425	191	-45	470	0	225	225	0.022	0.31
LS-1218N	2012	525025E	4248411N	7,296	191	-45	400	0	40	40	0.011	0.11
LS-1218N	2012	525025E	4248411N	7,296	191	-45	400	175	190	15	0.010	0.05
LS-1218N	2012	525025E	4248411N	7,296	191	-45	400	225	245	20	0.005	0.09
LS-1218N	2012	525025E	4248411N	7,296	191	-45	400	270	330	60	0.007	0.25
LS-1219N	2012	525080E	4248341N	7,316	191	-45	400	50	85	35	0.004	0.11
LS-1219N	2012	525080E	4248341N	7,316	191	-45	400	110	175	65	0.006	0.09
LS-1219N	2012	525080E	4248341N	7,316	191	-45	400	290	310	20	0.004	0.05
LS-1220N	2012	525143E	4248281N	7,349	191	-45	400	40	70	30	0.014	0.16
LS-1220N	2012	525143E	4248281N	7,349	191	-45	400	120	135	15	0.009	0.16
LS-1220N	2012	525143E	4248281N	7,349	191	-45	400	265	290	25	0.005	0.25
LS-1221	2012	525252E	4247610N	7,365	191	-70	600	0	50	50	0.008	0.23
LS-1223	2012	525354E	4247539N	7,470	191	-45	510	0	20	20	0.006	0.19
LS-1223	2012	525354E	4247539N	7,470	191	-45	510	155	205	50	0.008	0.51
LS-1223	2012	525354E	4247539N	7,470	191	-45	510	370	385	15	0.006	0.68

Table 30-1 Reverse Circulation Drilling Record (1984-1997, and 2011-2013)

Star Gold Corp. – Longstreet Au-Ag Project, Nevada

Hole ID	Year	UTM Coordinates		Elevation (ft.)	Azimuth (°)	Inclination (°)	Length (ft.)	Intersection (ft.)		Interval (ft.)	oz/ton Au	oz/ton Ag
								From	To			
LS-1223	2012	525354E	4247539N	7,470	191	-45	510	395	410	15	0.005	0.64
LS-1225	2012	525311E	4247491N	7,560	191	-45	480	0	50	50	0.010	0.29
LS-1225	2012	525311E	4247491N	7,560	191	-45	480	100	110	10	0.006	0.22
LS-1225	2012	525311E	4247491N	7,560	191	-45	480	130	165	35	0.022	1.31
LS-1225	2012	525311E	4247491N	7,560	191	-45	480	190	210	20	0.006	1.45
LS-1225	2012	525311E	4247491N	7,560	191	-45	480	255	340	85	0.008	0.94
LS-1225	2012	525311E	4247491N	7,560	191	-45	480	360	370	10	0.005	0.07
LS-1226	2012	525377E	4247478N	7,550	191	-45	450	0	75	75	0.008	0.42
LS-1226	2012	525377E	4247478N	7,550	191	-45	450	85	105	20	0.005	0.58
LS-1226	2012	525377E	4247478N	7,550	191	-45	450	320	355	35	0.004	1.39
LS-1226	2012	525377E	4247478N	7,550	191	-45	450	400	410	10	0.004	0.24
LS-1227	2012	525367E	4247571N	7,402	191	-45	500	0	10	10	0.004	0.11
LS-1227	2012	525367E	4247571N	7,402	191	-45	500	230	255	35	0.018	1.03
LS-1227	2012	525367E	4247571N	7,402	191	-45	500	335	350	15	0.004	0.41
LS-1301	2013	525295E	4247236N	7,792	191	-45	300	0	50	50	0.008	0.27
LS-1301	2013	525295E	4247236N	7,792	191	-45	300	90	105	15	0.004	0.13
LS-1301	2013	525295E	4247236N	7,792	191	-45	300	150	160	10	0.016	0.06
LS-1301	2013	525295E	4247236N	7,792	191	-45	300	190	215	25	0.009	0.14
LS-1302	2013	525316E	4247293N	7,788	191	-45	450	0	40	40	0.015	0.89
LS-1302	2013	525316E	4247293N	7,788	191	-45	450	75	150	75	0.011	0.56
LS-1302	2013	525316E	4247293N	7,788	191	-45	450	210	265	55	0.013	0.46
LS-1303	2013	525355E	4247239N	7,750	191	-80	400	90	110	20	0.003	1.12
LS-1303	2013	525355E	4247239N	7,750	191	-80	400	165	205	40	0.006	0.26
LS-1303	2013	525355E	4247239N	7,750	191	-80	400	220	270	50	0.004	0.27
LS-1304	2013	525234E	4247300N	7,705	191	-45	300	45	85	40	0.006	0.36
LS-1304	2013	525234E	4247300N	7,705	191	-45	300	120	155	35	0.047	0.36
LS-1305	2013	525246E	4247384N	7,683	191	-45	400	0	125	125	0.008	0.27

Table 30-1 Reverse Circulation Drilling Record (1984-1997, and 2011-2013)

Star Gold Corp. – Longstreet Au-Ag Project, Nevada

Hole ID	Year	UTM Coordinates		Elevation (ft.)	Azimuth (°)	Inclination (°)	Length (ft.)	Intersection (ft.) From	To	Interval (ft.)	oz/ton Au	oz/ton Ag
LS-1305	2013	525246E	4247384N	7,683	191	-45	400	205	220	15	0.005	0.27
LS-1306	2013	525373E	4247378N	7,649	191	-45	400	205	230	25	0.005	0.97
LS-1307	2013	525197E	4247356N	7,628	191	-45	300	10	40	30	0.004	0.11
LS-1307	2013	525197E	4247356N	7,628	191	-45	300	125	140	15	0.010	1.16
LS-1308	2013	525420E	4247328N	7,601	191	-45	400	85	100	15	0.004	0.16
LS-1308	2013	525420E	4247328N	7,601	191	-45	400	285	310	25	0.005	1.56
LS-1309	2013	525289E	4247469N	7,593	191	-45	350	0	230	230	0.022	0.64
LS-1309	2013	525289E	4247469N	7,593	191	-45	350	325	340	15	0.003	0.33
LS-1310	2013	525150E	4247385N	7,150	188	-45	295	No significant values				
LS-1311	2013	525411E	4247491N	7,480	191	-55	400	20	115	95	0.008	0.66
LS-1312	2013	525324E	4247529N	7,487	191	-45	400	45	70	25	0.009	0.74
LS-1312	2013	525324E	4247529N	7,487	191	-45	400	120	220	100	0.013	1.04
LS-1312	2013	525324E	4247529N	7,487	191	-45	400	295	310	15	0.010	0.61
LS-1313	2013	525264E	4247531N	7,480	191	-45	400	0	15	15	0.009	0.29
LS-1313	2013	525264E	4247531N	7,480	191	-45	400	50	105	55	0.019	0.74
LS-1313	2013	525264E	4247531N	7,480	191	-45	400	160	200	40	0.038	0.81
LS-1313	2013	525264E	4247531N	7,480	191	-45	400	235	250	15	0.005	0.15
LS-1314	2013	525392E	4247461N	7,550	191	-45	400	0	60	60	0.018	0.63
LS-1314	2013	525392E	4247461N	7,550	191	-45	400	310	370	60	0.006	2.06
LS-1315	2013	525138E	4247529N	7,420	191	-45	270	0	15	15	0.005	0.32
LS-1316	2013	525278E	4247611N	7,380	191	-45	395	0	30	30	0.014	0.22
LS-1316	2013	525278E	4247611N	7,380	191	-45	395	175	280	105	0.010	0.29
LS-1317	2013	525519E	4247421N	7,401	191	-45	280	No significant values				
LS-1318	2013	525152E	4247588N	7,355	191	-45	280	0	75	75	0.006	0.32
LS-1319	2013	525483E	4247561N	7,359	191	-45	410	175	195	20	0.047	15.43
LS-1320	2013	525272E	4247685N	7,260	191	-45	100	0	20	20	0.004	0.20

Source: Star Gold, 2012, Kern, 2012, 2013.

Notes:

1. Average assay values >0.005 oz/ton Au (0.18 g/t Au) are considered significant.
2. Detection limits: 2 g/t Ag, 0.01 g/t Au; Results below these detection limits are half of the detection limits.
3. Gold and silver values are rounded.
4. NSV means no significant values.
5. N/A means not available.
6. Reported assay values are uncut.
7. Elevations are drill hole collar elevations in metres.
8. Drill holes LS-1218N, 1219N, and 1220N were drilled on the North Zone.
9. The exact date of the historic holes from 1984 to 1987 are uncertain.

Summary of Significant Mineralized Intersections in Diamond Drill Holes (1987 and 2012)

Table 30-2 Diamond Drilling Record (1987 and 2012)
Star Gold Corp. – Longstreet Au-Ag Project, Nevada

Hole ID	Year	Zone	UTM Coordinates		Elevation (ft.)	Azimuth (°)	Inclination (°)	Length (ft.)	Intersection (ft.) From	Intersection (ft.) To	Interval (ft.)	oz/ton Au	oz/ton Ag
LS-1	1987	Cyprus Ridge	N/A	N/A	N/A	216	-75	285	260	270	10	0.011	N/A
LS-2	1987	Cyprus Ridge	N/A	N/A	N/A	215	-83	345	310	320	10	0.013	N/A
LS-3	1987	Cyprus Ridge	N/A	N/A	N/A	225	-75	340	240	260	20	0.010	N/A
LS-4	1987	Cyprus Ridge	N/A	N/A	N/A	225	-70	290	100	120	20	0.012	N/A
LS-4	1987	Cyprus Ridge	N/A	N/A	N/A	225	-70	290	230	260	30	0.010	N/A
LS-5	1987	Cyprus Ridge	N/A	N/A	N/A	185	-70	360	300	310	10	0.034	N/A
LS-6	1987	Cyprus Ridge	N/A	N/A	N/A	225	-70	280	No significant values				
LS-7	1987	Cyprus Ridge	N/A	N/A	N/A	0	-90	275	No significant values				
LS-8	1987	Cyprus Ridge	N/A	N/A	N/A	0	-90	150	No significant values				
LS-9	1987	Cyprus Ridge	N/A	N/A	N/A	0	-90	330	220	230	30	0.009	N/A
LS-10	1987	Cyprus Ridge	N/A	N/A	N/A	0	-90	80	No significant values				
LS-11	1987	Cyprus Ridge	N/A	N/A	N/A	0	-90	100	No significant values				
LS-12	1987	Cyprus Ridge	N/A	N/A	N/A	0	-90	185	No significant values				
LS-1216C	2012	Main	525331E	4247362N	7,733	191	-55	397	25	235	210	0.008	0.47
LS-1217C	2012	Main	525265E	4247488N	7,563	191	-55	298	0	205	205	0.017	0.40
LS-1222C	2012	Main	525252E	4247566N	7,440	191	-50	299	5	65	60	0.006	0.17
LS-1222C	2012	Main	525252E	4247566N	7,440	191	-50	299	125	220	95	0.017	0.30
LS-1224C	2012	Main	525300E	4247518N	7,509	216	-65	299	105	120	15	0.021	0.48
LS-1224C	2012	Main	525300E	4247518N	7,509	216	-65	299	155	175	20	0.005	0.06
LS-1224C	2012	Main	525300E	4247518N	7,509	216	-65	299	195	255	60	0.034	2.47

Source: Noland, 2012.

Notes:
1. Diamond drilling in 1987 carried out by Cyprus Minerals Company.
2. Diamond drilling in 2012 carried out by Star Gold Corp.

Appendix 3. McClelland Metallurgical Report 2014

McCLELLAND LABORATORIES, INC.

1016 Greg Street, Sparks, Nevada 89431 (775) 356-1300
FAX (775) 356-8917
E-MAIL mli@mettest.com

April 16, 2014

Mr. David Segelov
Star Gold Corp.
611 E. Sherman Ave.
Coeur d'Alene, ID 83814

Dear David:

Enclosed is our report concerning results from heap leach cyanidation testing conducted on three composites from your Longstreet project.

Our invoice for the completed work will be sent under separate cover.

Thank you for allowing us to serve you.

Sincerely,

Jared R. Olson
Metallurgist / Project Manager

JRO:mh
Enclosure

McCLELLAND LABORATORIES, INC.
1016 Greg Street, Sparks, Nevada 89431 (775) 356-1300
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Report
on
Heap Leach Cyanidation Testing -
Longstreet Project
MLI Job No. 3829
April 16, 2014

for

Mr. David Segelov
Star Gold Corp.
611 E. Sherman Ave.
Coeur d'Alene, ID 83814

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Report
on
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MLI Job No. 3829
April 16, 2014

for

Mr. David Segelov
Star Gold Corp.
611 E. Sherman Ave.
Coeur d'Alene, ID 83814

EXECUTIVE SUMMARY

A heap leach cyanidation testing program was undertaken on three composites from the Longstreet project. The composites were prepared from 19 underground adit samples and 3 surface samples taken from the project site. Composites were identified as the surface, underground, and master composites. Average gold head grades of the composites ranged from 0.38 to 0.84 gAu/mt ore. Average silver head grades of the three composites 25 to 59 gAg/mt ore.

Column leach tests were conducted on each composite at an 80%-19mm feed size to determine gold recovery, recovery rate, and reagent requirements, under simulated heap leaching conditions. Bottle roll tests were conducted on each of the three composites at an 80%-1.7mm feed size. Additional bottle roll tests were conducted on the master composite at feed sizes ranging from 100%-50mm to 80%-75µm, and at cyanide concentrations of 1.0 and 5.0 gNaCN/L, to determine sensitivity to feed size and cyanide concentration.

Summary results from the column leach and bottle roll tests are presented in Table 1.

Table 1. - Summary Metallurgical Results, Heap Leach Testing, Longstreet Composites

Composite	Test Type	Test No.	Leach Time, days	Feed Size	NaCN Conc. g/L	Recovery, % Au	Recovery, % Ag	Calc'd. Head, g/mt ore Au	Calc'd. Head, g/mt ore Ag	NaCN Consumed, kg/mt ore	Lime Added, kg/mt ore
Surface	CLT	P-1	190	80%-19mm	1.0	88.9	20.0	0.36	25	1.56	1.7
Surface	BRT	CY-2	4	80%-1.7mm	1.0	80.6	20.0	0.31	25	0.08	2.1
Underground	CLT	P-2	190	80%-19mm	1.0	84.6	15.4	0.78	52	1.93	2.7
Underground	BRT	CY-1	4	80%-1.7mm	1.0	81.9	18.9	0.83	53	0.13	3.4
Master	CLT	P-3	190	80%-19mm	1.0	86.3	16.7	0.73	48	1.86	2.0
Master	BRT	CY-4	4	100%-50mm	1.0	62.9	3.6	0.70	56	0.07	1.3
Master	BRT	CY-5	4	80%-19mm	1.0	67.1	12.8	0.76	39	0.07	2.1
Master	BRT	CY-6	4	80%-6.3mm	1.0	77.9	13.6	0.68	44	<0.07	3.0
Master	BRT	CY-3	4	80%-1.7mm	1.0	81.3	17.5	0.64	40	0.13	2.5
Master	BRT	CY-7	4	80%-19mm	5.0	76.4	14.6	0.72	41	0.48	1.0
Master	BRT	CY-8	4	80%-6.3mm	5.0	77.6	14.0	0.58	43	0.67	1.0
Master	BRT	CY-9	4	80%-75µm	5.0	88.7	60.6	0.53	33	0.91	1.3

Column test results show that the three composites were readily amenable to heap leach cyanidation treatment at an 80%-19mm feed size. Gold recoveries were similar for each composite, and ranged from 84.6% to 88.9%, in 190 days of leaching and rinsing.

Column leach test silver recoveries were low and ranged from 15.4% to 20.0%.

Gold recovery rates, during column leach testing were rapid. Silver recovery rates were slow.

Several bottle roll tests were conducted on the master composite at varying feed sizes and cyanide concentrations, in an attempt to improve silver recovery. Tests conducted at crushed feed sizes (-50mm to 80%-1.7mm), using cyanide concentrations of 1.0 and 5.0 gNaCN/L, indicated that the composite was not particularly sensitive to feed size or cyanide concentration, with respect to silver recovery. Silver recoveries, at these conditions, ranged from 3.6% to 17.5%. A test conducted at 80%-75µm (5.0 gNaCN/L) showed that fine grinding was effective in substantially increasing silver recovery by cyanidation (to 60.6%). Column leach test recovery by size fraction data also suggest that fine grinding would likely be required to maximize silver recovery.

The master composite was not particularly sensitive to feed size with respect to gold recovery, given a sufficiently long leach cycle. Gold recovery achieved by column leach testing of the master composite at an 80%-19mm feed size (86.3%) was nearly the same as the bottle roll test recovery achieved at the 80%-75µm feed size (88.7%).

Cyanide consumption during column leach testing was high, in part because of the long leach cycles employed, and ranged from 1.56 to 1.93 kgNaCN/mt ore. Cyanide consumption for column leach testing typically is significantly higher than observed during commercial heap leaching. Cyanide consumption was much lower during bottle roll testing, and ranged from <0.07 to 0.13 kgNaCN/mt ore, when a cyanide concentration of 1.0 gNaCN/L was maintained.

The column test lime additions of 1.7 to 2.7 kg/mt ore were sufficient for maintaining protective alkalinity throughout the leach cycle.

SAMPLE PREPARATION AND HEAD ANALYSIS

On June 30, 2013, a total of 22 "section" bulk samples were received for preparation and analysis. Of those samples, 19 were designated as underground adit samples, and 3 were designated as surface samples. Underground adit samples weighed 9 to 34 kg each. Surface samples weighed 129 to 145 kg each.

A total of 20 competent pieces of rock were taken from the 22 samples for comminution testing. Half of the 20 rock pieces were selected from the underground adit samples, and half were taken from the surface samples. The rock pieces were combined and then submitted to Phillips Enterprises for crusher work index and abrasion index testing.

After comminution testing samples were taken, each of the 22 samples was stage crushed in entirety to 100%-50mm. Each of the underground adit samples was then blended and split to generate duplicate 1 kg head assay samples. Surface samples were each blended and split to generate duplicate 5 kg splits. Each of the assay splits was then assayed directly using conventional fire assay procedures, to determine gold and silver content. In many cases (low grade samples), the silver grades required that assays be repeated using a four acid digest procedure in order to obtain a more reliable result.

Assay results were reviewed by Dan Peldiak of Coffey Mining, and instructions were issued to blend and split each of the 22 samples and combine splits in order to generate a surface composite, an underground composite, and a master composite. The surface and underground composites were then crushed to 80%-19mm. The 19mm material was blended and split to generate 75 kg for a column leach test, 25 kg for a head screen analysis, triplicate 1 kg splits for head analysis, and 1 kg for further crushing. That 1 kg split was crushed to 80%-1.7mm for bottle roll testing.

Prior to crushing the master composite, a 5 kg split was taken for bottle roll testing (100%-50mm feed size). Remaining material was then crushed to 80%-19mm. The 19mm material was blended and split to generate 75 kg for a column leach test, 25 kg for a head screen analysis, 2 kg for bottle roll testing, triplicate 1 kg splits for head analysis, and 2 kg for further crushing. That 2 kg split was crushed to 80%-6.3mm and then split in half. One half split was further crushed to 80%-1.7mm. Both half splits were then used for bottle roll testing. The triplicate head assay splits from each of the three composites were assayed for gold (fire assay) and silver content (four acid digest).

After initial bottle roll testing was complete, additional sample preparation of the master composite was required. Rejects from the master composite at the 80%-19mm feed size were blended and split to generate an additional 2 kg sample for bottle roll testing and 3 kg for further crushing. That 3 kg split was sequentially crushed, blended, and split to generate 1 kg samples for bottle roll tests (80%-6.3mm and 100%-850µm feed sizes) and for mineralogical analysis (nominal 1.7mm feed size). The sample taken for mineralogical analysis, labeled as "3829 BMC", as well as a sample of bottle roll test tailings, were submitted to DCM Science Laboratories for evaluation.

Composite head assay results and head grade comparisons are presented in Tables 2 and 3. Section sample assay results are given in Section 1 of the Appendix. Composite make-up information, including a description of the samples submitted for comminution testing, is provided in Section 2 of the Appendix. Comminution testing results from Phillips Enterprises are provided in Section 3 of the Appendix. The mineralogical analysis report from DCM Science Laboratories is provided in Section 4 of the Appendix.

Table 2. - Gold and Silver Head Assay Results and Head Grade Comparisons, Longstreet Surface and Underground Composites

	Surface Composite		Underground Composite	
Determination	gAu/mt ore	gAg/mt ore	gAu/mt ore	gAg/mt ore
Direct Assay, Init.	0.21	17	0.70	67
Direct Assay, Dup.	0.67	34	0.82	63
Direct Assay, Trip.	0.37	21	1.09	53
Calc'd., Bottle Roll, 80%-1.7mm	0.31	25	0.83	53
Calc'd., Head Screen	0.34	25	0.82	65
Calc'd., Column	0.36	25	0.78	52
Average	0.38	25	0.84	59
Std. Deviation	0.15	6	0.13	7

Table 3. - Gold and Silver Head Assay Results and Head Grade Comparisons, Longstreet Master Composite

	Head Grade, g/mt ore	
Determination	Au	Ag
Direct Assay, Init.	0.57	40
Direct Assay, Dup.	0.66	41
Direct Assay, Trip.	0.77	50
Calc'd., Bottle Roll, 1.0 gNaCN/L		
100%-50mm	0.70	56
80%-19mm	0.76	39
80%-6.3mm	0.68	44
80%-1.7mm	0.64	40
Calc'd., Bottle Roll, 5.0 gNaCN/L		
80%-19mm	0.72	41
80%-6.3mm	0.58	43
80%-75µm	0.53	33
Calc'd., Head Screen	0.79	47
Calc'd., Column	0.73	48
Average	0.68	44
Std. Deviation	0.08	6

Head assay results and calculated head grades show that the Longstreet composites contained between 0.38 and 0.84 gAu/mt ore. Gold head grade standard deviation ranged from 0.08 to 0.15 gAu/mt ore.

Average silver head grades ranged from 25 to 59 gAg/mt ore. Silver head grade standard deviation ranged from 6 to 7 gAg/mt ore.

In the case of the surface composite, head grade comparisons showed that gold and silver head grade standard deviation was high relative to head grade, and that gold occurrence was somewhat "spotty." The high standard deviation for this composite was due to variability in the direct head assays. Because of the high variability, head assays for all three composites were repeated, and the original results were confirmed.

DIRECT AGITATED CYANIDATION TEST PROCEDURES AND RESULTS

Direct agitated cyanidation (bottle roll) tests were conducted on each composite at a feed size of 80%-1.7mm to determine gold and silver recovery, recovery rate, and reagent requirements. Tests were also conducted on the master composite at feed sizes ranging from 100%-50mm to 80%-1.7mm, and at a cyanide concentration of 1.0 gNaCN/L to determine sensitivity to feed size. Due to the very low silver recoveries observed during initial testing, additional bottle roll tests were conducted on the master composite at feed sizes ranging from 80%-19mm to 80%-75µm, and at a cyanide concentration of 5.0 gNaCN/L to determine response to milling/cyanidation treatment and sensitivity to cyanide concentration.

Ore charges were mixed with water to achieve 40 weight percent solids. In the case of the test conducted at 80%-75µm, a crushed ore sample (100%-850µm) was ground using a laboratory steel ball mill, and then settled and decanted to achieve 40% solids. Natural pulp pH was measured. Lime was added to adjust the pH of the pulps to 11.0 before adding cyanide. Sodium cyanide (either 1.0 or 5.0 gNaCN/L), was then added to the alkaline pulps.

Leaching was conducted by rolling the pulps in bottles on laboratory rolls for 96 hours. Rolling was suspended briefly after 2, 6, 24, 48 and 72 hours to allow the pulps to settle so samples of pregnant solution could be taken for gold and silver analysis by A.A. and ICP methods. Pregnant solution volumes were measured and sampled. Make-up water, equivalent to that withdrawn, was added to the pulps. Cyanide concentrations were restored to initial levels. Lime was added when necessary, to maintain the leaching pH at between 10.8 and 11.2. Rolling was then resumed.

After 96 hours, the pulps were settled to separate liquids and solids. Final pregnant solution volumes were measured and sampled for gold and silver analysis. Final pH and cyanide concentrations were determined. Leached residues were filtered, dried, and assayed in triplicate to determine residual precious metal content.

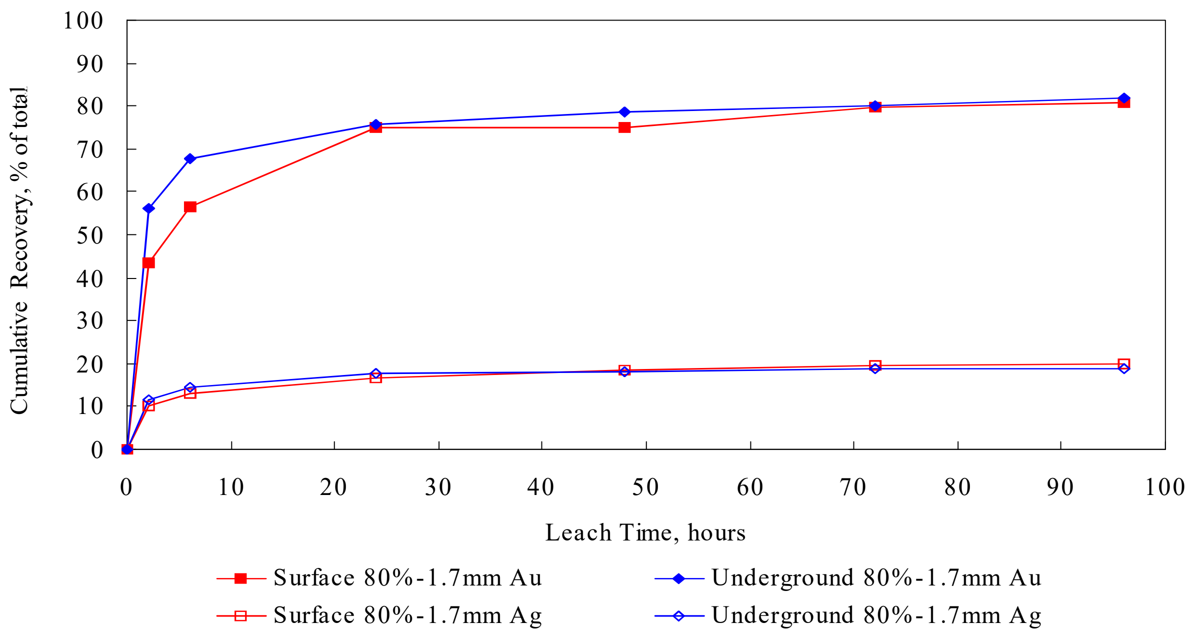
Overall metallurgical results from bottle roll tests are provided in Tables 4 through 6. Corresponding gold leach rate profiles are shown graphically in Figures 1 through 3. Summary BRT results are presented graphically in Figure 4. Detailed bottle roll test data are provided in Section 5 of the Appendix to this report.

Table 4. - Overall Metallurgical Results, Bottle Roll Tests, Longstreet Surface and Underground Composites, 1.0 gNaCN/L

Composite:	Surface		Underground	
Feed Size:	80%-1.7mm		80%-1.7mm	
Metallurgical Results	(CY-2)		(CY-1)	
Extraction: % of total	Au	Ag	Au	Ag
in 2 hours	43.5	10.3	56.0	11.4
in 6 hours	56.6	12.9	67.7	14.5
in 24 hours	75.0	16.6	75.7	17.6
in 48 hours	74.9	18.3	78.6	18.2
in 72 hours	79.7	19.6	79.9	18.9
in 96 hours	80.6	20.0	81.9	18.9
Extracted, gAu/mt ore	0.25	5	0.68	10
Tail Assay, gAu/mt ore[1)]	0.06	20	0.15	43
Calc'd. Head, gAu/mt ore	0.31	25	0.83	53
Average Head, gAu/mt ore[2)]	0.38	25	0.84	59
NaCN Consumed, kg/mt ore	0.08		0.13	
Lime Added, kg/mt ore	2.1		3.4	
Final pH	11.1		11.3	
Natural pH (40% solids)	7.5		5.5	

1) Average of triplicate tail assays.
2) Average of all head grade determinations.

Figure 1. - Gold and Silver Leach Rate Profiles, Bottle Roll Tests, Longstreet Surface and Underground Composites, 1.0 gNaCN/L



Overall metallurgical results show that the surface and underground composites were amenable to direct agitated cyanidation treatment at the 80%-1.7mm feed size. Gold recoveries from the surface and underground composites were 80.6% and 81.9%, respectively in 96 hours of leaching.

Silver recoveries from the surface and underground composites were 20.0% and 18.9%, respectively.

Gold recovery rates were moderate. Gold extraction from the underground composite decreased slightly between 24 and 48 hours. This minor decrease is likely due to analytical variability. The effects of analytical variability are more apparent in low grade solutions such as those generated during leaching of this composite. Silver recovery rates were slow. It does not appear that extending the leach cycle would significantly improve silver recovery.

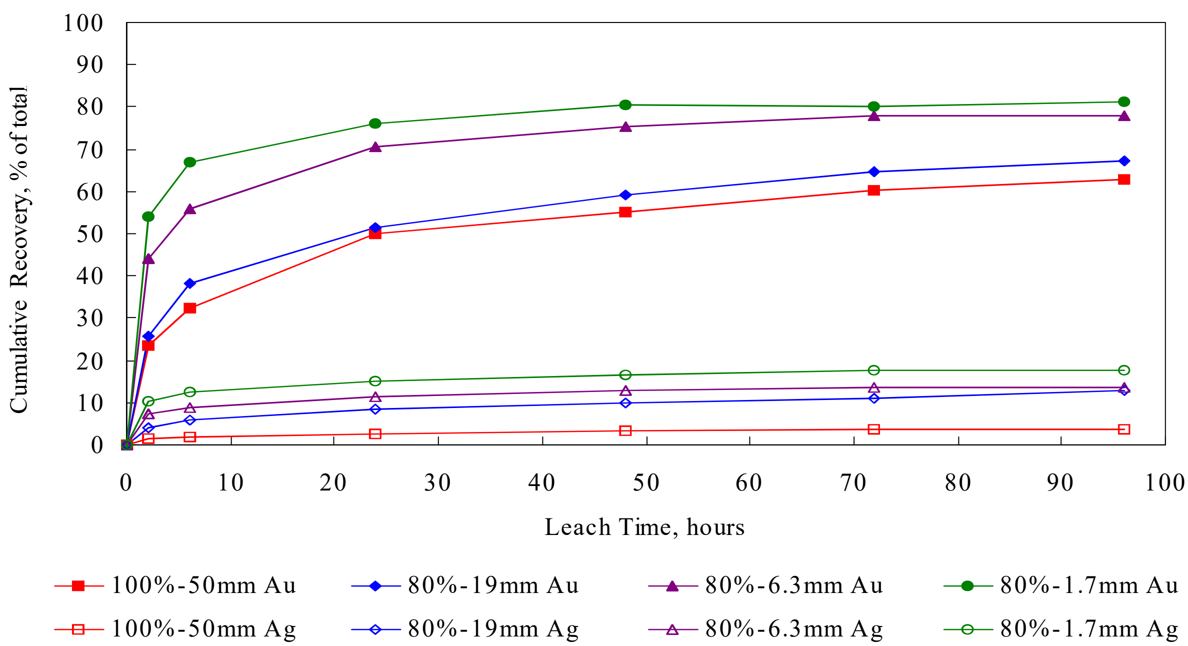
Cyanide consumption for the surface and underground composites was low (0.08 and 0.13 kgNaCN/mt ore, respectively). Lime requirement was low for the surface composite (2.1 kg/mt ore) and moderate for the underground composite (3.4 kg/mt ore).

Table 5. - Overall Metallurgical Results, Bottle Roll Tests, Longstreet Master Composite, 1.0 gNaCN/L

Composite:	Master		Master		Master		Master	
Feed Size:	100%-50mm		80%-19mm		80%-6.3mm		80%-1.7mm	
Metallurgical Results	(CY-4)		(CY-5)		(CY-6)		(CY-3)	
Extraction: % of total	Au	Ag	Au	Ag	Au	Ag	Au	Ag
in 2 hours	23.6	1.4	25.7	4.2	44.1	7.2	53.9	10.4
in 6 hours	32.5	2.0	38.4	6.0	56.0	8.8	67.0	12.4
in 24 hours	50.1	2.7	51.5	8.5	70.7	11.6	76.0	14.9
in 48 hours	55.1	3.3	59.0	10.1	75.2	13.0	80.5	16.6
in 72 hours	60.1	3.6	64.9	11.1	77.9	13.6	80.1	17.5
in 96 hours	62.9	3.6	67.1	12.8	77.9	13.6	81.3	17.5
Extracted, gAu/mt ore	0.44	2	0.51	5	0.53	6	0.52	7
Tail Assay, gAu/mt ore[1)]	0.26	54	0.25	34	0.15	38	0.12	33
Calc'd. Head, gAu/mt ore	0.70	56	0.76	39	0.68	44	0.64	40
Average Head, gAu/mt ore[2)]	0.68	44	0.68	44	0.68	44	0.68	44
NaCN Consumed, kg/mt ore	0.07		0.07		<0.07		0.13	
Lime Added, kg/mt ore	1.3		2.1		3.0		2.5	
Final pH	11.1		11.2		11.0		10.9	
Natural pH (40% solids)	6.6		6.5		6.4		6.3	

1) Average of triplicate tail assays.
2) Average of all head grade determinations.

Figure 2. - Gold and Silver Leach Rate Profiles, Bottle Roll Tests, Longstreet Master Composite, 1.0 gNaCN/L



Overall metallurgical results show that the master composite was amenable to direct agitated cyanidation treatment at feed sizes ranging from 100%-50mm to 80%-1.7mm. Gold recoveries ranged from 62.9% (-50mm) to 81.3% (1.7mm), in 96 hours of leaching at a cyanide concentration of 1.0 gNaCN/L.

Silver recoveries ranged from 12.8% to 17.5% at feed sizes ranging from 80%-19mm to 80%-1.7mm. Silver recovery was significantly lower at the 100%-50mm feed size (3.6%).

Gold recovery rates were slow for the 50mm feed, and increased slightly at each incrementally finer feed size. Gold extraction from the 50mm and 19mm feeds was progressing at a slow, but significant rate when leaching was terminated after 96 hours. It is expected that if leach cycles for these tests were extended, gold recoveries would have approached the recoveries achieved from the 6.3mm and 1.7mm feeds. Silver recovery rates were also slow, however it does not appear that extending the leach cycle would significantly improve silver recovery.

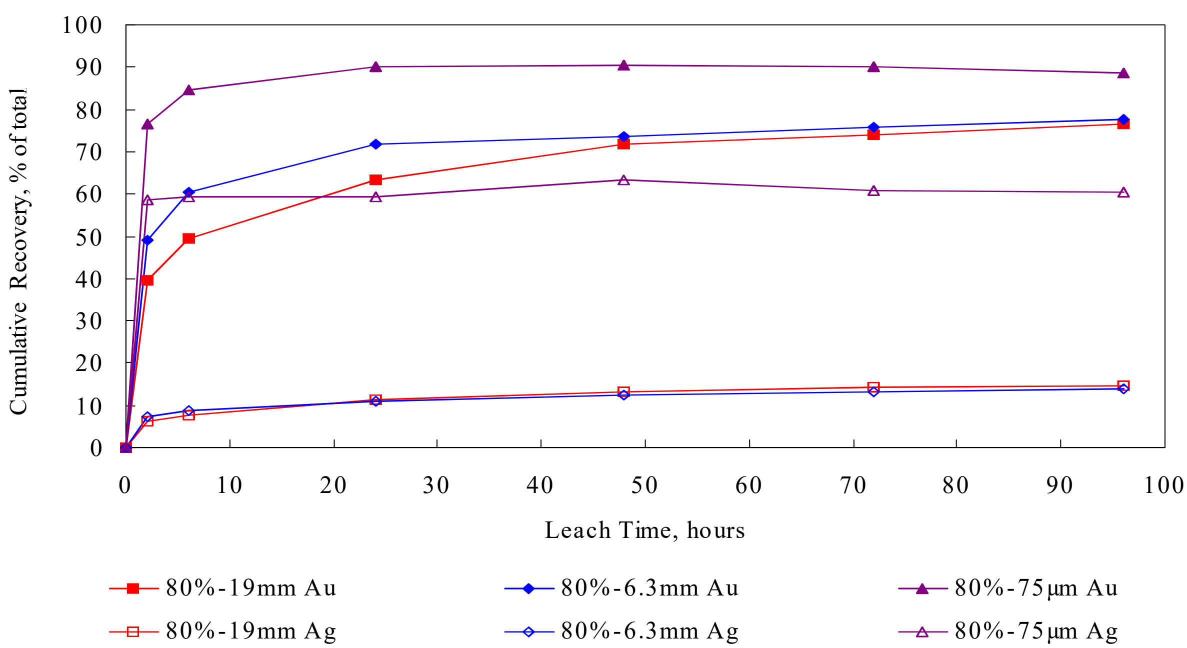
Cyanide consumption for the master composite was low at all feed sizes tested and ranged from <0.07 to 0.13 kgNaCN/mt ore. Lime requirements were low to moderate and ranged from 1.3 to 3.0 kg/mt ore.

Table 6. - Overall Metallurgical Results, Bottle Roll Tests, Longstreet Master Composite, 5.0 gNaCN/L

Composite:	Master		Master		Master	
Feed Size:	80%-19mm		80%-6.3mm		80%-75µm	
Metallurgical Results	(CY-7)		(CY-8)		(CY-9)	
Extraction: % of total	Au	Ag	Au	Ag	Au	Ag
in 2 hours	39.6	6.4	49.1	7.2	76.4	58.7
in 6 hours	49.3	7.8	60.3	8.7	84.6	59.5
in 24 hours	63.4	11.3	71.8	10.9	89.9	59.5
in 48 hours	71.7	13.2	73.7	12.3	90.3	63.3
in 72 hours	74.0	14.4	75.8	13.2	90.2	60.9
in 96 hours	76.4	14.6	77.6	14.0	88.7	60.6
Extracted, gAu/mt ore	0.55	6	0.45	6	0.47	20
Tail Assay, gAu/mt ore[1)]	0.17	35	0.13	37	0.06	13
Calc'd. Head, gAu/mt ore	0.72	41	0.58	43	0.53	33
Average Head, gAu/mt ore[2)]	0.68	44	0.68	44	0.68	44
NaCN Consumed, kg/mt ore	0.48		0.67		0.91	
Lime Added, kg/mt ore	1.0		1.0		1.3	
Final pH	11.0		11.0		11.2	
Natural pH (40% solids)	6.3		6.3		7.0	

1) Average of triplicate tail assays.
2) Average of all head grade determinations.

Figure 3. - Gold and Silver Leach Rate Profiles, Bottle Roll Tests, Longstreet Master Composite, 5.0 gNaCN/L



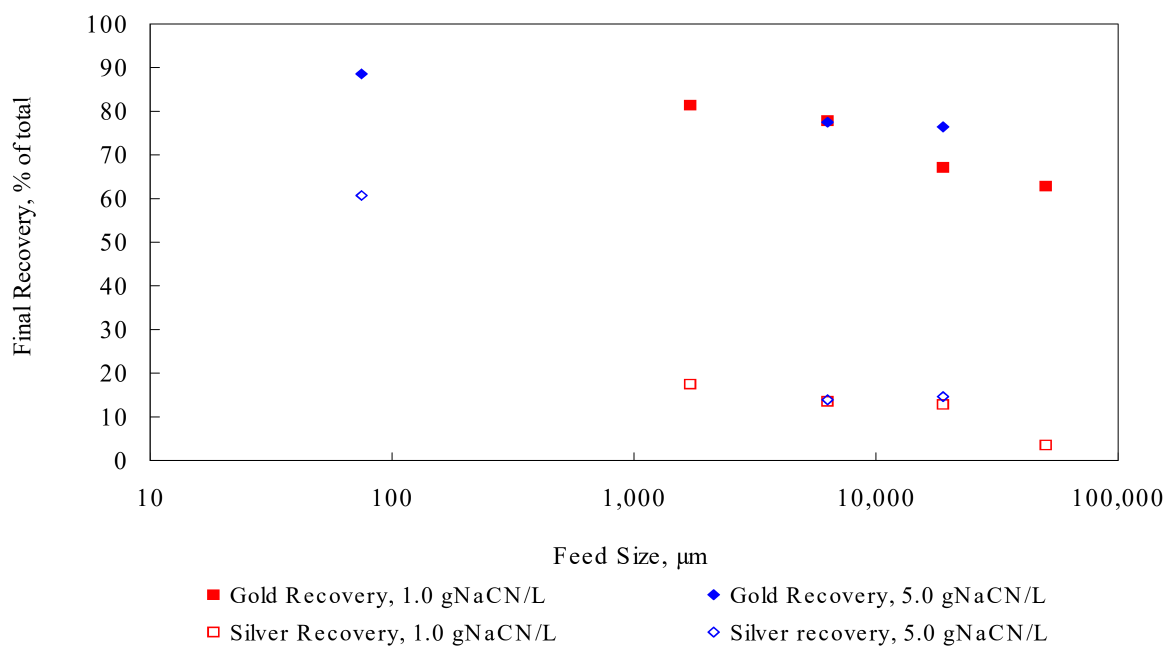
Overall metallurgical results from show that the master composite was readily amenable to direct agitated cyanidation treatment at the 80%-75µm feed size. Gold recovery at this feed size was 88.7%, in 96 hours of leaching, and at a cyanide concentration of 5.0 gNaCN/L. Gold recoveries at the 19mm and 6.3mm feed sizes were 76.4% and 77.6%, respectively.

Silver recoveries at the 19mm and 6.3mm feed sizes were 14.6% and 14.0%, respectively. Silver recovery at the 80%-75µm feed size was significantly higher (60.6%).

Gold and silver recovery rates were moderate at the 19mm and 6.3mm feed sizes. Gold extraction was still progressing at a slow, but significant rate when leach cycles were terminated after 96 hours. It is expected that gold recoveries may be higher if leach cycles were extended beyond 96 hours. Gold and silver recovery rates at the 75µm feed size were rapid, and extraction was essentially complete in the first 2 to 6 hours of leaching. Both gold and silver recovery decreased slightly at times during leaching of the 75µm feed. It is believed that these slight decreases were due to analytical variability.

Cyanide consumption was moderate and ranged from 0.48 to 0.91 kgNaCN/mt ore. Lime requirements were low and ranged from 1.0 to 1.3 kg/mt.

Figure 4. - Gold and Silver Recovery vs. Feed Size, Bottle Roll Tests, Longstreet Master Composite, 1.0 and 5.0 gNaCN/L



Low silver recoveries were observed at feed sizes as fine at 80%-1.7mm, and at a cyanide concentration of 1.0 gNaCN/L. In an effort to improve silver recovery, tests were conducted at feed sizes as fine as 80%-75µm and at an elevated cyanide concentration (5.0 gNaCN/L). Comparing these results shows that decreasing the feed size to 80%-75µm dramatically improved silver recovery. Results also show that increasing the cyanide concentration to 5.0 gNaCN/L likely would not improve gold or silver recovery during heap leaching.

The data show that the master composite was not particularly sensitive to feed size, with respect to silver recovery, in the range of crushed feed sizes tested (-50mm to 1.7mm). Within this range of sizes, silver recovery ranged from 3.6% at the 100%-50mm feed size to 17.5% at the 80%-1.7mm feed size. When fine grinding was employed (80%-75µm), the silver recovery increased substantially to 60.6%.

The overall trend of the bottle roll test recovery vs. feed size data seems to indicate that gold recovery was moderately sensitive to feed size. However this would not likely be the case in a heap leach setting. Gold recovery achieved by column leach testing of the master composite at an 80%-19mm feed size (86.3%) was nearly the same as the bottle roll test recovery achieved at the 80%-75µm feed size (88.7%). Bottle roll test leach rate data (see Figures 2 and 3) show that gold recovery rate was slow, but increased with decreasing feed size and potentially with increasing cyanide concentration. Because bottle roll tests were terminated after 96 hours, gold recovery was limited by the slow leach rates of the tests conducted at coarse feed sizes.

It is believed that increasing the cyanide concentration did not significantly impact the gold or silver recovery. At feed sizes of 80%-6.3mm and 19mm, bottle roll tests were conducted at both 1.0 and 5.0 gNaCN/L concentrations. At the 19mm feed size, gold recovery was slightly higher at the elevated cyanide concentration. This difference is potentially due to an increased leach rate at the higher concentration. Gold recoveries at the 6.3mm feed size, and silver recoveries at both feed sizes were essentially the same, regardless of cyanide concentration.

COLUMN PERCOLATION LEACH TEST PROCEDURES AND RESULTS

Column percolation leach tests were conducted on each composite at an 80%-19mm feed size to determine gold and silver recoveries, recovery rates, and reagent requirements, under simulated heap leaching conditions.

Hydrated lime was mixed with the dry ore charges before column loading procedures. Lime additions were based on bottle roll test lime requirements. Ore charges were placed into the 15 cm diameter by 3 m high PVC leaching columns in a manner to minimize particle segregation and compaction.

Leaching was conducted by applying cyanide solution (1.0 gNaCN/L) over the ore charges at a rate of 12 Lph/m^2 of column cross-sectional area. Pregnant effluent solutions were collected each 24 hour period. Pregnant solution volumes were measured by weighing, and samples were taken for gold and silver analysis using A.A. methods. Cyanide concentration and pH were determined for each pregnant solution. Pregnant solutions were then pumped through a three stage carbon circuit for adsorption of dissolved gold values. Barren solution volumes were measured and sampled for the same analyses. Barren solution, with appropriate make-up reagent, was applied to the ore charges daily.

After leaching, fresh water rinsing was conducted to remove residual cyanide (county requirement) and to recover dissolved gold and silver values. Moisture required to saturate the ore charges (in process solution inventory) and retained moisture were determined. Apparent ore bulk densities were measured before and after leaching.

Drain down rate tests were conducted after rinsing was complete. Tests were conducted by terminating solution application, and at that time, measuring drain volume. Drain volumes were collected and measured periodically by weighing until drain down was complete.

After leaching, rinsing, and draining, residues were removed from the columns and moisture samples were taken immediately. Leached residues were air dried, blended and split to obtain samples for a tail screen analysis. Head and tail screen analyses were conducted, using the same size fractions, to determine residual gold and silver content and distribution, and to obtain recovery by size fraction data.

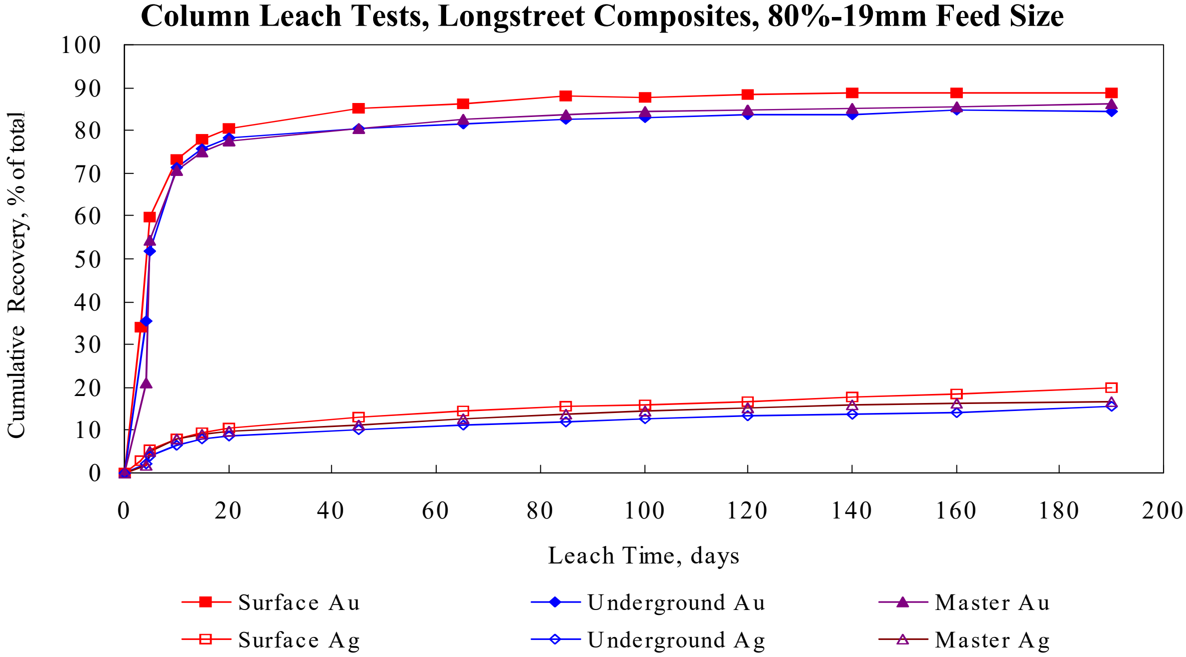
Overall metallurgical results from column tests are shown in Table 7. Gold leach rate profiles are shown graphically in Figure 5. Head and tail screen analysis results, and recovery by size fraction data are provided in Tables 8 through 10. Metallurgical balance data are provided in Table 11. Physical ore characteristics data are provided in Table 12. Detailed column leach test data, including results from drain down rate tests, are provided in Section 6 of the Appendix to this report.

Table 7. - Overall Metallurgical Results, Column Leach Tests, Longstreet Composites, 80%-19mm Feed Size

Composite:	Surface		Underground		Master	
Metallurgical Results	(P-1)		(P-2)		(P-3)	
Extraction: % of total	Au	Ag	Au	Ag	Au	Ag
1st Effluent	34.0	2.8	35.5	2.3	21.1	1.6
in 5 days	59.8	5.5	51.8	3.8	54.4	5.0
in 10 days	73.4	8.1	71.4	6.6	70.5	7.8
in 15 days	77.9	9.4	75.9	8.0	75.1	9.1
in 20 days	80.5	10.4	78.1	8.7	77.6	9.8
in 45 days	85.0	13.0	80.5	10.0	80.5	11.4
in 65 days	86.1	14.4	81.7	11.1	82.6	12.7
in 85 days	88.0	15.4	82.5	11.9	83.7	13.6
in 100 days	87.8	15.8	83.1	12.6	84.3	14.4
in 120 days	88.3	16.8	83.6	13.3	84.9	15.3
in 140 days	88.9	17.7	83.9	13.8	85.3	15.9
in 160 days	88.9	18.3	84.6	14.2	85.7	16.4
End of Leach/Rinse	88.9	20.0	84.6	15.4	86.3	16.7
Extracted, gAu/mt ore	0.32	5	0.66	8	0.63	8
Tail Screen, gAu/mt	0.04	20	0.12	44	0.10	40
Calculated Head, gAu/mt ore	0.36	25	0.78	52	0.73	48
Average Head, gAu/mt ore[1)]	0.38	25	0.84	59	0.68	44
NaCN Consumed, kg/mt ore	1.56		1.93		1.86	
Lime Added, kg/mt ore	1.7		2.7		2.0	
Final Solution pH	10.3		10.4		10.3	
pH After Rinse	10.2		10.5		10.2	
Leach/Rinse Cycle, Days	190		190		190	

1) Average of all head grade determinations.

Figure 5. - Gold and Silver Leach Rate Profiles, Column Leach Tests, Longstreet Composites, 80%-19mm Feed Size



Overall metallurgical results show that the Longstreet composites were readily amenable to simulated heap leaching treatment, at the 80%-19mm feed size. Gold recoveries were similar for all three composites, and ranged from 84.6% to 88.9% in 190 days of leaching and rinsing.

Silver recoveries were also similar for all three composites, and ranged from 15.4% to 20.0%.

Gold leach rates were rapid and gold extraction was essentially complete in the first 30 days of leaching. Silver leach rates were slow, however, it is not expected that extending the leach cycles beyond 190 days would significantly improve recovery.

Cyanide consumption was high for each composite and ranged from 1.56 to 1.93 kgNaCN/mt ore. Cyanide consumption for column leach testing typically is significantly higher than observed during commercial heap leaching. Cyanide consumption was likely driven higher during column testing due to the long leach cycles employed.

The lime additions of 1.7 to 2.7 kg/mt ore were sufficient for maintaining protective alkalinity throughout the leaching cycle.

Table 8. - Head and Tail Screen Analysis Results, and Recovery by Size Fraction Data, Longstreet Surface Composite, 80%-19mm Feed Size

Size Fraction	Weight, %	Cum. Wt., %	Assay, g/mt Au	Assay, g/mt Ag	Distribution Au %	Distribution Au Cum. %	Distribution Ag %	Distribution Ag Cum. %
HEAD SCREEN ANALYSIS RESULTS								
+19mm	20.5	20.5	0.27	27	16.5	16.5	22.1	22.1
-19mm+12.5mm	31.3	51.8	0.35	28	32.6	49.1	35.1	57.2
-12.5mm+6.3mm	23.2	75.0	0.27	24	18.6	67.7	22.3	79.5
-6.3mm+1.7mm	15.1	90.1	0.36	22	16.2	83.9	13.3	92.8
-1.7mm+850µm	4.0	94.1	0.26	21	3.1	87.0	3.4	96.2
-850µm+425µm	1.3	95.4	0.30	19	1.2	88.2	1.0	97.2
-425µm+150µm	1.5	96.9	0.31	17	1.4	89.6	1.0	98.2
-150µm+75µm	0.7	97.6	0.50	16	1.0	90.6	0.4	98.6
-75µm	2.4	100.0	1.32	15	9.4	100.0	1.4	100.0
Composite	100.0		0.34	25	100.0		100.0	
TAIL SCREEN, COLUMN LEACHED RESIDUES (P-1)								
+19mm	19.8	19.8	0.03	18	15.3	15.3	17.8	17.8
-19mm+12.5mm	37.0	56.8	0.04	25	38.0	53.3	46.2	64.0
-12.5mm+6.3mm	21.6	78.4	0.03	20	16.7	70.0	21.6	85.6
-6.3mm+1.7mm	12.1	90.5	0.07	17	21.8	91.8	10.3	95.9
-1.7mm+850µm	2.7	93.2	0.04	16	2.8	94.6	2.1	98.0
-850µm+425µm	1.5	94.7	0.03	11	1.2	95.8	0.8	98.8
-425µm+150µm	1.5	96.2	0.03	9	1.1	96.9	0.7	99.5
-150µm+75µm	0.8	97.0	0.04	6	0.8	97.7	0.2	99.7
-75µm	3.0	100.0	0.03	2	2.3	100.0	0.3	100.0
Composite	100.0		0.04	20	100.0		100.0	

RECOVERY BY SIZE FRACTION DATA, COLUMN LEACH TEST (P-1)

Size Fraction	Weight, % Head	Weight, % Tail	Assay, g/mt Au Head	Assay, g/mt Au Tail	Assay, g/mt Ag Head	Assay, g/mt Ag Tail	Recovery, % Au	Recovery, % Ag
+19mm	20.5	19.8	0.27	0.03	27	18	88.9	33.3
-19mm+12.5mm	31.3	37.0	0.35	0.04	28	25	88.6	10.7
-12.5mm+6.3mm	23.2	21.6	0.27	0.03	24	20	88.9	16.7
-6.3mm+1.7mm	15.1	12.1	0.36	0.07	22	17	80.6	22.7
-1.7mm+850µm	4.0	2.7	0.26	0.04	21	16	84.6	23.8
-850µm+425µm	1.3	1.5	0.30	0.03	19	11	90.0	42.1
-425µm+150µm	1.5	1.5	0.31	0.03	17	9	90.3	47.1
-150µm+75µm	0.7	0.8	0.50	0.04	16	6	92.0	62.5
-75µm	2.4	3.0	1.32	0.03	15	2	97.7	86.7
Composite	100.0	100.0	0.34	0.04	25	20	88.2	19.9

Table 9. - Head and Tail Screen Analysis Results, and Recovery by Size Fraction Data, Longstreet Underground Composite, 80%-19mm Feed Size

Size Fraction	Weight, %	Cum. Wt., %	Assay, g/mt Au	Assay, g/mt Ag	Distribution Au %	Distribution Au Cum. %	Distribution Ag %	Distribution Ag Cum. %
HEAD SCREEN ANALYSIS RESULTS								
+19mm	19.8	19.8	0.85	64	20.5	20.5	19.5	19.5
-19mm+12.5mm	30.8	50.6	0.67	70	25.1	45.6	33.3	52.8
-12.5mm+6.3mm	20.2	70.8	0.65	62	16.0	61.6	19.3	72.1
-6.3mm+1.7mm	14.0	84.8	0.86	74	14.7	76.3	16.0	88.1
-1.7mm+850µm	3.4	88.2	0.83	65	3.4	79.7	3.4	91.5
-850µm+425µm	2.1	90.3	0.79	59	2.0	81.7	1.9	93.4
-425µm+150µm	2.5	92.8	0.78	47	2.4	84.1	1.8	95.2
-150µm+75µm	1.3	94.1	1.04	54	1.6	85.7	1.1	96.3
-75µm	5.9	100.0	1.99	41	14.3	100.0	3.7	100.0
Composite	100.0		0.82	65	100.0		100.0	
TAIL SCREEN, COLUMN LEACHED RESIDUES (P-2)								
+19mm	21.9	21.9	0.11	39	20.9	20.9	19.2	19.2
-19mm+12.5mm	27.4	49.3	0.10	41	23.8	44.7	25.3	44.5
-12.5mm+6.3mm	19.9	69.2	0.13	49	22.5	67.2	22.0	66.5
-6.3mm+1.7mm	14.2	83.4	0.12	64	14.8	82.0	20.5	87.0
-1.7mm+850µm	3.3	86.7	0.12	53	3.4	85.4	3.9	90.9
-850µm+425µm	2.3	89.0	0.12	48	2.4	87.8	2.5	93.4
-425µm+150µm	2.2	91.2	0.12	36	2.3	90.1	1.8	95.2
-150µm+75µm	1.3	92.5	0.12	25	1.4	91.5	0.7	95.9
-75µm	7.5	100.0	0.13	24	8.5	100.0	4.1	100.0
Composite	100.0		0.12	44	100.0		100.0	

RECOVERY BY SIZE FRACTION DATA, COLUMN LEACH TEST (P-2)

Size Fraction	Weight, % Head	Weight, % Tail	Assay, g/mt Au Head	Assay, g/mt Au Tail	Assay, g/mt Ag Head	Assay, g/mt Ag Tail	Recovery, % Au	Recovery, % Ag
+19mm	19.8	21.9	0.85	0.11	64	39	87.1	39.1
-19mm+12.5mm	30.8	27.4	0.67	0.10	70	41	85.1	41.4
-12.5mm+6.3mm	20.2	19.9	0.65	0.13	62	49	80.0	21.0
-6.3mm+1.7mm	14.0	14.2	0.86	0.12	74	64	86.0	13.5
-1.7mm+850µm	3.4	3.3	0.83	0.12	65	53	85.5	18.5
-850µm+425µm	2.1	2.3	0.79	0.12	59	48	84.8	18.6
-425µm+150µm	2.5	2.2	0.78	0.12	47	36	84.6	23.4
-150µm+75µm	1.3	1.3	1.04	0.12	54	25	88.5	53.7
-75µm	5.9	7.5	1.99	0.13	41	24	93.5	41.5
Composite	100.0	100.0	0.82	0.12	65	44	85.4	31.6

Table 10. - Head and Tail Screen Analysis Results, and Recovery by Size Fraction Data, Longstreet Master Composite, 80%-19mm Feed Size

Size Fraction	Weight, %	Cum. Wt., %	Assay, g/mt Au	Assay, g/mt Ag	Distribution Au %	Distribution Au Cum. %	Distribution Ag %	Distribution Ag Cum. %
HEAD SCREEN ANALYSIS RESULTS								
+19mm	16.8	16.8	1.02	43	21.7	21.7	15.3	15.3
-19mm+12.5mm	28.3	45.1	0.42	45	15.0	36.7	27.0	42.3
-12.5mm+6.3mm	20.2	65.3	0.90	47	23.0	59.7	20.1	62.4
-6.3mm+1.7mm	16.4	81.7	0.66	57	13.7	73.4	19.9	82.3
-1.7mm+850µm	4.8	86.5	0.71	53	4.3	77.7	5.4	87.7
-850µm+425µm	3.0	89.5	0.64	48	2.4	80.1	3.1	90.8
-425µm+150µm	2.9	92.4	0.64	44	2.4	82.5	2.7	93.5
-150µm+75µm	1.5	93.9	1.08	37	2.0	84.5	1.2	94.7
-75µm	6.1	100.0	2.01	41	15.5	100.0	5.3	100.0
Composite	100.0		0.79	47	100.0		100.0	
TAIL SCREEN, COLUMN LEACHED RESIDUES (P-3)								
+19mm	21.0	21.0	0.06	41	12.9	12.9	21.3	21.3
-19mm+12.5mm	35.2	56.2	0.13	43	47.0	59.9	37.4	58.7
-12.5mm+6.3mm	20.8	77.0	0.07	35	15.0	74.9	18.0	76.7
-6.3mm+1.7mm	12.0	89.0	0.08	50	9.9	84.8	14.8	91.5
-1.7mm+850µm	2.8	91.8	0.10	46	2.9	87.7	3.2	94.7
-850µm+425µm	1.3	93.1	0.11	37	1.5	89.2	1.2	95.9
-425µm+150µm	1.6	94.7	0.10	29	1.6	90.8	1.2	97.1
-150µm+75µm	1.0	95.7	0.12	22	1.2	92.0	0.6	97.7
-75µm	4.3	100.0	0.18	22	8.0	100.0	2.3	100.0
Composite	100.0		0.10	40	100.0		100.0	

RECOVERY BY SIZE FRACTION DATA, COLUMN LEACH TEST (P-3)

Size Fraction	Weight, % Head	Weight, % Tail	Assay, g/mt Au Head	Assay, g/mt Au Tail	Assay, g/mt Ag Head	Assay, g/mt Ag Tail	Recovery, % Au	Recovery, % Ag
+19mm	16.8	21.0	1.02	0.06	43	41	94.1	4.7
-19mm+12.5mm	28.3	35.2	0.42	0.13	45	43	69.0	4.4
-12.5mm+6.3mm	20.2	20.8	0.90	0.07	47	35	92.2	25.5
-6.3mm+1.7mm	16.4	12.0	0.66	0.08	57	50	87.9	12.3
-1.7mm+850µm	4.8	2.8	0.71	0.10	53	46	85.9	13.2
-850µm+425µm	3.0	1.3	0.64	0.11	48	37	82.8	22.9
-425µm+150µm	2.9	1.6	0.64	0.10	44	29	84.4	34.1
-150µm+75µm	1.5	1.0	1.08	0.12	37	22	88.9	40.5
-75µm	6.1	4.3	2.01	0.18	41	22	91.0	46.3
Composite	100.0	100.0	0.79	0.10	47	40	87.3	14.2

Head screen analysis results showed that the Longstreet composites contained 0.34 to 0.82 gAu/mt ore and 25 to 65 gAg/mt ore. Contained gold and silver values generally were fairly evenly distributed throughout the various size fractions, with a moderate enrichment of gold values in the fines (-150µm). Size fraction assays for the master composite were somewhat "spotty".

Tail screen analysis results showed that the leached residues contained 0.04 to 0.12 gAu/mt ore and 20 to 44 gAg/mt ore. Residual gold values generally were fairly evenly distributed throughout the various size fractions. Silver values in the leach residues were not evenly distributed and a minor to moderate depletion of silver values was noted in the finer size fractions.

Recovery by size fraction data indicate that finer crushing or grinding would not substantially improve gold recovery. Gold recovery generally was similar throughout the various size fractions with only a slightly elevated recovery noted in the finest size fraction (-75µm).

Recovery by size fraction data indicate that fine grinding would likely be required to maximize silver recovery from the surface and master composites. Silver recovery by size fraction data for the underground composite show that silver recovery was similar throughout the various size fractions, and that fine grinding may not significantly improve silver recovery from this composite.

Table 11. - Metallurgical Balances, Column Leach Tests, Longstreet Composites, 80%-19mm Feed Size

	Metallurgical Balance		
	Sol. vs. Tail	Carbon vs. Tail	Head vs. Tail[2]
Surface Composite (P-1)			
Extracted, gAu/mt ore	0.32	0.33	0.34
Tail Assay, gAu/mt	0.04	0.04	0.04
Calculated, Head, gAu/mt	0.36	0.37	0.38
Recovery, %	88.9	89.2	89.5
Deviation, g/mt[1]	N/A	0.01	0.02
Precision, %	100.0	97.2	94.4
Underground Composite (P-2)			
Extracted, gAu/mt ore	0.66	0.69	0.72
Tail Assay, gAu/mt	0.12	0.12	0.12
Calculated, Head, gAu/mt	0.78	0.81	0.84
Recovery, %	84.6	85.2	85.7
Deviation, g/mt[1]	N/A	0.03	0.06
Precision, %	100.0	96.2	92.3
Master Composite (P-3)			
Extracted, gAu/mt ore	0.63	0.63	0.58
Tail Assay, gAu/mt	0.10	0.10	0.10
Calculated, Head, gAu/mt	0.73	0.73	0.68
Recovery, %	86.3	86.3	85.3
Deviation, g/mt[1]	N/A	<0.01	0.05
Precision, %	100.0	>98.6	93.2

1) Deviation from solution versus tail balance.
2) Calculated, based on average of all head grades and tail screen results.

Solution versus tail and loaded carbon versus tail metallurgical balances agreed closely. Deviation between the two balances was 0.03 gAu/mt ore or less. Head versus tail metallurgical balances agreed closely as well. Deviation between these and the solution versus tail balances ranged from 0.02 to 0.06 gAu/mt ore. These deviations are all within normally expected experimental and analytical precision limits for column leach tests. The solution versus tail balance is considered the most reliable because of the number of check analyses performed on column test pregnant solutions. That balance was used for all percent recovery calculations.

Table 12. - Physical Ore Characteristics Data, Column Leach Tests, Longstreet Composites

Composite	Feed Size	Test No.	Ore Charge, kg	Moisture, wt. % As Rec'd.	Moisture, wt. % To Saturate*	Moisture, wt. % Retained	Apparent Bulk Density, mt ore/m^3 Before	Apparent Bulk Density, mt ore/m^3 After
Surface	80%-19mm	P-1	71.97	0.1	14.3	6.8	1.35	1.36
Underground	80%-19mm	P-2	71.75	0.1	21.5	11.6	1.35	1.35
Master	80%-19mm	P-3	71.95	0.1	14.5	9.8	1.36	1.36

* Calculated on a dry ore weight basis.

Physical ore characteristics data show that little or no "slumping" of charges occurred during leaching. Moisture requirements were not unusual for 19mm feeds. No solution percolation, fines migration or solution channeling problems were encountered during leaching.

CONCLUSIONS

- Each of the three Longstreet composites was readily amenable to simulated heap leach cyanidation treatment at an 80%-19mm feed size. Gold recoveries of 84.6% to 88.9% were achieved.

- Column test silver recoveries were low and ranged from 15.4% to 20.0%.

- Gold recovery rates, during column leach testing, were rapid. Silver recovery rates were slow.

- Bottle roll test results and column test recovery by size fraction data indicate that fine grinding would likely be required to maximize silver recovery. A silver recovery of 60.6% was achieved by milling/cyanidation treatment (80%-75µm feed size).

- Results indicate that, within the range of feed sizes tested, the master composite was not particularly sensitive to feed size, with respect to gold recovery, given a sufficiently long leach cycle.

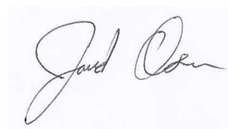
- Increasing the cyanide concentration from 1.0 to 5.0 gNaCN/L did not significantly improve silver bottle roll test recoveries at the 19mm or 6.3mm feed sizes.

- Cyanide consumption during column leach testing was high and ranged from 1.56 to 1.93 kgNaCN/mt ore. Cyanide consumption was significantly lower during bottle roll testing, and ranged from <0.07 to 0.13 kgNaCN/mt ore when a cyanide concentration of 1.0 gNaCN/L was used.

- Lime requirements generally were low.

RECOMMENDATIONS

We recommend that load/permeability testing be conducted on column leached residue samples to confirm permeability under simulated commercial heap leach stack height compressive loadings.



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APPENDIX

Section 1 - Section Sample Assay Results

Section 2 - Composite Make-up Information

Section 3 - Comminution Testing Results

Section 4 - Mineralogical Analysis Report

Section 5 - Detailed Bottle Roll Test Results

Section 6 - Detailed Column Leach Test Results

APPENDIX

Section 1 - Section Sample Assay Results

Table A1-1. - Gold and Silver Head Assay Results, Longstreet Mine, Section Samples

	Au, g/mt ore			Ag, g/mt ore		
Sample	Init.	Dup.	Average	Init.	Dup.	Average
LUA 10'	0.93	0.83	0.88	66	110	88
LUA 20'	2.10	1.89	2.00	173	125	149
LUA 30'	1.91	2.22	2.07	141	177	159
LUA 40'	2.71	3.28	2.99	182	214	198
LUA 50'	3.09	3.18	3.14	202	281	242
LUA 60'	2.65	3.86	3.25	117	89	103
LUA 180' to 190'	0.10	0.06	0.08	11	9	10
LUA 190' to 200'	0.09	0.07	0.08	8	10	9
LUA 200' to 210'	0.39	0.36	0.37	16	14	15
LUA 210' to 220'	0.24	0.17	0.20	7	5	6
LUA 220' to 230'	0.15	0.21	0.18	4	4	4
LUA 230' to 240'	0.29	0.23	0.26	17	13	15
LUA 240' to 250'	0.33	0.38	0.36	20	21	21
LUA 250' to 260'	0.24	0.56	0.40	8	11	10
LUA 260' to 270'	0.28	0.21	0.24	11	8	10
LUA 270' to 280'	0.16	0.20	0.18	7	8	8
LUA 280' to 290'	0.24	0.29	0.27	6	7	7
LUA 290' to 300'	0.10	0.15	0.12	5	6	6
LUA 300' to 310'	0.28	0.27	0.27	6	7	7
LS1	0.16	0.10	0.13	12	11	12
LS2	0.25	0.35	0.30	14	15	15
LS3	0.61	0.48	0.54	34	32	33

APPENDIX

Section 2 - Composite Make-up Information

Table A2-1. - Composite Make-up Information, Longstreet Project, Underground Adit Sample at 10' (LUA 10')

Sample ID	Intervals, ft		Weight to Comp.	
	From	To	kg	%
LUA 1 OF 3	10	-	*6.05	30.8
LUA 2 OF 2	10	-	6.51	33.1
LUA 3 OF 3	10	-	7.10	36.1
Composite Total			**19.66**	**100.0**

*Comminution sample taken

Table A2-2. - Composite Make-up Information, Longstreet Project, Underground Adit Sample at 20' (LUA 20')

Sample ID	Intervals, ft		Weight to Comp.	
	From	To	kg	%
LUA 1 OF 2	20	-	4.29	51.0
LUA 2 OF 2	20	-	*4.12	49.0
Composite Total			**8.41**	**100.0**

*Comminution sample taken

Table A2-3. - Composite Make-up Information, Longstreet Project, Underground Adit Sample at 30' (LUA 30')

Sample ID	Intervals, ft		Weight to Comp.	
	From	To	kg	%
LUA 1 OF 2	30	-	*4.30	39.4
LUA 2 OF 2	30	-	6.61	60.6
Composite Total			**10.91**	**100.0**

*Comminution sample taken

Table A2-4. - Composite Make-up Information, Longstreet Project, Underground Adit Sample at 40' (LUA 40')

Sample ID	Intervals, ft		Weight to Comp.	
	From	To	kg	%
LUA 1 OF 3	40	-	6.31	35.9
LUA 2 OF 3	40	-	*5.71	32.5
LUA 3 OF 3	40	-	5.55	31.6
Composite Total			**17.57**	**100.0**

*Comminution sample taken

Table A2-5. - Composite Make-up Information, Longstreet Project, Underground Adit Sample at 50' (LUA 50')

Sample ID	Intervals, ft From	Intervals, ft To	Weight to Comp. kg	Weight to Comp. %
LUA 1 OF 3	50	-	*4.85	35.1
LUA 2 OF 3	50	-	4.99	36.1
LUA 3 OF 3	50	-	3.98	28.8
Composite Total			**13.82**	**100.0**

*Comminution sample taken

Table A2-6. - Composite Make-up Information, Longstreet Project, Underground Adit Sample at 60' (LUA 60')

Sample ID	Intervals, ft From	Intervals, ft To	Weight to Comp. kg	Weight to Comp. %
LUA 1 OF 3	60	-	*5.88	33.0
LUA 2 OF 3	60	-	5.68	31.8
LUA 3 OF 3	60	-	6.28	35.2
Composite Total			**17.84**	**100.0**

*Comminution sample taken

Table A2-7. - Composite Make-up Information, Longstreet Project, Underground Adit Sample at 180' to 190' (LUA 180' to 190')

Sample ID	Intervals, ft From	Intervals, ft To	Weight to Comp. kg	Weight to Comp. %
LUA 1 OF 4	180	190	5.36	26.6
LUA 2 OF 4	180	190	7.43	36.8
LUA 3 OF 4	180	190	*4.43	22.0
LUA 4 OF 4	180	190	2.95	14.6
Composite Total			**20.17**	**100.0**

*Comminution sample taken

Table A2-8. - Composite Make-up Information, Longstreet Project, Underground Adit Sample at 190' to 200' (LUA 190' to 200')

	Intervals, ft		Weight to Comp.	
Sample ID	From	To	kg	%
LUA 1 OF 3	190	200	5.04	31.6
LUA 2 OF 3	190	200	4.94	31.0
LUA 3 OF 3	190	200	5.95	37.4
Composite Total			**15.93**	**100.0**

Table A2-9. - Composite Make-up Information, Longstreet Project, Underground Adit Sample at 200' to 210' (LUA 200' to 210')

	Intervals, ft		Weight to Comp.	
Sample ID	From	To	kg	%
LUA 1 OF 4	200	210	*4.80	25.5
LUA 2 OF 4	200	210	5.17	27.5
LUA 3 OF 4	200	210	5.13	27.3
LUA 4 OF 4	200	210	3.70	19.7
Composite Total			**18.8**	**100.0**

*Comminution sample taken

Table A2-10. - Composite Make-up Information, Longstreet Project, Underground Adit Sample at 210' to 220' (LUA 210' to 220')

	Intervals, ft		Weight to Comp.	
Sample ID	From	To	kg	%
LUA 1 OF 4	210	220	*5.23	25.3
LUA 2 OF 4	210	220	6.56	31.7
LUA 3 OF 4	210	220	5.09	24.6
LUA 4 OF 4	210	220	3.82	18.5
Composite Total			**20.7**	**100.0**

*Comminution sample taken

Table A2-11. - Composite Make-up Information, Longstreet Project, Underground Adit Sample at 220' to 230' (LUA 220' to 230')

	Intervals, ft		Weight to Comp.	
Sample ID	From	To	kg	%
LUA 1 OF 3	220	230	6.04	42.4
LUA 2 OF 3	220	230	5.41	38.0
LUA 3 OF 3	220	230	2.78	19.5
Composite Total			**14.23**	**100.0**

Table A2-12. - Composite Make-up Information, Longstreet Project, Underground Adit Sample at 230' to 240' (LUA 230' to 240')

	Intervals, ft		Weight to Comp.	
Sample ID	From	To	kg	%
LUA 1 OF 6	230	240	4.60	13.4
LUA 2 OF 6	230	240	5.74	16.7
LUA 3 OF 6	230	240	5.55	16.1
LUA 4 OF 6	230	240	5.42	15.7
LUA 5 OF 6	230	240	7.37	21.4
LUA 6 OF 6	230	240	5.75	16.7
Composite Total			**34.43**	**100.0**

Table A2-13. - Composite Make-up Information, Longstreet Project, Underground Adit Sample at 240' to 250' (LUA 240' to 250')

	Intervals, ft		Weight to Comp.	
Sample ID	From	To	kg	%
LUA 1 OF 3	240	250	*5.16	26.2
LUA 2 OF 3	240	250	7.25	36.8
LUA 3 OF 3	240	250	7.30	37.0
Composite Total			**19.71**	**100.0**

*Comminution sample taken

Table A2-14. - Composite Make-up Information, Longstreet Project, Underground Adit Sample at 250' to 260' (LUA 250' to 260')

	Intervals, ft		Weight to Comp.	
Sample ID	From	To	kg	%
LUA 1 OF 3	250	260	6.10	37.5
LUA 2 OF 3	250	260	5.45	33.5
LUA 3 OF 3	250	260	4.72	29.0
Composite Total			**16.27**	**100.0**

Table A2-15. - Composite Make-up Information, Longstreet Project, Underground Adit Sample at 260' to 270' (LUA 260' to 270')

	Intervals, ft		Weight to Comp.	
Sample ID	From	To	kg	%
LUA 1 OF 4	260	270	5.80	25.7
LUA 2 OF 4	260	270	5.57	24.6
LUA 3 OF 4	260	270	6.00	26.5
LUA 4 OF 4	260	270	5.23	23.1
Composite Total			**22.6**	**100.0**

Table A2-16. - Composite Make-up Information, Longstreet Project, Underground Adit Sample at 270' to 280' (LUA 270' to 280')

	Intervals, ft		Weight to Comp.	
Sample ID	From	To	kg	%
LUA 1 OF 3	270	280	6.33	42.1
LUA 2 OF 3	270	280	5.61	37.3
LUA 3 OF 3	270	280	3.11	20.7
Composite Total			**15.05**	**100.0**

Table A2-17. - Composite Make-up Information, Longstreet Project, Underground Adit Sample at 280' to 290' (LUA 280' to 290')

	Intervals, ft		Weight to Comp.	
Sample ID	From	To	kg	%
LUA 1 OF 3	280	290	5.53	34.1
LUA 2 OF 3	280	290	6.35	39.1
LUA 3 OF 3	280	290	4.35	26.8
Composite Total			**16.23**	**100.0**

Table A2-18. - Composite Make-up Information, Longstreet Project, Underground Adit Sample at 290' to 300' (LUA 290' to 300')

	Intervals, ft		Weight to Comp.	
Sample ID	From	To	kg	%
LUA 1 OF 4	290	300	5.69	26.4
LUA 2 OF 4	290	300	6.49	30.1
LUA 3 OF 4	290	300	7.03	32.6
LUA 4 OF 4	290	300	2.38	11.0
Composite Total			**21.59**	**100.0**

Table A2-19. - Composite Make-up Information, Longstreet Project, Underground Adit Sample at 300' to 310' (LUA 300' to 310')

	Intervals, ft		Weight to Comp.	
Sample ID	From	To	kg	%
LUA 1 OF 5	300	310	5.62	20.3
LUA 2 OF 5	300	310	6.63	23.9
LUA 3 OF 5	300	310	5.49	19.8
LUA 4 OF 5	300	310	5.00	18.0
LUA 5 OF 5	300	310	4.99	18.0
Composite Total			**27.73**	**100.0**

Table A2-20. - Composite Make-up Information, Longstreet Project, Surface Sample 1 (LS1)

	Intervals, ft		Weight to Comp.	
Sample ID	From	To	kg	%
LS-#1 1 OF 6	-	-	*19.26	15.2
LS-#1 2 OF 6	-	-	*20.87	16.5
LS-#1 3 OF 6	-	-	24.61	19.4
LS-#1 4 OF 6	-	-	*19.81	15.6
LS-#1 5 OF 6	-	-	19.88	15.7
LS-#1 6 OF 6	-	-	22.34	17.6
Composite Total			**126.77**	**100.0**

*Comminution sample taken

Table A2-21. - Composite Make-up Information, Longstreet Project, Surface Sample 2 (LS2)

	Intervals, ft		Weight to Comp.	
Sample ID	From	To	kg	%
LS-#2 1 OF 6	-	-	*20.74	14.5
LS-#2 2 OF 6	-	-	*22.49	15.7
LS-#2 3 OF 6	-	-	*26.44	18.5
LS-#2 4 OF 6	-	-	*23.96	16.8
LS-#2 5 OF 6	-	-	24.38	17.1
LS-#2 6 OF 6	-	-	24.85	17.4
Composite Total			**142.86**	**100.0**

*Comminution sample taken

Table A2-22. - Composite Make-up Information, Longstreet Project, Surface Sample 3 (LS3)

	Intervals, ft		Weight to Comp.	
Sample ID	From	To	kg	%
LS-#3 1 OF 6	-	-	*20.88	15.2
LS-#3 2 OF 6	-	-	*22.77	16.5
LS-#3 3 OF 6	-	-	25.18	18.3
LS-#3 4 OF 6	-	-	*20.24	14.7
LS-#3 5 OF 6	-	-	24.72	18.0
LS-#3 6 OF 6	-	-	23.83	17.3
Composite Total			**137.62**	**100.0**

*Comminution sample taken

Table A2-23. - Composite Make-up Information, Longstreet Project, Underground Master Composite (UMC)

Sample ID	Weight to Comp. kg	Weight to Comp. %
LUA 10'	11.18	5.5
LUA 20'	6.36	3.1
LUA 30'	8.78	4.3
LUA 40'	11.07	5.5
LUA 50'	11.07	5.5
LUA 60'	11.09	5.5
LUA 180' to 190'	10.89	5.4
LUA 190' to 200'	10.99	5.4
LUA 200' to 210'	10.93	5.4
LUA 210' to 220'	10.94	5.4
LUA 220' to 230'	11.06	5.5
LUA 230' to 240'	11.01	5.4
LUA 240' to 250'	11.00	5.4
LUA 250' to 260'	11.01	5.4
LUA 260' to 270'	11.00	5.4
LUA 270' to 280'	10.90	5.4
LUA 280' to 290'	10.94	5.4
LUA 290' to 300'	10.96	5.4
LUA 300' to 310'	11.03	5.5
Composite Total	**202.21**	**100.0**

Table A2-24. - Composite Make-up Information, Longstreet Project, Surface Master Composite (SMC)

Sample ID	Weight to Comp. kg	Weight to Comp. %
LS1	64.94	33.5
LS2	64.59	33.3
LS3	64.56	33.3
Composite Total	**194.09**	**100.0**

Table A2-25. - Composite Make-up Information, Longstreet Project, Blended Master Composite (BMC)

Sample ID	Weight to Comp. kg	Weight to Comp. %
UMC	73.70	54.4
SMC	61.80	45.6
Composite Total	**135.50**	**100.0**

Table A2-26. - Composite Make-up Information, Longstreet Project, Comminution Testing Composite, 50mm to 75mm Rock Pieces

	Weight to Comp.	
Sample	kg	%
LUA 10'	0.45	3.5
LUA 20'	0.64	5.0
LUA 30'	0.49	3.8
LUA 40'	0.56	4.4
LUA 50'	0.67	5.3
LUA 60'	0.77	6.0
LUA 180' - 190'	0.63	4.9
LUA 200' - 210'	0.56	4.4
LUA 210' - 220'	0.36	2.8
LUA 240' - 250'	0.96	7.5
LS1	0.59	4.6
LS1	0.71	5.6
LS1	0.78	6.1
LS2	0.58	4.6
LS2	0.43	3.4
LS2	0.80	6.3
LS2	0.56	4.4
LS3	0.92	7.2
LS3	0.78	6.1
LS3	0.49	3.8
Composite Total	**12.73**	**100.0**

APPENDIX

Section 3 - Comminution Testing Results

⋱ **PHILLIPS ENTERPRISES, LLC** ⫽
Metallurgical Testing and Consulting Services

Mailing Address:
2501 Braun Dr.
Golden, CO 80401
(303) 279-0443

Laboratory and Shipping:
5946 McIntyre Street
Golden, CO 80403
Phone: (303) 854-2037
Fax: (303) 216-0258
E-mail: phillips81@att.net

August 16, 2013

Jared Olson
Project Engineer
MLI
1016 Greg St.
Sparks, NV 89431

Subject: Comminution Tests
Reference: Project 3829; Longstreet Mine
Phillips Project No.: 133017

Dear Mr. Olson:

Phillips Enterprises, LLC has completed a crusher work index test and an abrasion index test for your Project 3829. The sample was delivered on July 31, 2013.

Sample Preparation

No preparation was required for the crusher test sample. Pieces were natural rock. Fragments were used for the abrasion test.

The abrasion test sample was crushed and screened to extract a ¾"x ½" size fraction.

Crusher Work Index Test

The crusher work index test was conducted on a natural rock pieces according to test protocol.

Sample	CWi (kW-hr/st)	CWi (kW-hr/mt)
Longstreet Mine	10.08	11.11

Abrasion Index Test

An abrasion index test was conducted on a -3/4”+1/2” fraction of the sample according to test protocol.

Sample	**Abr. Index**
Longstreet Mine	0.2431

Data pages are attached for all tests. Please feel welcome to contact us if you have questions.

The sample rejects and products will be returned to MLI in the near future.

Sincerely,

Robert J. Phillips
Owner/manager

APPENDIX

Section 4 - Mineralogical Analysis Report

DCM SCIENCE LABORATORY, INC.

December 23, 2013

Mr. Jared Olson
McClelland Laboratories, Inc.
1016 Greg Street
Sparks, NV 89431

Dear Mr. Olson:

We have performed analyses of two leach samples (client samples **3829 BMC Mineralogy** and **3829 CY-7**). The results are outlined in the following report.

Thank you for the opportunity to provide this service. If you have any questions, please call.

Sincerely,

Ron Schott

Ron Schott
Laboratory Director

12421 W. 49th Ave. ● Unit 6 ● Wheat Ridge, Colorado 80033
303-463-8270 ● Fax 303-463-8267 ● 800-852-7340
www.dcmsciencelab.com

12421 W. 49th Avenue, Unit #6
Wheat Ridge, CO 80033 (303) 463-8270

Petrographic, Scanning Electron Microscopy and X-Ray Diffraction Analysis

Client:
McClelland Laboratories, Inc.
1016 Greg Street
Sparks, NV 89431

Analysis Date:	12-20-13
Reporting Date:	12-23-13
Receipt Date:	12-13-13
Client Job No.:	3829
Project Title:	None Given
DCMSL Project:	MCCL17,18,20

The purpose of this study is to determine the bulk mineralogy of two leach samples (client samples **3829 BMC Mineralogy** and **3829 CY-7**) with an emphasis on Au/Ag mineralogy. Each sample was prepared as a standard polished thin section for study by transmitted/reflected light microscopy and scanning electron microscopy (SEM) equipped with an energy dispersive system (EDS). In addition both samples were prepared as standard powder packs for analysis by x-ray diffraction (XRD). Color photomicrographs, SEM images and spectra are included for documentation of relevant features.

Mineral Assemblage

Petrographic, SEM and XRD analyses indicate the bulk mineralogy in both samples is essentially the same, therefore the mineralogy will be discussed together under individual category headings.

Silicate Mineralogy

In thin section silica mineralogy dominates both samples and is contained in fragments of porphyritic rhyolite. Quartz is the dominant phase and occurs in several habits. Secondary quartz seen filling fractures generally has a granular, mosaic texture with a grain size up to 100 µm. In the rhyolite matrix quartz takes on bipyramidal outlines that generally show deeply embayed margins. These grains float in a very fine grained matrix of quartz/feldspar and measure up to 1 mm in size. In the presence of vugs quartz takes on euhedral and prismatic outlines. Many of the rhyolite fragments are in part glassy and show vesicular glass structures preserved by divitrification and replacement by fine grained quartz. Sanidine feldspar occurs as subhedral to euhedral water clear phenocrysts. Grain size varies greatly from 20 µm laths to larger phenocrysts over 1.5 mm. Feldspar spherulites are also a common feature. Along some fractures intermingled with granular quartz, small grains of secondary adularia are also present. Clay mineralogy is present in low amounts and is primarily vermicular kaolinite that is seen filling small vugs. Some of the sanidine and matrix glass show mild replacement by a fine grained, brown colored clay with a sinuous habit.

Oxide Mineralogy

Both samples contain low amounts of oxide with hematite and goethite as the main types. Hematite occurs as small rosettes, thin strings and small pockets. Goethite is generally seen as euhedral pseudomorphs after pyrite. Yellow limonitic iron oxide is in the form of irregularly shaped masses or intermixed with kaolinite. Secondary rutile forms small aggregates and honey colored prisms in quartz.

Sulfate Mineralogy

Sulfates are well represented with jarosite as the main type. Jarosite occurs as granular masses mixed with iron oxide or as pseudomorphs after pyrite. Jarosite is also seen filling fractures that cross cut rock fragments. Barite is present as a trace and occurs as small inclusions up to 2 µm in quartz.

Phosphate Mineralogy

Phosphates are present as a trace and are mainly apatite and lesser amounts of a monazite mineral carrying typical rare earth chemistry. The majority of grains are locked in quartz/feldspar and measure up to 5 µm.

Sulfide Mineralogy

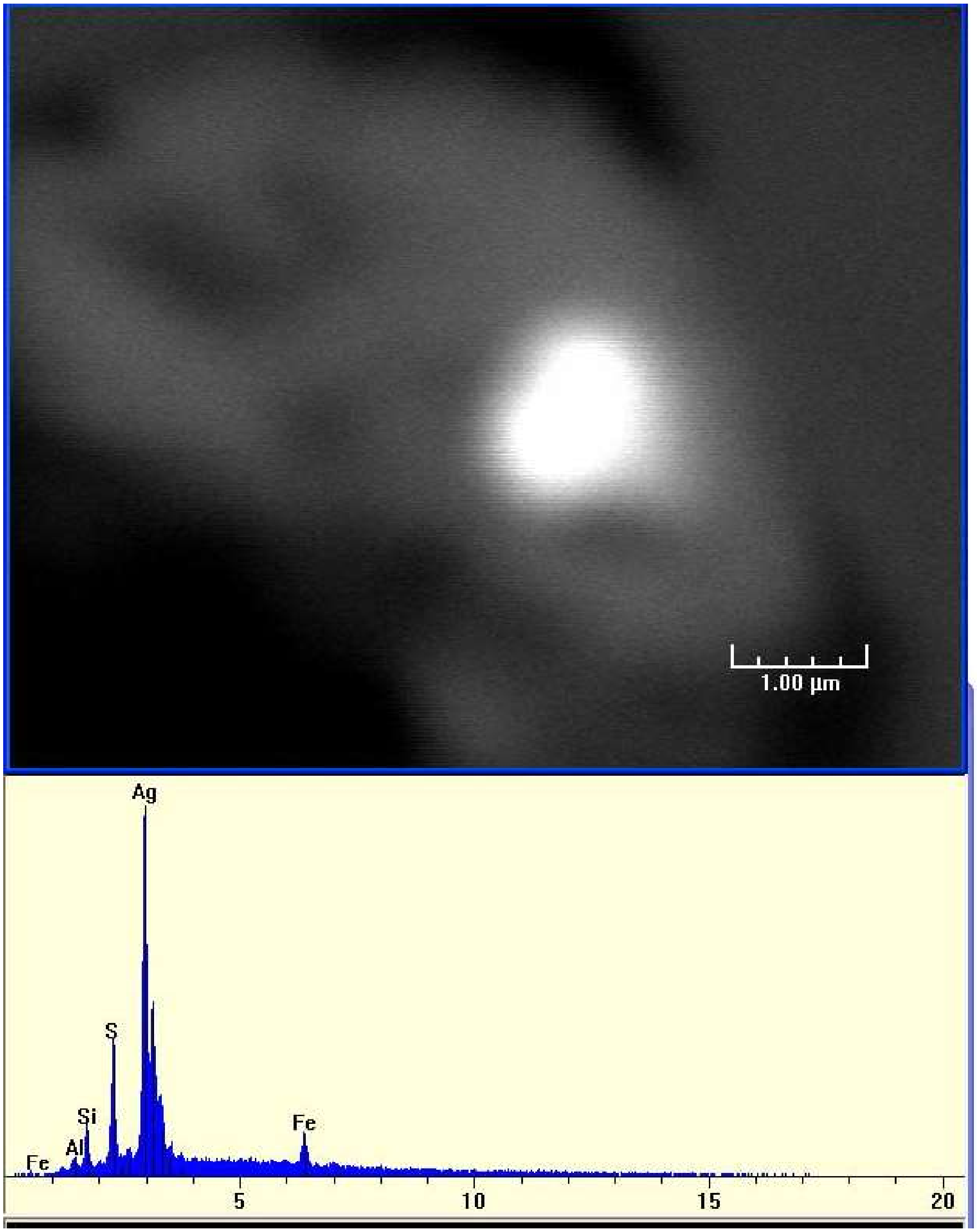
Sulfides are present as a trace with pyrite as the main type. Pyrite occurs as minute cubes and drop-like grains that vary in size from <1 µm up to approximately 20 µm. Most grains are unaltered but a small population wear thin goethite jackets. A trace of chalcopyrite is present and shows no apparent decay.

Au/Ag Mineralogy

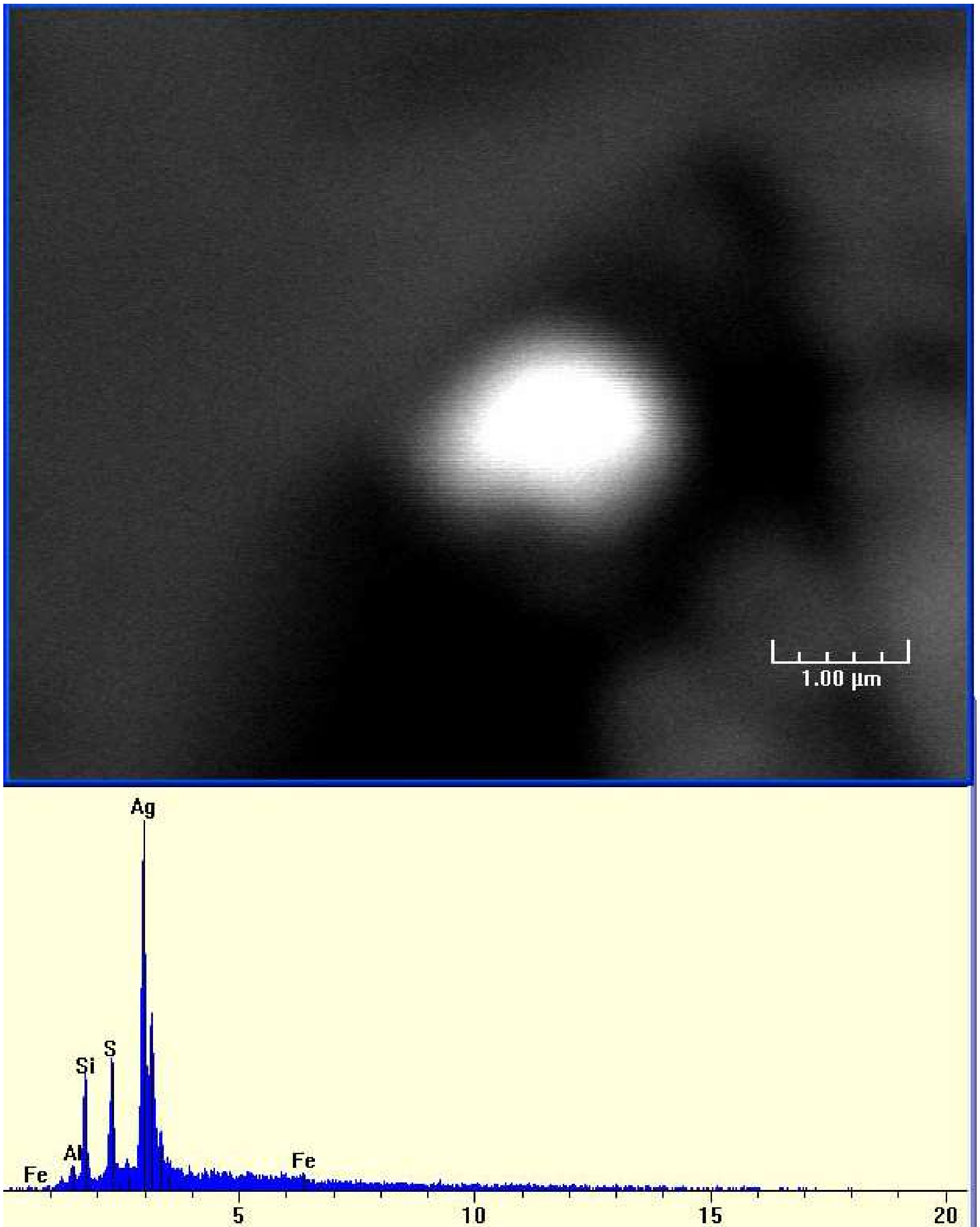
An extensive search using SEM/EDS indicates Ag phases are present in both samples, however, Au was not identified. Silver sulfide is the main Ag phase and occurs as irregularly shaped inclusions in quartz, pyrite and goethite pseudomorphs after pyrite. Cube-like grains are also seen in quartz and likely represent pseudomorphs of acanthite after argentite. Grain size of the Ag sulfide is very fine with measurements that range from 0.5 µm up to approximately 5 µm. Ag sulfide is also seen as thin rinds around pyrite and as small inclusions in jarosite. Much of the jarosite analyzed in these samples by EDS contains low but detectable Ag. The jarosite contained in the samples is potassium jarosite, however, vague bright areas in large masses are discernable using backscatter imaging. These areas are Ag rich and likely represent argentojarosite intimately mixed with the more abundant potassium variety. In sample **3829 CY-7** one small grain having a chemistry of Hg, Br, Cl and Ag was identified as an inclusion in quartz with a measurement just over 1 µm. This phase may represent capgaronnite or possibly iltisite. The primary reason for low Ag recovery in this material appears to be due to the very fine grained nature of the Ag sulfide, which should leach easily if liberated or exposed. In contrast, Ag bearing jarosites tend to be refractory and are usually unaffected by leaching.

The following table outlines individual phases based on XRD, petrography and SEM/EDS.

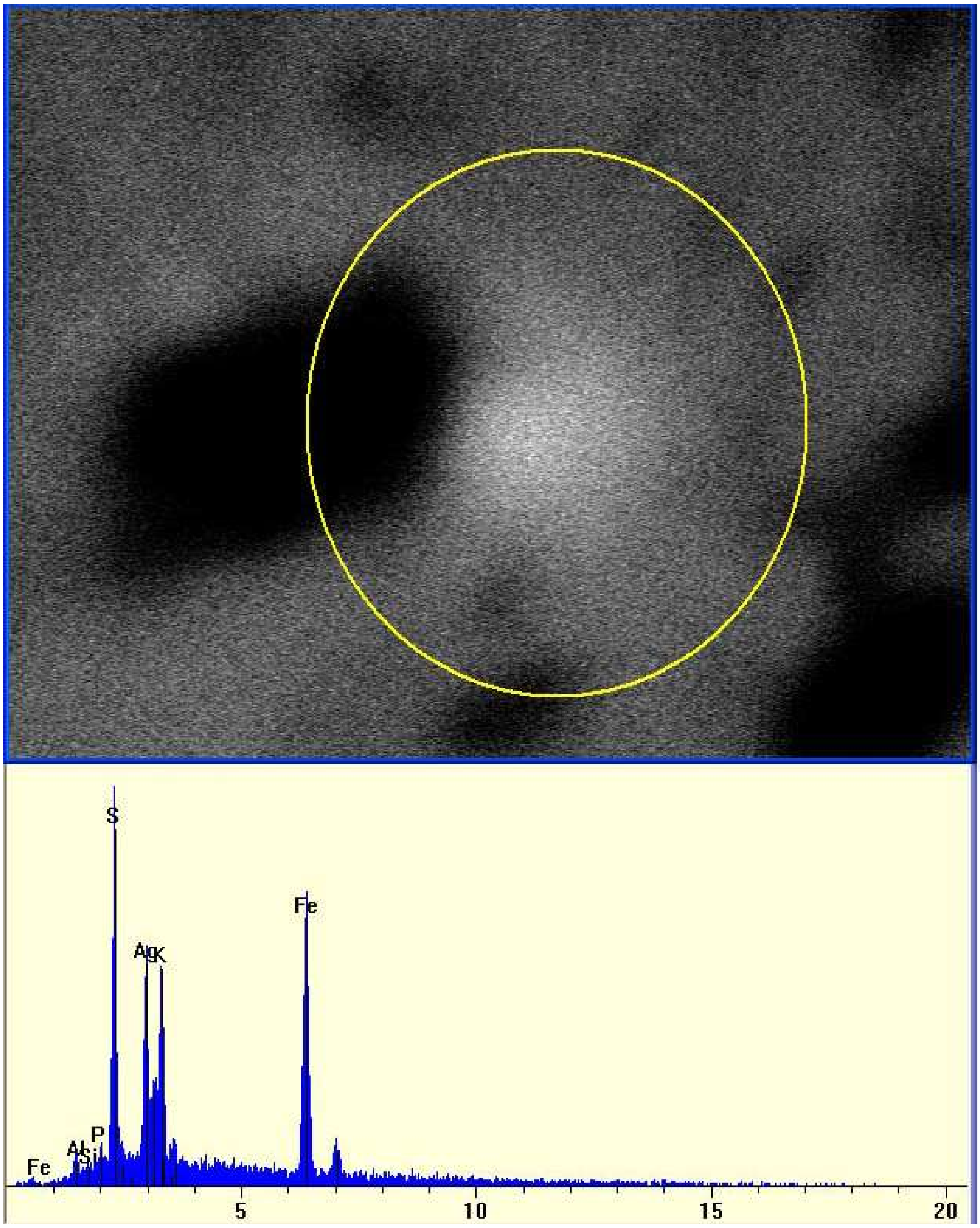
Client sample No.:	**3829 BMC Mineralogy**	**3829 CY-7**
Quartz	60	59
K-Feldspar	27	26
Jarosite	7	9
Iron Oxide	3	3
Pyrite	TR	TR
Chalcopyrite	TR	TR
Barite	TR	TR
Apatite	TR	TR
Zircon	TR	TR
Rutile	TR	TR
Ag Sulfide	TR	TR
Sericite	TR	TR
Capgaronnite (?)	TR	TR



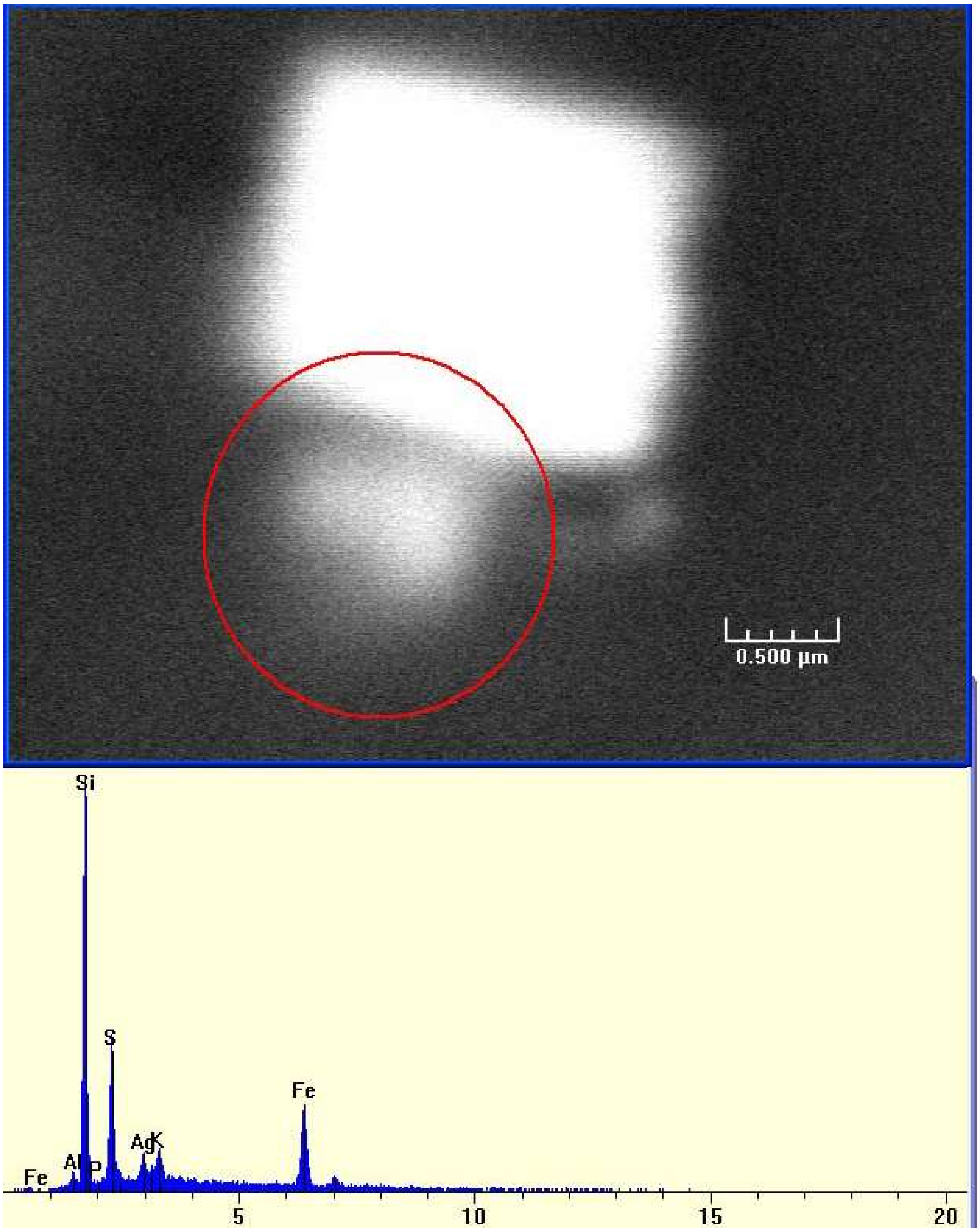
Client sample no. **3829 BMC Mineralogy**
Backscatter image of Ag sulfide surrounded by jarosite – 16,000X.



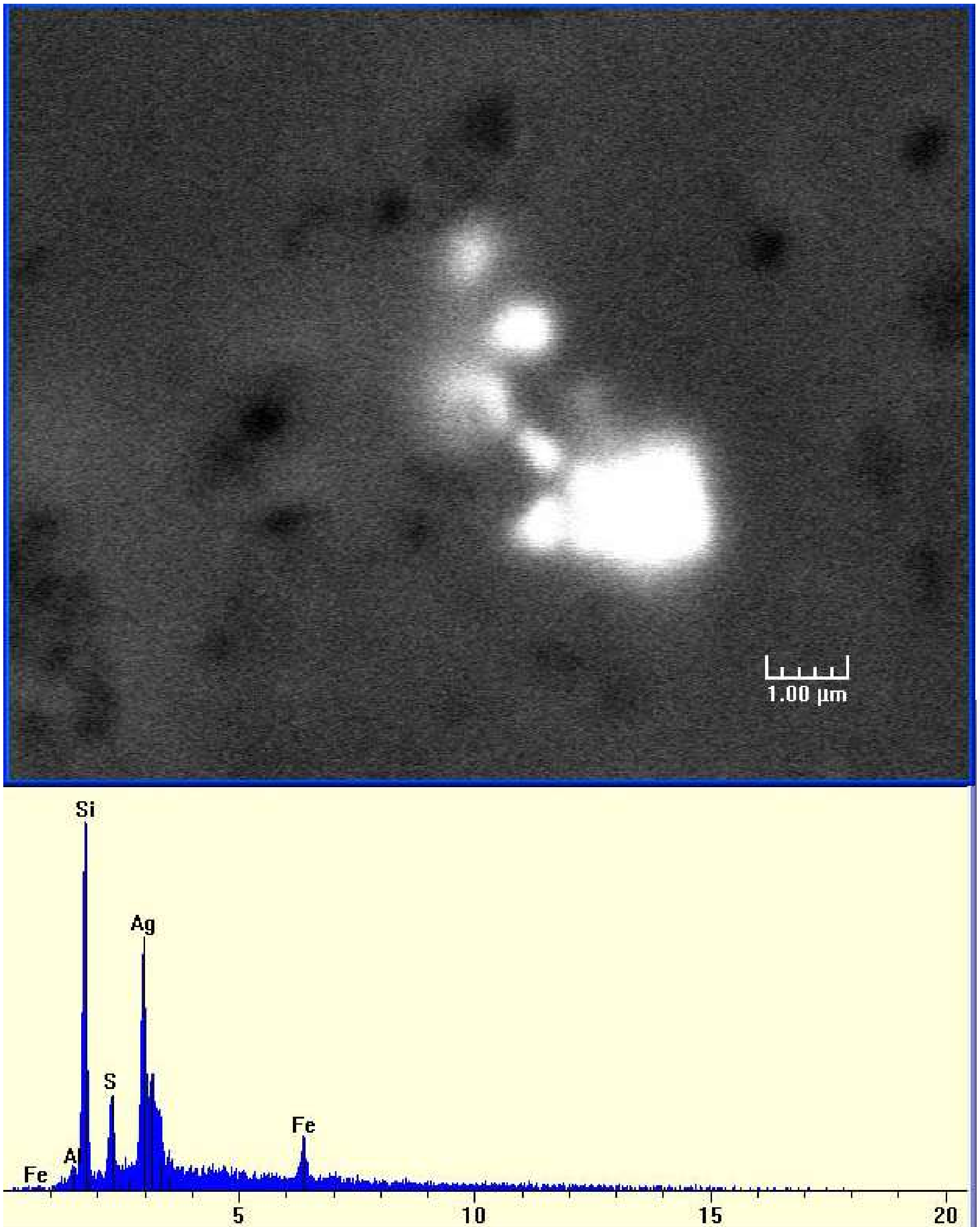
Client sample no. **3829 BMC Mineralogy**
Backscatter image of Ag sulfide in quartz – 16,000X.



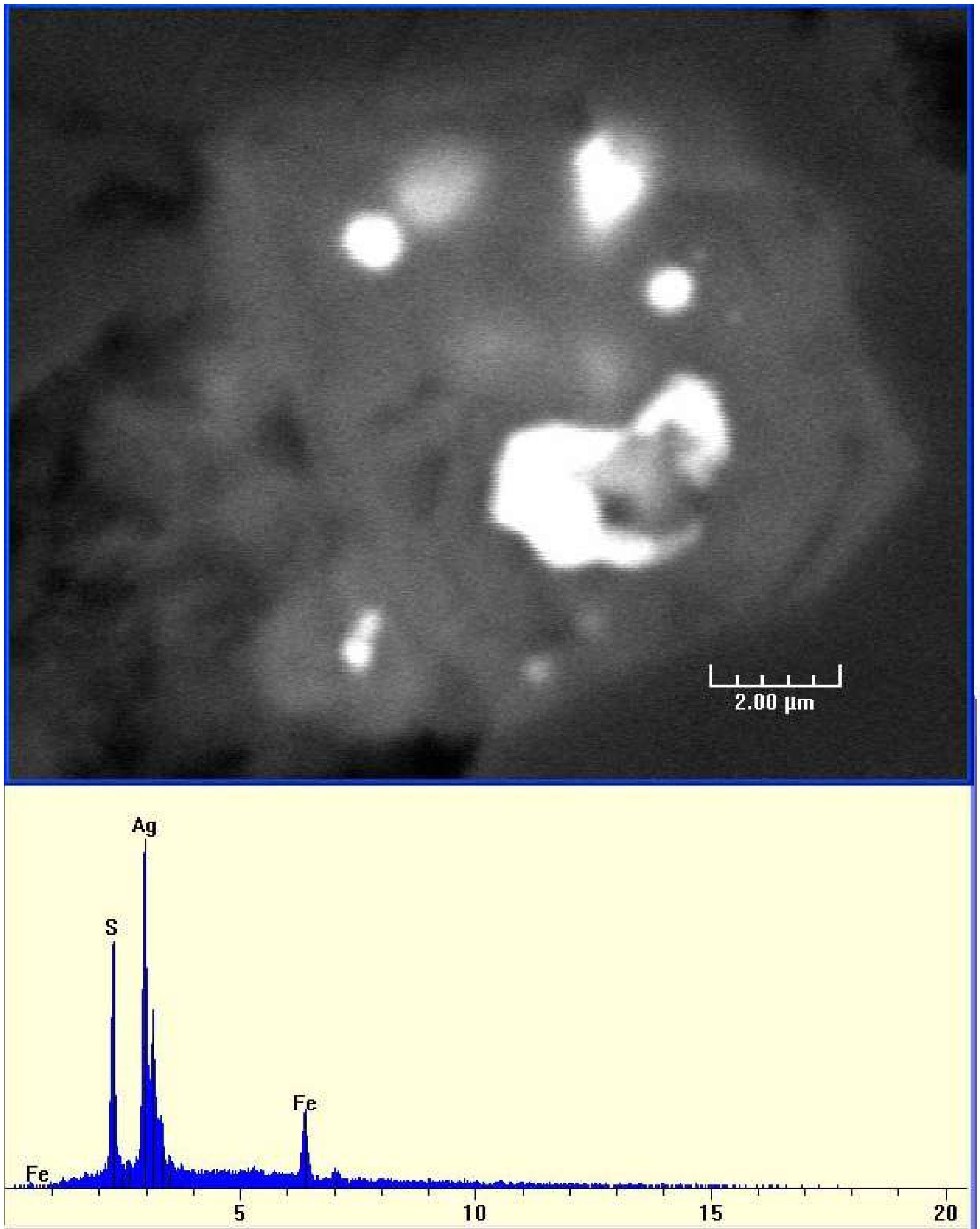
Client sample no. **3829 BMC Mineralogy**
Backscatter image of a bright Ag rich area in jarosite – 23,000X.



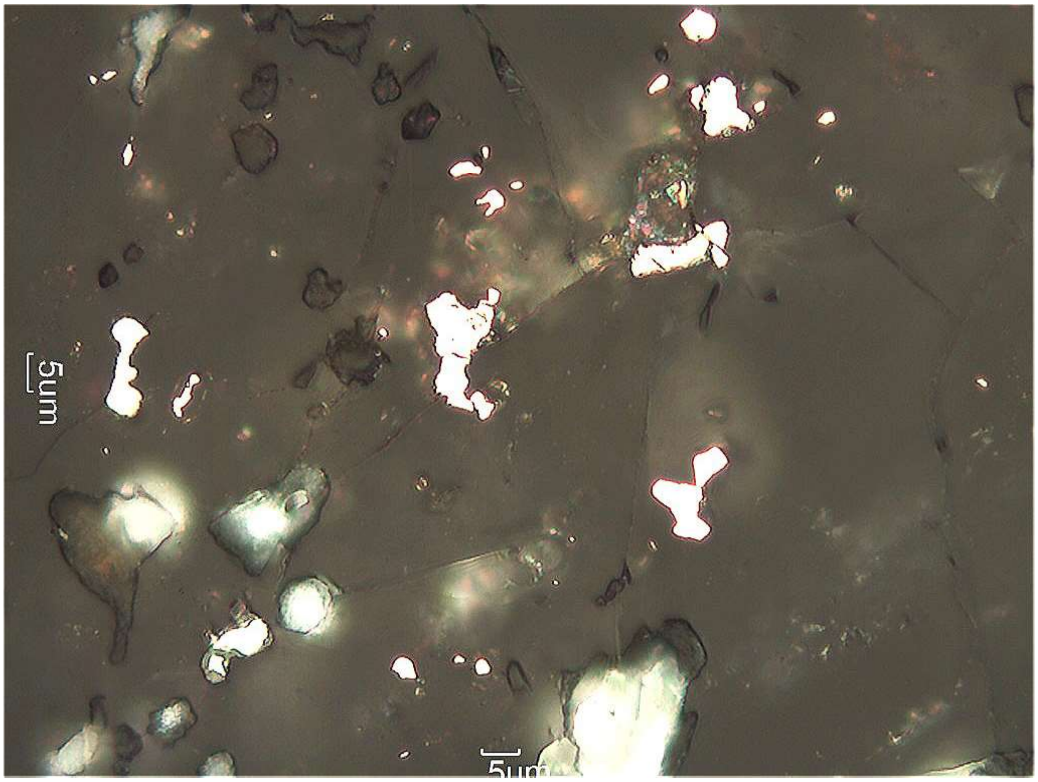
Client sample no. **3829 BMC Mineralogy**
Backscatter image of a pyrite cube attached to Ag bearing jarosite – 27,000X.



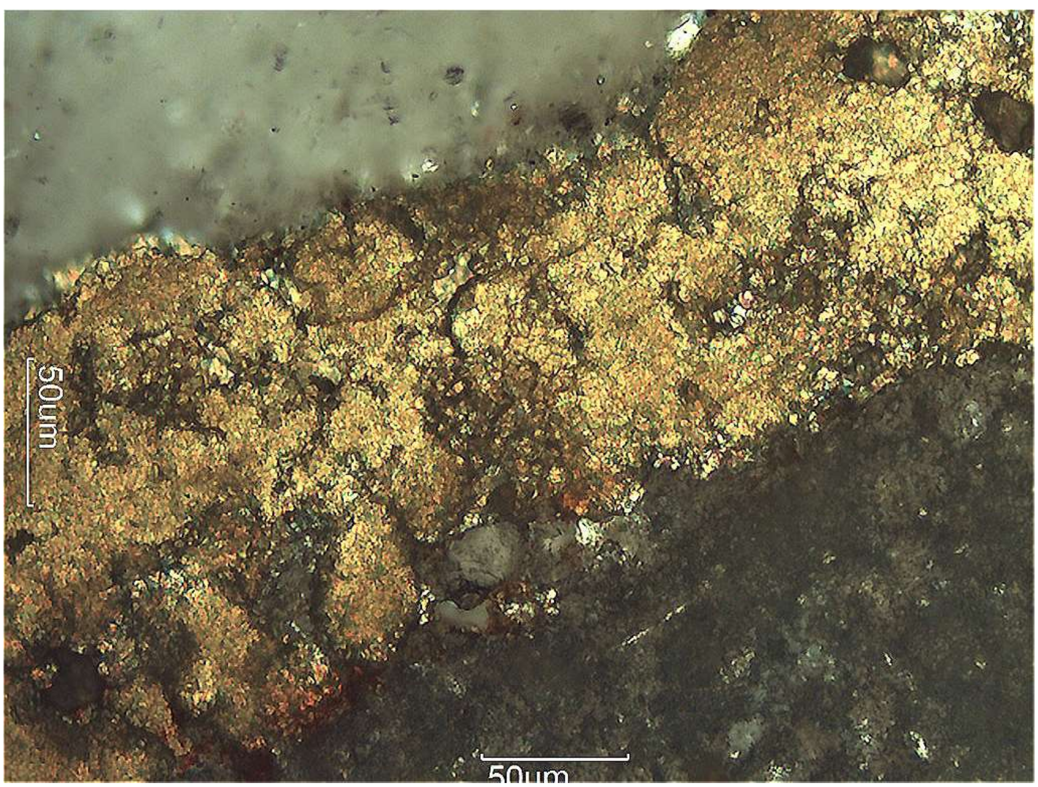
Client sample no. **3829 BMC Mineralogy**
Backscatter image of Ag sulfide grains mixed with iron oxide in quartz – 9,500X.



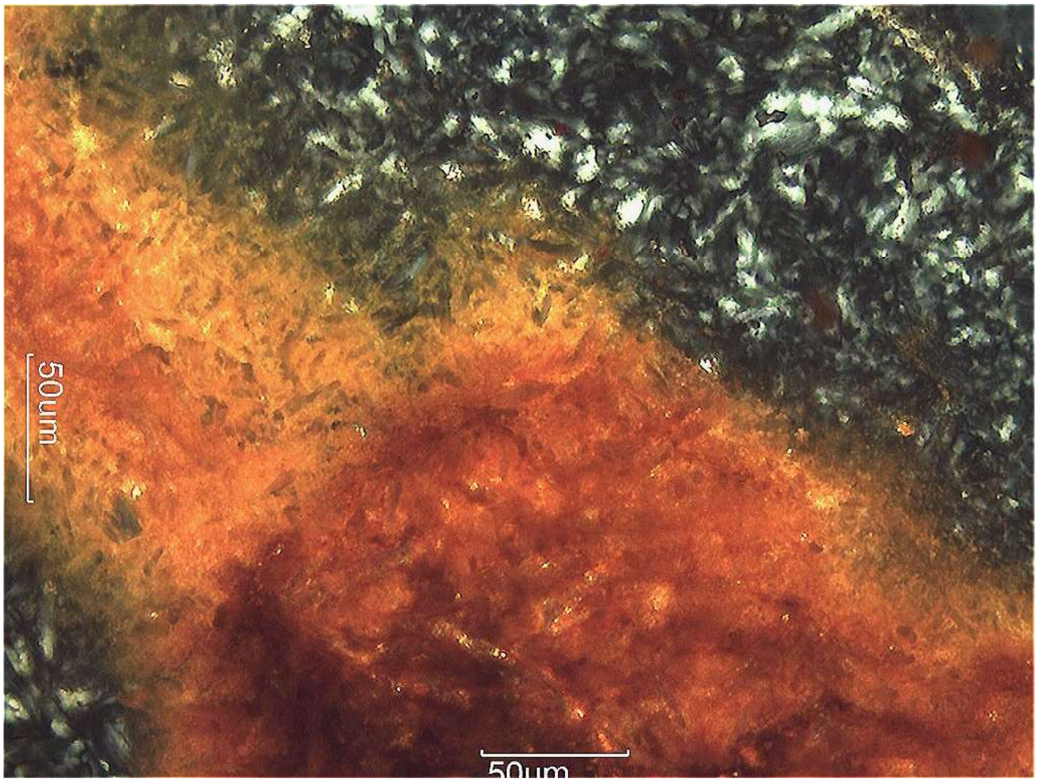
Client sample no. **3829 BMC Mineralogy**
Backscatter image of several Ag sulfide grains in a goethite pseudomorph after pyrite – 7,500X.



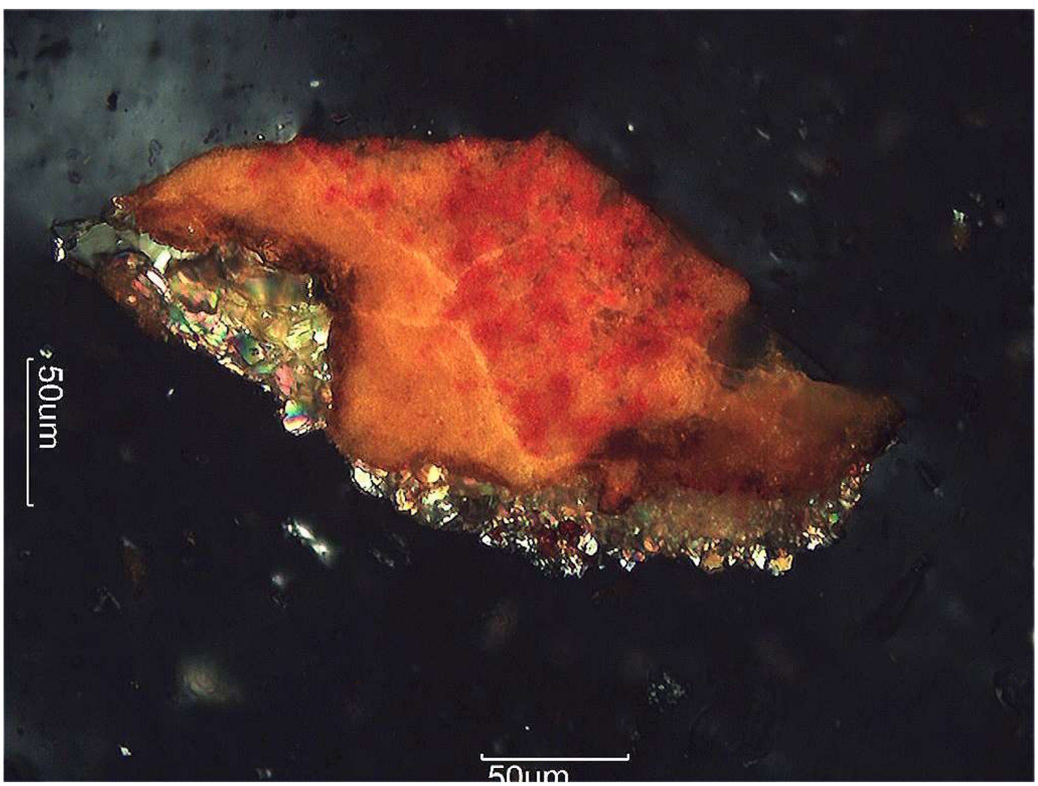
Client sample no. **3829 BMC Mineralogy**
Photo 1 – Numerous grains of pyrite in quartz. Reflected light – 500X.



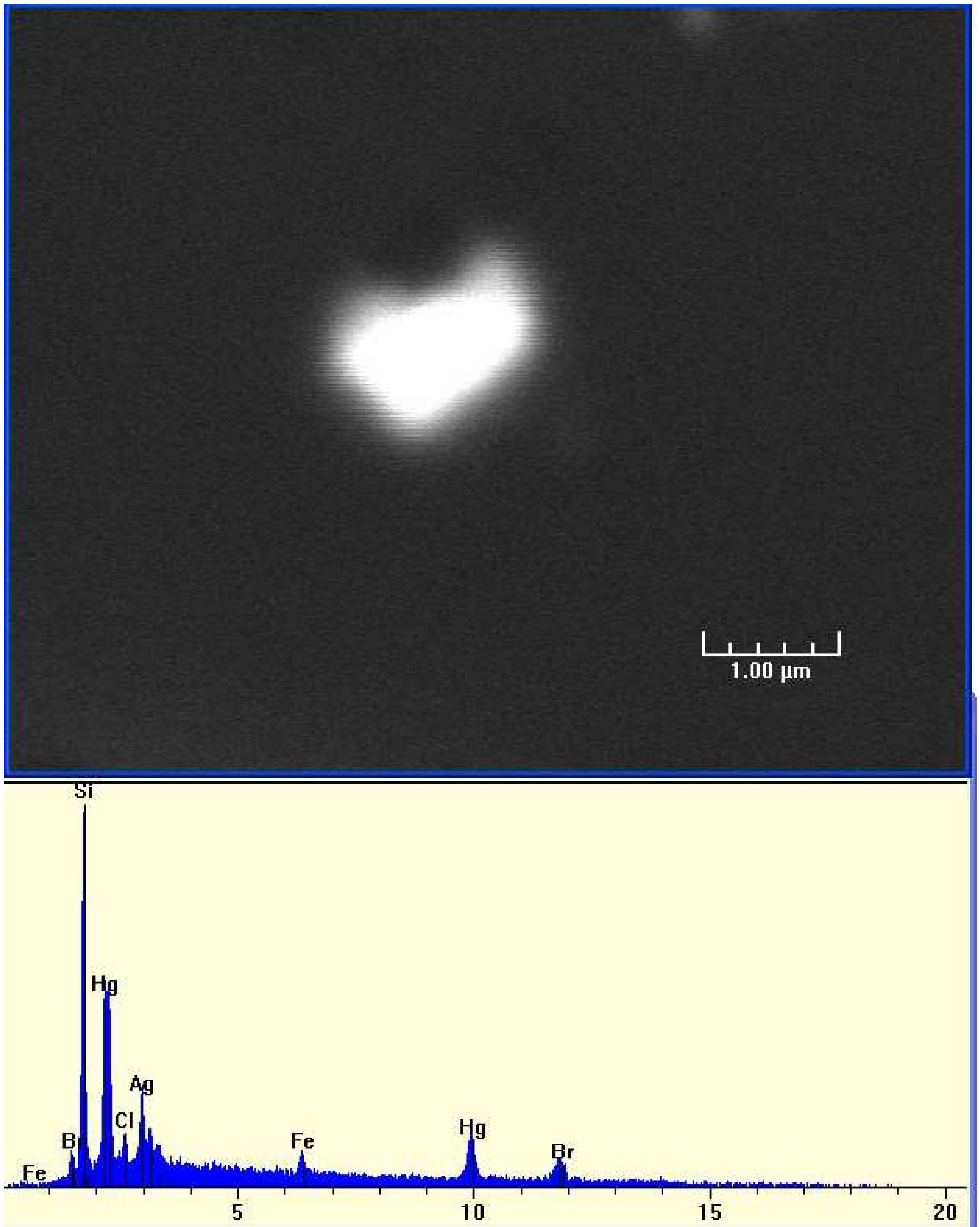
Client sample no. **3829 BMC Mineralogy**
Photo 2 – Large mass of granular jarosite. Polarized light – 200X.



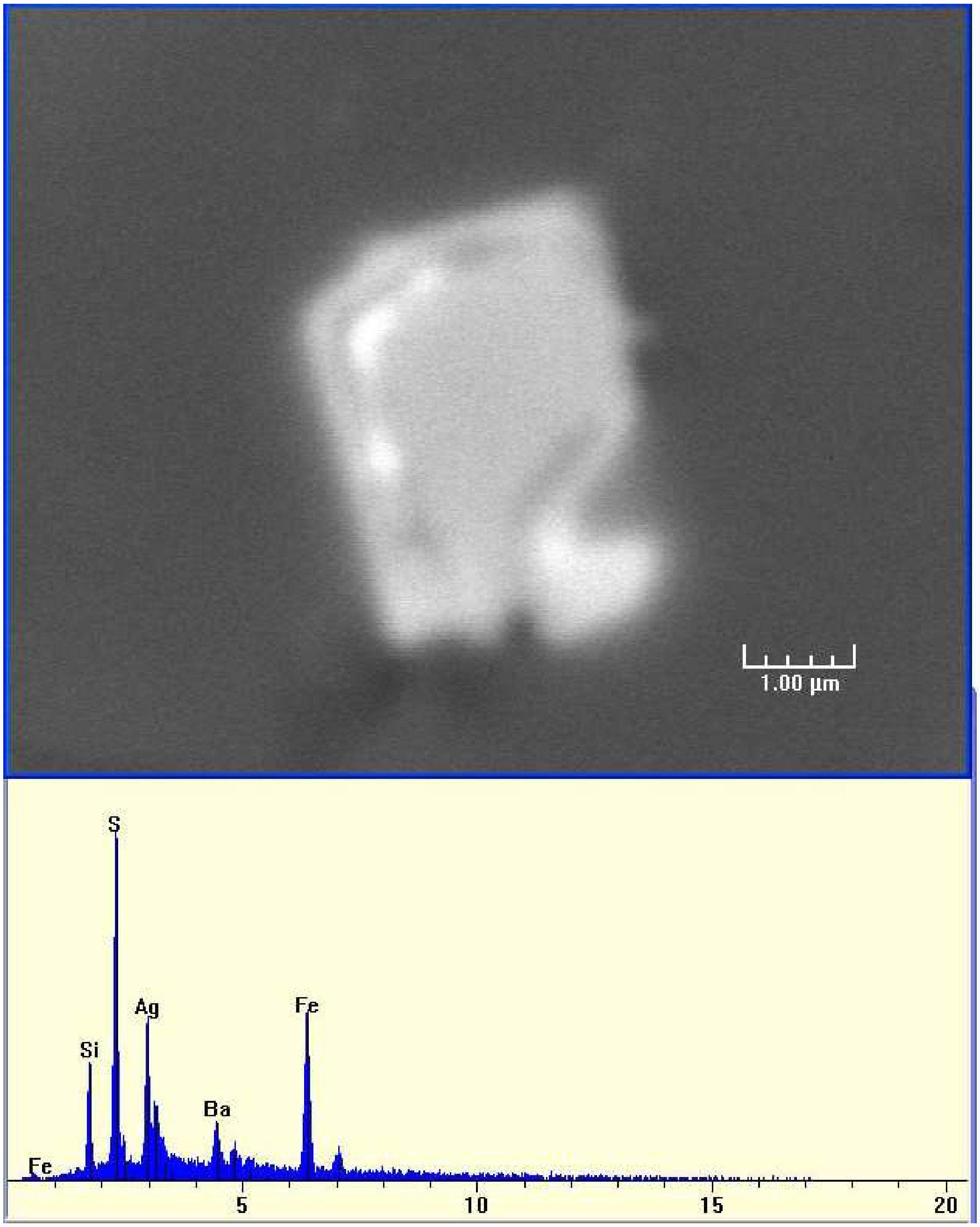
Client sample no. **3829 BMC Mineralogy**
Photo 3 – Iron oxide mixed with fine grained kaolinite. Polarized light – 200X.



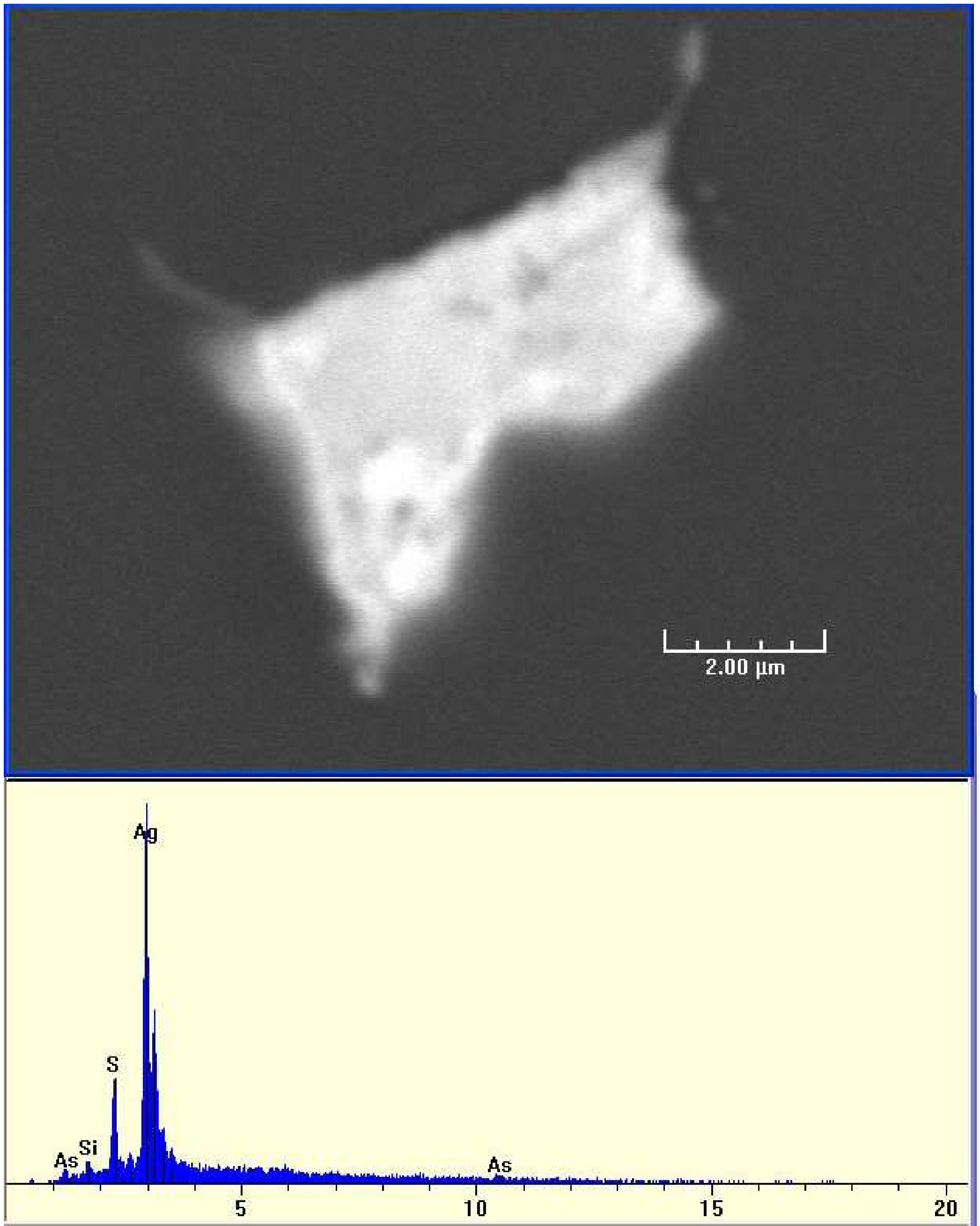
Client sample no. **3829 BMC Mineralogy**
Photo 4 – Iron oxide rimmed by colorful jarosite. Reflected light – 200X. Crossed Nichols



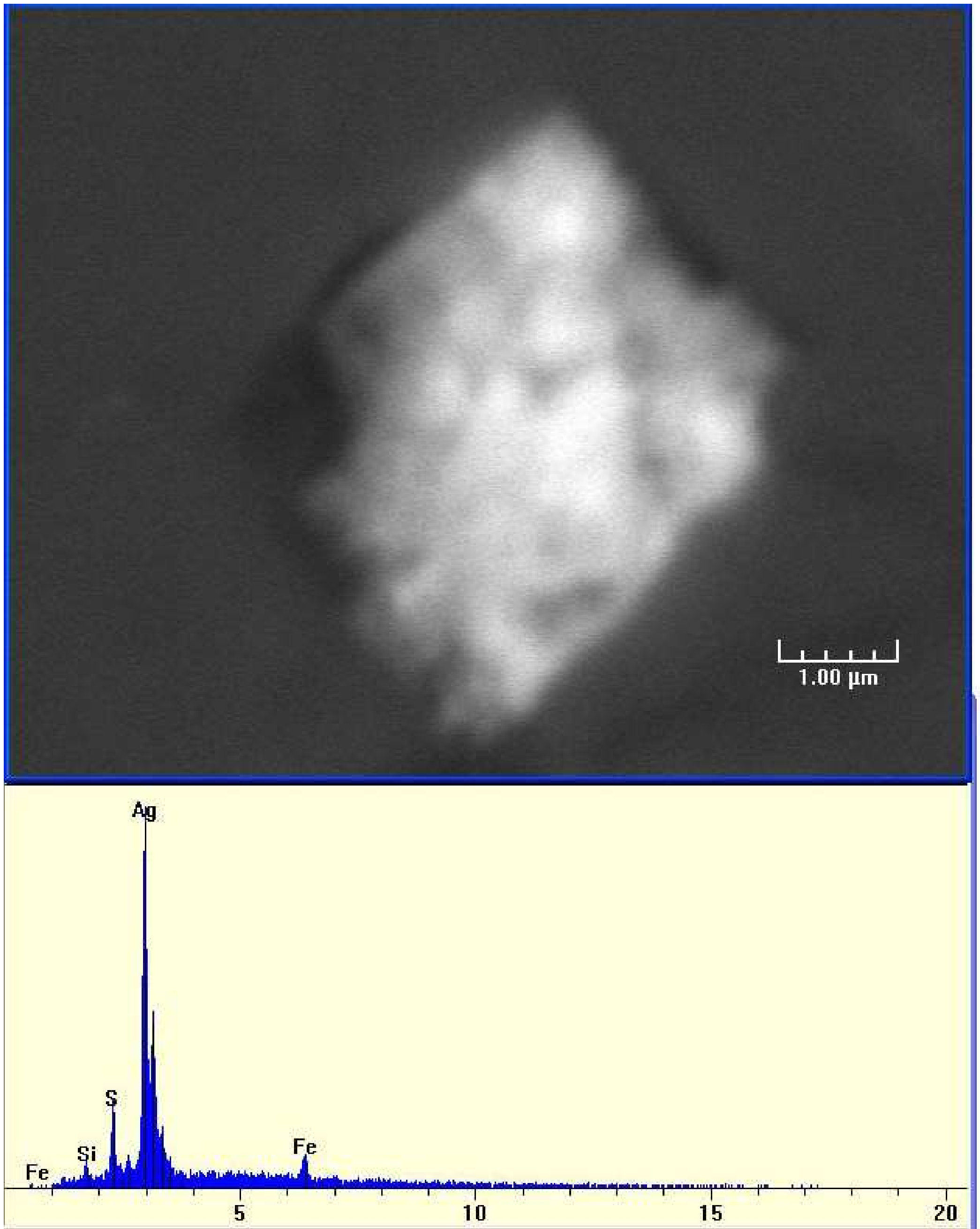
Client sample no. **3829 CY-7**
Backscatter image of capgaronnite (?) inclusion in quartz – 16,000X.



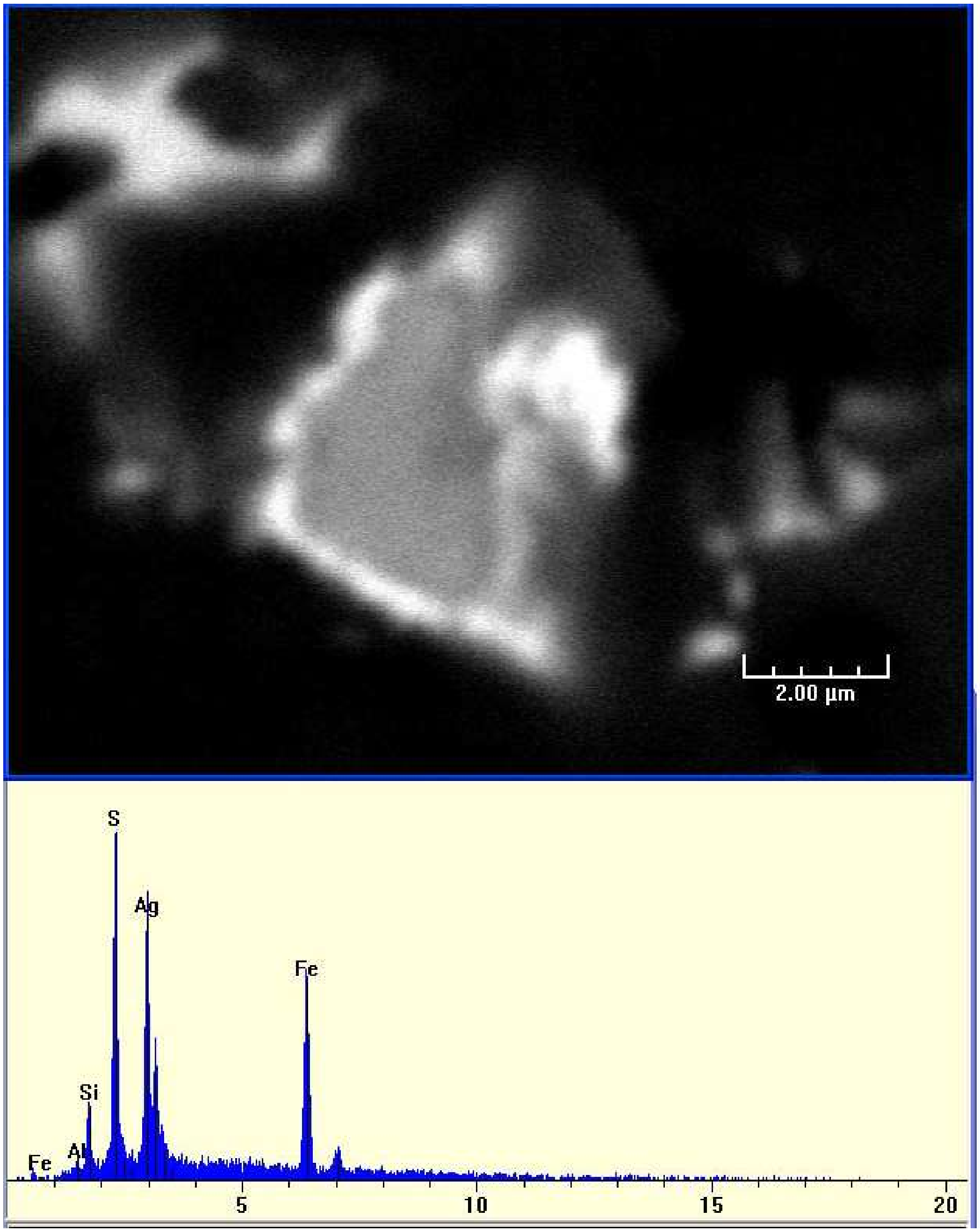
Client sample no. **3829 CY-7**
Backscatter image of pyrite rimmed with barite followed by bright Ag sulfide – 13,000X.



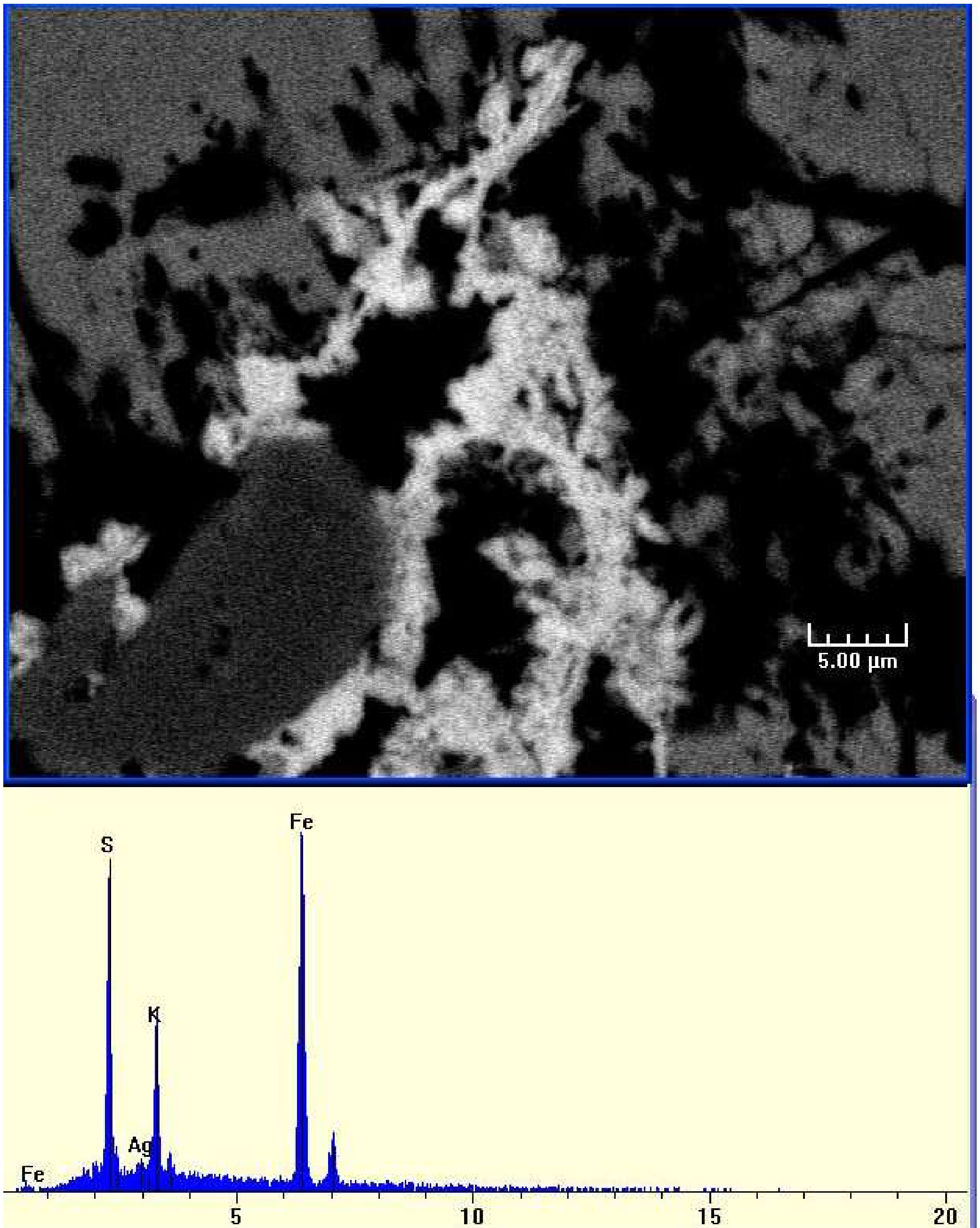
Client sample no. **3829 CY-7**
Backscatter image of Ag sulfide in quartz – 9,500X.



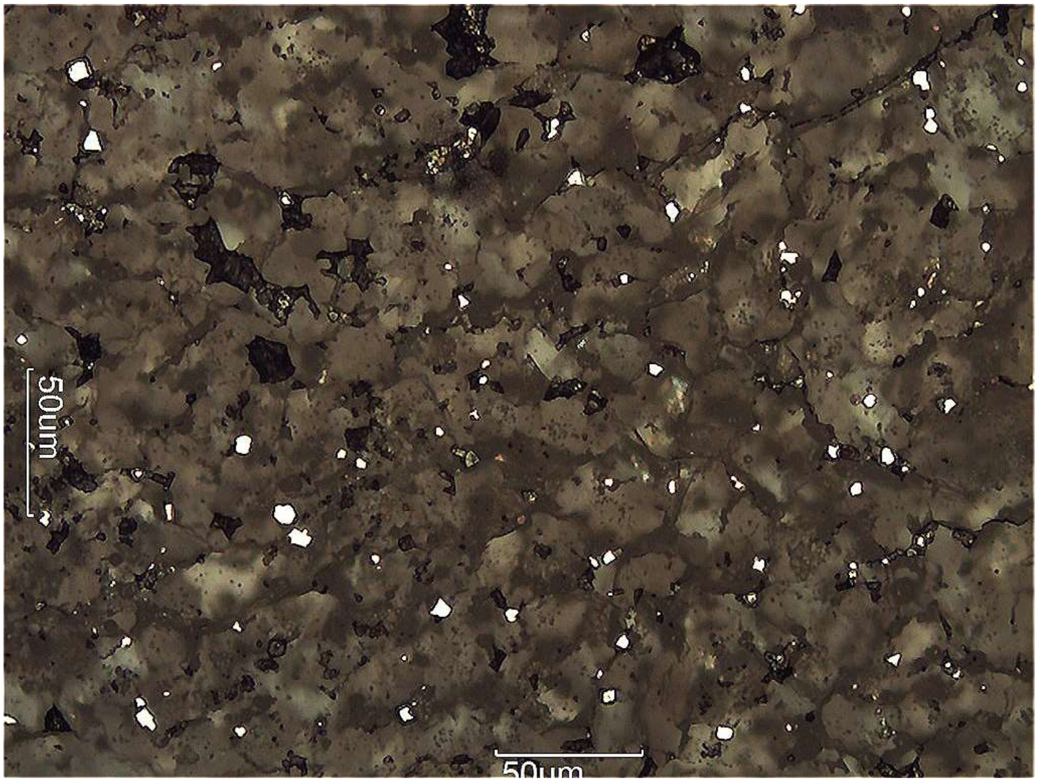
Client sample no. **3829 CY-7**
Backscatter image of cube like grain of Ag sulfide in quartz – 14,000X.



Client sample no. **3829 CY-7**
Backscatter image of pyrite rimmed with Ag sulfide – 8,500X.

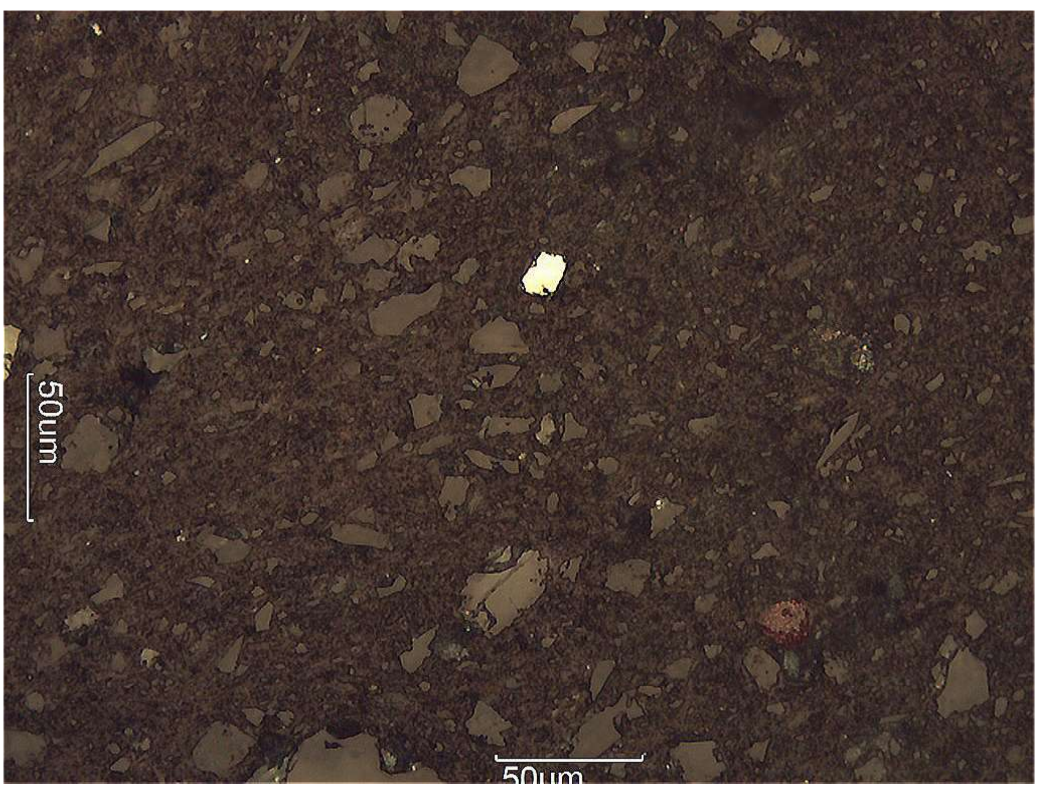


Client sample no. **3829 CY-7**
Backscatter image of bright jarosite with detectable Ag content – 2,300X.



Client sample no. **3829 CY-7**
Photo 1 – Numerous small grains of pyrite with granular quartz. Reflected light – 200X.

Client sample no. **3829 CY-7**
Photo 2 – Jarosite pseudomorph after pyrite. Reflected light – 500X. Crossed Nichols



Client sample no. **3829 CY-7**
Photo 3 – Small grain of chalcopyrite with granular quartz. Reflected light – 200X.

APPENDIX

Section 5 - Detailed Bottle Roll Test Results

Bottle Roll Test

Project No.	**3829**
Test No.	**CY-1**
Composite	**Underground Composite**
Feed Size	**80%-1.7mm**

Head Assay	g Au/mt	g Ag/mt
Predicted		
Initial	0.70	67
Duplicate	0.82	63
Triplicate	1.09	53
Average	0.87	61

Ore Charge 981.6 g

Solution Vol. 1.4724 L

Final Residue Wt 984.2 g

Natural pH 5.5

Tail Assay	g Au/mt	g Ag/mt
Initial	0.18	41
Duplicate	0.14	46
Triplicate	0.14	43
Average	0.15	43

Solid Density Wt. % 40.0

Cyanide Conc. Maintained at: 1.0 g/L

Raw Data

Leach Time	Solution Withdrawn			Reagents Applied		Sol. Analysis		Removed from pulp		
Hours	mL	NaCN (gpL)	pH	NaCN (g)	Lime (g)	Au (mg/L)	Ag (mg/L)	Au (mg)	Ag (mg)	NaCN (g)
0	-----	1.00	-----	1.47	1.30	-----	-----	-----	-----	-----
2	116	1.00	10.4	0.11	0.00	0.31	4.04	0.03596	0.46864	0.116
6	104	0.95	10.2	0.17	0.60	0.35	4.82	0.0364	0.50128	0.0988
24	102	1.00	10.5	0.10	1.00	0.37	5.57	0.03774	0.56814	0.102
48	112	1.00	11.3	0.11	0.30	0.36	5.37	0.04032	0.60144	0.112
72	138	0.95	11.3	0.20	0.10	0.34	5.34	0.04692	0.73692	0.1311
96	-----	1.00	11.3	-----	-----	0.32	5.03	-----	-----	-----

Metallurgical Results

Leach Time	Cumulative Au Extraction			Cumulative Ag Extraction			Reagent Requirements Cumulative kg/mt ore	
Hours	mg	g/mt ore	% of total	mg	g/mt ore	% of total	Cyanide Consumed	Lime Added
0		0.000	0.0		0.000	0.0		1.3
2	0.456	0.465	56.0	5.948	6.060	11.4	0.00	1.3
6	0.551	0.562	67.7	7.566	7.707	14.5	0.07	1.9
24	0.617	0.629	75.7	9.171	9.343	17.6	0.06	3.0
48	0.640	0.652	78.6	9.445	9.622	18.2	0.06	3.3
72	0.651	0.663	79.9	10.002	10	18.9	0.13	3.4
96	0.669	0.68	81.9	10.283	10	18.9	0.13	3.4

	Au	**% of Total**	**Ag**	**% of Total**
Extracted g/mt ore	**0.68**	**81.9**	**10**	**18.9**
Tail assay, g/mt	**0.15**		**43**	
Calculated Head g/mt ore	**0.83**		**53**	
NaCN Consumed, kg/mt ore	**0.13**			
Lime Added, kg/mt ore	**3.4**			

Bottle Roll Test

Head Assay	g Au/mt	g Ag/mt
Predicted		
Initial	0.21	17
Duplicate	0.67	34
Triplicate	0.37	21
Average	0.42	24

Project No. **3829**
Test No. **CY-2**
Composite **Surface Composite**
Feed Size **80%-1.7mm**

Ore Charge 992.7 g

Solution Vol. 1.4891 L

Final Residue Wt 982.2 g

Tail Assay	g Au/mt	g Ag/mt
Initial	0.05	19
Duplicate	0.07	19
Triplicate	0.05	21
Average	0.06	20

Natural pH 7.5

Solid Density Wt. % 40.0

Cyanide Conc. Maintained at: g/L 1.0

Raw Data

Leach Time	Solution Withdrawn			Reagents Applied		Sol. Analysis		Removed from pulp		
Hours	mL	NaCN (gpL)	pH	NaCN (g)	Lime (g)	Au (mg/L)	Ag (mg/L)	Au (mg)	Ag (mg)	NaCN (g)
0	-----	1.00	-----	1.49	1.00	-----	-----	-----	-----	-----
2	117	1.00	10.9	0.12	0.40	0.09	1.72	0.01053	0.20124	0.117
6	106	1.00	11.2	0.11	0.00	0.11	2.02	0.01166	0.21412	0.106
24	106	1.00	10.7	0.11	0.30	0.14	2.48	0.01484	0.26288	0.106
48	112	1.00	11.0	0.11	0.10	0.13	2.60	0.01456	0.2912	0.112
72	103	0.95	10.8	0.17	0.30	0.13	2.61	0.01339	0.26883	0.09785
96	-----	1.00	11.1	-----	-----	0.12	2.57	-----	-----	-----

Metallurgical Results

Leach Time	Cumulative Au Extraction			Cumulative Ag Extraction			Reagent Requirements Cumulative kg/mt ore	
Hours	mg	g/mt ore	% of total	mg	g/mt ore	% of total	Cyanide Consumed	Lime Added
0		0.000	0.0		0.000	0.0		1.0
2	0.134	0.135	43.5	2.561	2.580	10.3	0.00	1.4
6	0.174	0.176	56.6	3.209	3.233	12.9	0.00	1.4
24	0.231	0.232	75.0	4.108	4.139	16.6	0.01	1.7
48	0.231	0.232	74.9	4.550	4.583	18.3	0.01	1.8
72	0.245	0.247	79.7	4.856	4.892	19.6	0.08	2.1
96	0.244	0.25	80.6	5.065	5	20.0	0.08	2.1

	Au	% of Total	Ag	% of Total
Extracted g/mt ore	**0.25**	**80.6**	**5**	**20.0**
Tail assay, g/mt	**0.06**		**20**	
Calculated Head g/mt ore	**0.31**		**25**	
NaCN Consumed, kg/mt ore	**0.08**			
Lime Added, kg/mt ore	**2.1**			

Bottle Roll Test

Project No.	**3829**
Test No.	**CY-3**
Composite	**Master Composite**
Feed Size	**80%-1.7mm**

Head Assay	g Au/mt	g Ag/mt
Predicted		
Initial	0.57	40
Duplicate	0.66	41
Triplicate	0.77	50
Average	0.67	44

Ore Charge 1042.8 g

Solution Vol. 1.5642 L

Final Residue Wt 1036.5 g

Natural pH 6.3

Tail Assay	g Au/mt	g Ag/mt
Initial	0.13	33
Duplicate	0.12	33
Triplicate	0.12	34
Average	0.12	33

Solid Density Wt. % 40.0

Cyanide Conc. Maintained at: 1.0 g/L

Raw Data

Leach Time	Solution Withdrawn			Reagents Applied		Sol. Analysis		Removed from pulp		
Hours	mL	NaCN (gpL)	pH	NaCN (g)	Lime (g)	Au (mg/L)	Ag (mg/L)	Au (mg)	Ag (mg)	NaCN (g)
0	-----	1.00	-----	1.56	1.00	-----	-----	-----	-----	-----
2	107	0.95	10.2	0.18	1.00	0.23	2.77	0.02461	0.29639	0.10165
6	107	1.00	11.3	0.10	0.00	0.27	3.11	0.02889	0.33277	0.107
24	103	1.00	10.7	0.10	0.30	0.29	3.57	0.02987	0.36771	0.103
48	153	1.00	10.9	0.15	0.10	0.29	3.79	0.04437	0.57987	0.153
72	153	1.00	10.8	0.15	0.20	0.26	3.65	0.03978	0.55845	0.153
96	-----	0.95	10.9	-----	-----	0.24	3.52	-----	-----	-----

Metallurgical Results

Leach Time	Cumulative Au Extraction			Cumulative Ag Extraction			Reagent Requirements Cumulative kg/mt ore	
Hours	mg	g/mt ore	% of total	mg	g/mt ore	% of total	Cyanide Consumed	Lime Added
0		0.000	0.0		0.000	0.0		1.0
2	0.360	0.345	53.9	4.333	4.155	10.4	0.07	1.9
6	0.447	0.429	67.0	5.161	4.949	12.4	0.07	1.9
24	0.507	0.486	76.0	6.213	5.958	14.9	0.06	2.2
48	0.537	0.515	80.5	6.925	6.641	16.6	0.06	2.3
72	0.534	0.512	80.1	7.286	6.987	17.5	0.06	2.5
96	0.543	0.52	81.3	7.641	7	17.5	0.13	2.5

	Au	**% of Total**	**Ag**	**% of Total**
Extracted g/mt ore	**0.52**	**81.3**	**7**	**17.5**
Tail assay, g/mt	**0.12**		**33**	
Calculated Head g/mt ore	**0.64**		**40**	
NaCN Consumed, kg/mt ore	**0.13**			
Lime Added, kg/mt ore	**2.5**			

Bottle Roll Test

Project No. **3829**
Test No. **CY-4**
Composite **Master Composite**
Feed Size **100%-50mm**

Head Assay	g Au/mt	g Ag/mt
Predicted		
Initial	0.57	40
Duplicate	0.66	41
Triplicate	0.77	50
Average	0.67	44

Ore Charge 4999.5 g

Solution Vol. 7.4993 L

Final Residue Wt 5017.1 g

Natural pH 6.6

Tail Assay	g Au/mt	g Ag/mt
Initial	0.23	52
Duplicate	0.28	59
Triplicate	0.26	52
Average	0.26	54

Solid Density Wt. % 40.0

Cyanide Conc. Maintained at: g/L 1.0

Raw Data

Leach Time	Solution Withdrawn			Reagents Applied		Sol. Analysis		Removed from pulp		
Hours	mL	NaCN (gpL)	pH	NaCN (g)	Lime (g)	Au (mg/L)	Ag (mg/L)	Au (mg)	Ag (mg)	NaCN (g)
0	-----	1.00	-----	7.50	3.00	-----	-----	-----	-----	-----
2	109	1.00	10.8	0.11	0.40	0.11	0.53	0.01199	0.05777	0.109
6	109	1.00	10.7	0.11	0.60	0.15	0.74	0.01635	0.08066	0.109
24	104	1.00	10.5	0.10	1.00	0.23	1.00	0.02392	0.104	0.104
48	109	1.00	10.7	0.11	1.00	0.25	1.19	0.02725	0.12971	0.109
72	104	0.95	10.9	0.47	0.70	0.27	1.31	0.02808	0.13624	0.0988
96	-----	1.00	11.1	-----	-----	0.28	1.40	-----	-----	-----

Metallurgical Results

Leach Time Hours	Cumulative Au Extraction mg	Cumulative Au Extraction g/mt ore	Cumulative Au Extraction % of total	Cumulative Ag Extraction mg	Cumulative Ag Extraction g/mt ore	Cumulative Ag Extraction % of total	Reagent Requirements Cumulative kg/mt ore Cyanide Consumed	Reagent Requirements Cumulative kg/mt ore Lime Added
0		0.000	0.0		0.000	0.0		0.6
2	0.825	0.165	23.6	3.975	0.795	1.4	0.00	0.7
6	1.137	0.227	32.5	5.607	1.122	2.0	0.00	0.8
24	1.753	0.351	50.1	7.638	1.528	2.7	0.00	1.0
48	1.927	0.385	55.1	9.167	1.834	3.3	0.00	1.2
72	2.104	0.421	60.1	10.196	2	3.6	0.07	1.3
96	2.207	0.44	62.9	11.007	2	3.6	0.07	1.3

	Au	**% of Total**	**Ag**	**% of Total**
Extracted g/mt ore	**0.44**	**62.9**	**2**	**3.6**
Tail assay, g/mt	**0.26**		**54**	
Calculated Head g/mt ore	**0.70**		**56**	
NaCN Consumed, kg/mt ore	**0.07**			
Lime Added, kg/mt ore	**1.3**			

Bottle Roll Test

Project No.	**3829**
Test No.	**CY-5**
Composite	**Master Composite**
Feed Size	**80%-19mm**

Head Assay	g Au/mt	g Ag/mt
Predicted		
Initial	0.57	40
Duplicate	0.66	41
Triplicate	0.77	50
Average	0.67	44

Ore Charge 2040.8 g

Solution Vol. 3.0612 L

Final Residue Wt 2014.2 g

Natural pH 6.5

Tail Assay	g Au/mt	g Ag/mt
Initial	0.19	31
Duplicate	0.33	38
Triplicate	0.24	34
Average	0.25	34

Solid Density Wt. % 40.0

Cyanide Conc. Maintained at: 1.0 g/L

Raw Data

Leach Time	Solution Withdrawn			Reagents Applied		Sol. Analysis		Removed from pulp		
Hours	mL	NaCN (gpL)	pH	NaCN (g)	Lime (g)	Au (mg/L)	Ag (mg/L)	Au (mg)	Ag (mg)	NaCN (g)
0	-----	1.00	-----	3.06	2.00	-----	-----	-----	-----	-----
2	109	1.00	11.2	0.11	0.00	0.13	1.09	0.01417	0.11881	0.109
6	102	1.00	10.8	0.10	0.30	0.19	1.51	0.01938	0.15402	0.102
24	100	0.95	10.5	0.24	0.70	0.25	2.12	0.025	0.212	0.095
48	105	1.00	10.7	0.10	0.70	0.28	2.47	0.0294	0.25935	0.105
72	108	1.00	10.9	0.11	0.50	0.30	2.64	0.0324	0.28512	0.108
96	-----	1.00	11.2	-----	-----	0.30	2.79	-----	-----	-----

Metallurgical Results

Leach Time	Cumulative Au Extraction			Cumulative Ag Extraction			Reagent Requirements Cumulative kg/mt ore	
Hours	mg	g/mt ore	% of total	mg	g/mt ore	% of total	Cyanide Consumed	Lime Added
0		0.000	0.0		0.000	0.0		1.0
2	0.398	0.195	25.7	3.337	1.635	4.2	0.00	1.0
6	0.596	0.292	38.4	4.741	2.323	6.0	0.00	1.1
24	0.799	0.391	51.5	6.763	3.314	8.5	0.07	1.5
48	0.916	0.449	59.0	8.046	3.943	10.1	0.07	1.8
72	1.006	0.493	64.9	8.826	4.325	11.1	0.07	2.1
96	1.039	0.51	67.1	9.570	5	12.8	0.07	2.1

	Au	**% of Total**	**Ag**	**% of Total**
Extracted g/mt ore	**0.51**	**67.1**	**5**	**12.8**
Tail assay, g/mt	**0.25**		**34**	
Calculated Head g/mt ore	**0.76**		**39**	
NaCN Consumed, kg/mt ore	**0.07**			
Lime Added, kg/mt ore	**2.1**			

Bottle Roll Test

Head Assay	g Au/mt	g Ag/mt
Predicted		
Initial	0.57	40
Duplicate	0.66	41
Triplicate	0.77	50
Average	0.67	44

Project No. **3829**
Test No. **CY-6**
Composite **Master Composite**
Feed Size **80%-6.3mm**

Ore Charge 1001.6 g
Solution Vol. 1.5024 L
Natural pH 6.4

Final Residue Wt 993.0 g

Tail Assay	g Au/mt	g Ag/mt
Initial	0.15	38
Duplicate	0.12	42
Triplicate	0.18	35
Average	0.15	38

Solid Density Wt. % 40.0

Cyanide Conc. Maintained at: g/L 1.0

Raw Data

Leach Time	Solution Withdrawn			Reagents Applied		Sol. Analysis		Removed from pulp		
Hours	mL	NaCN (gpL)	pH	NaCN (g)	Lime (g)	Au (mg/L)	Ag (mg/L)	Au (mg)	Ag (mg)	NaCN (g)
0	-----	1.00	-----	1.50	1.00	-----	-----	-----	-----	-----
2	105	1.00	10.5	0.10	1.00	0.20	2.12	0.021	0.2226	0.105
6	104	1.00	11.5	0.10	0.00	0.24	2.43	0.02496	0.25272	0.104
24	105	1.00	11.0	0.10	0.00	0.29	3.08	0.03045	0.3234	0.105
48	122	0.95	10.7	0.12	0.20	0.29	3.29	0.03538	0.40138	0.1159
72	114	0.95	10.7	0.18	0.80	0.28	3.26	0.03192	0.37164	0.1083
96	-----	1.00	11.0	-----	-----	0.26	3.21	-----	-----	-----

Metallurgical Results

Leach Time	Cumulative Au Extraction			Cumulative Ag Extraction			Reagent Requirements Cumulative kg/mt ore	
Hours	mg	g/mt ore	% of total	mg	g/mt ore	% of total	Cyanide Consumed	Lime Added
0		0.000	0.0		0.000	0.0		1.0
2	0.300	0.300	44.1	3.185	3.180	7.2	0.00	2.0
6	0.382	0.381	56.0	3.873	3.867	8.8	-0.01	2.0
24	0.482	0.481	70.7	5.103	5.095	11.6	-0.01	2.0
48	0.512	0.511	75.2	5.742	5.732	13.0	0.06	2.2
72	0.532	0.53	77.9	6.098	6	13.6	0.06	3.0
96	0.534	0.53	77.9	6.394	6	13.6	0.06	3.0

	Au	**% of Total**	**Ag**	**% of Total**
Extracted g/mt ore	**0.53**	**77.9**	**6**	**13.6**
Tail assay, g/mt	**0.15**		**38**	
Calculated Head g/mt ore	**0.68**		**44**	

NaCN Consumed, kg/mt ore **<0.07**
Lime Added, kg/mt ore **3.0**

Bottle Roll Test

Project No. **3829**
Test No. **CY-7**
Composite **Master Composite**
Feed Size **80%-19mm**

Head Assay	g Au/mt	g Ag/mt
Predicted		
Initial	0.57	40
Duplicate	0.66	41
Triplicate	0.77	50
Average	0.67	44

Ore Charge 1997.5 g

Solution Vol. 2.9963 L

Final Residue Wt 1977.5 g

Natural pH 6.3

Tail Assay	g Au/mt	g Ag/mt
Initial	0.13	34
Duplicate	0.16	35
Triplicate	0.22	36
Average	0.17	35

Solid Density Wt. % 40.0

Cyanide Conc. Maintained at: g/L 5.0

Raw Data

Leach Time	Solution Withdrawn			Reagents Applied		Sol. Analysis		Removed from pulp		
Hours	mL	NaCN (gpL)	pH	NaCN (g)	Lime (g)	Au (mg/L)	Ag (mg/L)	Au (mg)	Ag (mg)	NaCN (g)
0	-----	5.01	-----	15.00	2.00	-----	-----	-----	-----	-----
2	104	5.05	11.7	0.39	0.00	0.19	1.74	0.01976	0.18096	0.5252
6	100	4.95	11.4	0.64	0.00	0.23	2.07	0.023	0.207	0.495
24	104	5.00	11.0	0.54	0.00	0.29	2.96	0.03016	0.30784	0.52
48	100	4.80	10.9	1.09	0.00	0.32	3.38	0.032	0.338	0.48
72	100	5.00	11.0	0.51	0.00	0.32	3.59	0.032	0.359	0.5
96	-----	4.90	11.0	-----	-----	0.32	3.64	-----	-----	-----

Metallurgical Results

Leach Time	Cumulative Au Extraction			Cumulative Ag Extraction			Reagent Requirements Cumulative kg/mt ore	
Hours	mg	g/mt ore	% of total	mg	g/mt ore	% of total	Cyanide Consumed	Lime Added
0		0.000	0.0		0.000	0.0		1.0
2	0.569	0.285	39.6	5.214	2.610	6.4	-0.07	1.0
6	0.709	0.355	49.3	6.383	3.196	7.8	0.02	1.0
24	0.912	0.456	63.4	9.257	4.634	11.3	0.01	1.0
48	1.032	0.517	71.7	10.823	5.418	13.2	0.32	1.0
72	1.064	0.533	74.0	11.791	5.903	14.4	0.33	1.0
96	1.096	0.55	76.4	12.299	6	14.6	0.48	1.0

	Au	**% of Total**	**Ag**	**% of Total**
Extracted g/mt ore	**0.55**	**76.4**	**6**	**14.6**
Tail assay, g/mt	**0.17**		**35**	
Calculated Head g/mt ore	**0.72**		**41**	
NaCN Consumed, kg/mt ore	**0.48**			
Lime Added, kg/mt ore	**1.0**			

Bottle Roll Test

Project No. **3829**
Test No. **CY-8**
Composite **Master Composite**
Feed Size **80%-6.3mm**

Head Assay	g Au/mt	g Ag/mt
Predicted		
Initial	0.57	40
Duplicate	0.66	41
Triplicate	0.77	50
Average	0.67	44

Ore Charge 1007.4 g

Solution Vol. 1.5111 L

Final Residue Wt 988.0 g

Natural pH 6.3

Tail Assay	g Au/mt	g Ag/mt
Initial	0.11	35
Duplicate	0.12	38
Triplicate	0.15	39
Average	0.13	37

Solid Density Wt. % 40.0

Cyanide Conc. Maintained at: 5.0 g/L

Raw Data

Leach Time	Solution Withdrawn			Reagents Applied		Sol. Analysis		Removed from pulp		
Hours	mL	NaCN (gpL)	pH	NaCN (g)	Lime (g)	Au (mg/L)	Ag (mg/L)	Au (mg)	Ag (mg)	NaCN (g)
0	-----	5.00	-----	7.56	1.00	-----	-----	-----	-----	-----
2	104	5.00	11.4	0.53	0.00	0.19	2.06	0.01976	0.21424	0.52
6	100	5.00	11.2	0.47	0.00	0.22	2.36	0.022	0.236	0.5
24	105	4.90	11.0	0.67	0.00	0.25	2.82	0.02625	0.2961	0.5145
48	113	4.85	10.9	0.78	0.00	0.24	3.04	0.02712	0.34352	0.54805
72	100	4.95	11.0	0.57	0.00	0.23	3.05	0.023	0.305	0.495
96	-----	4.85	11.0	-----	-----	0.22	3.06	-----	-----	-----

Metallurgical Results

Leach Time Hours	Cumulative Au Extraction mg	Cumulative Au Extraction g/mt ore	Cumulative Au Extraction % of total	Cumulative Ag Extraction mg	Cumulative Ag Extraction g/mt ore	Cumulative Ag Extraction % of total	Reagent Requirements Cumulative kg/mt ore: Cyanide Consumed	Reagent Requirements Cumulative kg/mt ore: Lime Added
0		0.000	0.0		0.000	0.0		1.0
2	0.287	0.285	49.1	3.113	3.090	7.2	0.00	1.0
6	0.352	0.350	60.3	3.780	3.753	8.7	0.01	1.0
24	0.420	0.416	71.8	4.712	4.677	10.9	0.13	1.0
48	0.431	0.428	73.7	5.340	5.301	12.3	0.36	1.0
72	0.443	0.439	75.8	5.699	5.657	13.2	0.44	1.0
96	0.451	0.45	77.6	6.019	6	14.0	0.67	1.0

	Au	% of Total	Ag	% of Total
Extracted g/mt ore	**0.45**	**77.6**	**6**	**14.0**
Tail assay, g/mt	**0.13**		**37**	
Calculated Head g/mt ore	**0.58**		**43**	
NaCN Consumed, kg/mt ore	**0.67**			
Lime Added, kg/mt ore	**1.0**			

Bottle Roll Test

Project No. **3829**
Test No. **CY-9**
Composite **Master Composite**
Feed Size **80%-75µm**

Head Assay	g Au/mt	g Ag/mt
Predicted		
Initial	0.57	40
Duplicate	0.66	41
Triplicate	0.77	50
Average	0.67	44

Ore Charge 999.8 g

Solution Vol. 1.4997 L

Final Residue Wt 921.0 g

Tail Assay	g Au/mt	g Ag/mt
Initial	0.06	13
Duplicate	0.06	13
Triplicate	0.06	13
Average	0.06	13

Natural pH 7.0

Solid Density Wt. % 40.0

Cyanide Conc. Maintained at: 5.0 g/L

Raw Data

Leach Time	Solution Withdrawn			Reagents Applied		Sol. Analysis		Removed from pulp		
Hours	mL	NaCN (gpL)	pH	NaCN (g)	Lime (g)	Au (mg/L)	Ag (mg/L)	Au (mg)	Ag (mg)	NaCN (g)
0	-----	5.00	-----	7.50	1.30	-----	-----	-----	-----	-----
2	106	4.85	11.1	0.74	0.00	0.27	12.92	0.02862	1.36952	0.5141
6	100	5.00	11.1	0.50	0.00	0.28	12.17	0.028	1.217	0.5
24	114	4.80	11.0	0.85	0.00	0.28	11.36	0.03192	1.29504	0.5472
48	114	4.85	11.5	0.78	0.00	0.26	11.34	0.02964	1.29276	0.5529
72	109	5.00	11.1	0.55	0.00	0.24	9.94	0.02616	1.08346	0.545
96	-----	4.90	11.2	-----	-----	0.22	9.37	-----	-----	-----

Metallurgical Results

Leach Time	Cumulative Au Extraction			Cumulative Ag Extraction			Reagent Requirements Cumulative kg/mt ore	
Hours	mg	g/mt ore	% of total	mg	g/mt ore	% of total	Cyanide Consumed	Lime Added
0		0.000	0.0		0.000	0.0		1.3
2	0.405	0.405	76.4	19.376	19.380	58.7	0.23	1.3
6	0.449	0.449	84.6	19.621	19.625	59.5	0.23	1.3
24	0.477	0.477	89.9	19.623	19.627	59.5	0.53	1.3
48	0.478	0.479	90.3	20.888	20.892	63.3	0.76	1.3
72	0.478	0.478	90.2	20.081	20.085	60.9	0.76	1.3
96	0.474	0.47	88.7	20.310	20	60.6	0.91	1.3

	Au	**% of Total**	**Ag**	**% of Total**
Extracted g/mt ore	**0.47**	**88.7**	**20**	**60.6**
Tail assay, g/mt	**0.06**		**13**	
Calculated Head g/mt ore	**0.53**		**33**	
NaCN Consumed, kg/mt ore	**0.91**			
Lime Added, kg/mt ore	**1.3**			

APPENDIX

Section 6 - Detailed Column Leach Test Results

3829 P-1

		NaCN added	379.72 g	NaCN	1.00 g/L solution		g/mt ore

Kilograms	71.97	NaCN Consumption	1.56 kg/mt ore				Au / Ag
						Head Grade	0.38 / 25
Metric Tons	0.072	Lime:	1.7 kg/mt ore			Head Screen	0.34 / 25
						Tail Screen	0.04 / 20

Daily Column Leach Test Data,
Sample I.D. Surface Composite

Feed Size 80%-19mm

		Pregnant Solution Analyses					Barren Solution Analyses		Au Extraction		Ag Extraction		NaCN	Au		Ag	
			NaCN														
Date	Days Leached	Vol. l.	Conc. g/l	pH	Au ppm	Ag ppm	Au ppm	Ag ppm	Cum. g/mt ore	Cum. %	Cum. g/mt ore	Cum. %	Consumed kg/mt ore	mg	cum. mg	mg	cum. mg
8/30	1								0.000	**0.0**	0.000	0.0	0.00	0.00	0.00	0.00	0.00
8/31	2								0.000	0.0	0.000	0.0	0.07	0.00	0.00	0.00	0.00
9/1	3	3.75	0.95	11.9	2.35	13.20	0.00	0.00	0.122	34.0	0.688	2.8	0.09	8.81	8.81	49.50	49.50
9/2	4	4.74	0.85	11.8	0.97	6.77	0.00	0.03	0.186	51.8	1.134	4.5	0.11	4.60	13.41	32.09	81.59
9/3	5	5.05	0.90	11.8	0.41	3.39	0.00	0.02	0.215	59.8	1.369	5.5	0.11	2.07	15.48	16.97	98.56
9/4	6	4.92	0.95	11.8	0.26	2.81	0.00	0.02	0.233	64.7	1.560	6.2	0.12	1.28	16.76	13.72	112.28
9/5	7	4.85	0.90	11.6	0.17	2.27	0.00	0.00	0.244	67.9	1.712	6.8	0.13	0.82	17.58	10.91	123.19
9/6	8	5.01	0.90	11.0	0.12	1.75	0.00	0.02	0.253	70.2	1.833	7.3	0.14	0.60	18.19	8.77	131.95
9/7	9	4.87	0.90	11.1	0.09	1.57	0.00	0.02	0.259	71.9	1.938	7.8	0.15	0.44	18.62	7.54	139.50
9/8	10	4.79	0.90	10.9	0.08	1.43	0.00	0.03	0.264	73.4	2.032	8.1	0.16	0.38	19.01	6.75	146.25
9/9	11	4.39	0.80	10.7	0.06	1.27	0.00	0.04	0.268	74.4	2.107	8.4	0.18	0.26	19.27	5.42	151.67
9/10	12	5.43	0.70	10.8	0.06	1.08	0.00	0.05	0.272	75.6	2.186	8.7	0.20	0.33	19.60	5.66	157.33
9/11	13	4.81	0.60	10.7	0.05	0.94	0.00	0.04	0.276	76.6	2.245	9.0	0.23	0.24	19.84	4.27	161.60
9/12	14	5.04	0.60	10.8	0.03	0.87	0.00	0.05	0.278	77.1	2.303	9.2	0.26	0.15	19.99	4.18	165.78
9/13	15	4.85	0.65	10.7	0.04	0.88	0.00	0.05	0.280	77.9	2.359	9.4	0.29	0.19	20.18	4.01	169.79
9/14	16	4.65	0.70	10.7	0.03	0.86	0.00	0.04	0.282	78.4	2.411	9.6	0.31	0.14	20.32	3.74	173.53
9/15	17	4.97	0.75	10.7	0.03	0.81	0.00	0.05	0.284	79.0	2.464	9.9	0.33	0.15	20.47	3.82	177.35
9/16	18	4.58	0.75	10.3	0.04	0.76	0.00	0.05	0.287	79.7	2.509	10.0	0.35	0.18	20.65	3.23	180.58
9/17	19	5.44	0.70	10.4	0.02	0.71	0.00	0.06	0.288	80.1	2.559	10.2	0.37	0.11	20.76	3.61	184.19
9/18	20	4.89	0.70	10.4	0.02	0.67	0.00	0.05	0.290	80.5	2.601	10.4	0.40	0.10	20.86	2.97	187.16
9/19	21	4.75	0.70	10.5	0.02	0.67	0.00	0.06	0.291	80.9	2.641	10.6	0.42	0.10	20.96	2.93	190.09
9/20	22	4.86	0.70	10.3	0.02	0.65	0.00	0.07	0.293	81.3	2.681	10.7	0.44	0.10	21.05	2.85	192.94
9/21	23	4.87	0.70	10.5	0.02	0.65	0.00	0.06	0.294	81.6	2.720	10.9	0.47	0.10	21.15	2.81	195.75
9/22	24	4.55	0.80	10.6	0.02	0.65	0.00	0.06	0.295	82.0	2.757	11.0	0.49	0.09	21.24	2.65	198.40
9/23	25	5.87	0.80	10.4	0.01	0.51	0.00	0.08	0.296	82.2	2.794	11.2	0.49	0.06	21.30	2.69	201.09
9/24	26	4.62	0.75	10.3	0.00	0.59	0.00	0.09	0.296	82.2	2.826	11.3	0.52	0.00	21.30	2.32	203.40
9/25	27	4.99	0.75	10.3	0.00	0.57			0.296	82.2	2.859	11.4	0.54	0.00	21.30	2.39	205.79
9/26	28		Rest Cycle														
10/9	41						0.00	0.08					0.54	0.00	21.30	0.00	205.79
10/10	42	4.68	0.50	10.3	0.08	3.65	0.00	0.25	0.301	83.7	3.091	12.4	0.57	0.37	21.67	16.67	222.46
10/11	43	4.89	0.65	10.4	0.04	1.61	0.00	0.17	0.304	84.4	3.183	12.7	0.60	0.20	21.87	6.60	229.06
10/12	44	4.94	0.70	10.6	0.03	0.83	0.00	0.13	0.306	85.0	3.228	12.9	0.62	0.15	22.02	3.23	232.29
10/13	45	4.29	0.75	10.6	0.00	0.67	0.00	0.11	0.306	85.0	3.258	13.0	0.65	0.00	22.02	2.21	234.51
10/14	46	5.27	0.75	10.5	0.00	0.60	0.00	0.14	0.306	85.0	3.295	13.2	0.67	0.00	22.02	2.60	237.11
10/15	47	5.20	0.80	10.5	0.02	0.46	0.00	0.15	0.307	85.4	3.318	13.3	0.68	0.10	22.12	1.68	238.78
10/16	48	4.91	0.80	10.5	0.00	0.48			0.307	85.4	3.340	13.4	0.69	0.00	22.12	1.59	240.38
10/17	49		Rest Cycle														
10/30	62						0.00	0.15					0.69	0.00	22.12	0.00	240.38
10/31	63	4.68	0.55	10.0	0.04	2.38	0.00	0.26	0.310	86.1	3.484	13.9	0.73	0.19	22.31	10.37	250.75
11/1	64	5.00	0.70	10.1	0.00	1.22	0.00	0.16	0.310	86.1	3.550	14.2	0.75	0.00	22.31	4.77	255.52
11/2	65	4.92	0.70	10.3	0.00	0.72	0.00	0.20	0.310	86.1	3.588	14.4	0.77	0.00	22.31	2.73	258.25
11/3	66	5.02	0.80	10.3	0.00	0.59	0.00	0.18	0.310	86.1	3.615	14.5	0.79	0.00	22.31	1.94	260.19
11/4	67	4.54	0.85	10.2	0.00	0.54	0.00	0.17	0.310	86.1	3.637	14.5	0.81	0.00	22.31	1.53	261.73
11/5	68	5.32	0.85	10.2	0.02	0.45	0.00	0.19	0.311	86.5	3.658	14.6	0.82	0.11	22.42	1.53	263.25
11/6	69	5.02	0.80	10.2	0.03	0.44			0.314	87.1	3.675	14.7	0.83	0.15	22.57	1.24	264.49
11/7	70		Rest Cycle														
11/20	83						0.00	0.23					0.83	0.00	22.57	0.00	264.49
11/21	84	4.46	0.60	10.0	0.04	2.37	0.01	0.32	0.316	87.8	3.806	15.2	0.86	0.18	22.74	9.40	273.89
11/22	85	4.92	0.75	10.2	0.02	1.09	0.02	0.28	0.317	88.0	3.857	15.4	0.88	0.05	22.79	3.73	277.62
11/23	86	4.88	0.70	10.2	0.00	0.73	0.00	0.28	0.315	87.6	3.887	15.5	0.91	-0.10	22.69	2.13	279.76
11/24	87	4.88	0.75	10.3	0.00	0.59	0.00	0.26	0.315	87.6	3.907	15.6	0.93	0.00	22.69	1.45	281.21
11/25	88	4.92	0.70	10.2	0.01	0.51	0.00	0.25	0.316	87.8	3.924	15.7	0.95	0.05	22.74	1.18	282.39
11/26	89	5.00	0.75	10.2	0.00	0.50	0.00	0.26	0.316	87.8	3.941	15.8	0.97	0.00	22.74	1.23	283.61
11/27	90	4.93	0.75	10.3	0.00	0.51			0.316	87.8	3.957	15.8	0.99	0.00	22.74	1.19	284.80
11/28	91		Rest Cycle														
12/11	104						0.00	0.28					0.99	0.00	22.74	0.00	284.80
12/12	105	4.49	0.50	10.2	0.02	1.87	0.00	0.02	0.317	88.1	4.054	16.2	1.03	0.09	22.83	6.97	291.77
12/13	106	4.93	0.75	10.4	0.01	0.94	0.00	0.02	0.318	88.3	4.117	16.5	1.05	0.05	22.88	4.53	296.30
12/14	107	4.92	0.60	10.4	0.00	0.45	0.00	0.03	0.318	88.3	4.146	16.6	1.08	0.00	22.88	2.11	298.42
12/15	108	4.74	0.70	10.4	0.00	0.32	0.00	0.03	0.318	88.3	4.165	16.7	1.10	0.00	22.88	1.36	299.78
12/16	109	4.99	0.75	10.7	0.00	0.27	0.00	0.03	0.318	88.3	4.182	16.7	1.12	0.00	22.88	1.19	300.97
12/17	110	5.14	0.75	10.8	0.00	0.22	0.00	0.04	0.318	88.3	4.196	16.8	1.14	0.00	22.88	0.98	301.95
12/18	111	5.20	0.75	10.3	0.00	0.19			0.318	88.3	4.206	16.8	1.15	0.00	22.88	0.78	302.74
12/19	112		Rest Cycle														
1/1	125						0.00	0.05					1.15	0.00	22.88	0.00	302.74
1/2	126	4.41	0.55	10.1	0.01	1.52	0.00	0.08	0.318	88.5	4.296	17.2	1.19	0.04	22.92	6.45	309.18
1/3	127	4.86	0.65	10.3	0.01	0.68	0.00	0.08	0.319	88.7	4.336	17.3	1.22	0.05	22.97	2.90	312.08
1/4	128	4.94	0.65	10.4	0.01	0.40	0.00	0.07	0.32	88.9	4.358	17.4	1.25	0.05	23.02	1.57	313.65
1/5	129	4.93	0.75	10.4	0.00	0.31	0.00	0.06	0.32	88.9	4.374	17.5	1.26	0.00	23.02	1.17	314.82
1/6	130	4.89	0.85	10.3	0.01	0.29	0.00	0.07	0.32	88.9	4.390	17.6	1.28	0.05	23.07	1.11	315.93
1/7	131	4.93	0.75	10.4	0.00	0.25	0.00	0.07	0.32	88.9	4.402	17.6	1.30	0.00	23.07	0.88	316.81
1/8	132	5.00	0.75	10.4	0.00	0.23			0.32	88.9	4.413	17.7	1.32	0.00	23.07	0.79	317.60
1/9	133		Rest Cycle														
1/22	146						0.00	0.08					1.32	0.00	23.07	0.00	317.60

3829 P-1

		NaCN added	379.72 g	NaCN	1.00 g/L solution	
Kilograms	71.97	NaCN Consumption	1.56 kg/mt ore			
Metric Tons	0.072	Lime:	1.7 kg/mt ore			

	g/mt ore	
	Au	Ag
Head Grade	0.38	25
Head Screen	0.34	25
Tail Screen	0.04	20

Daily Column Leach Test Data,
Sample I.D. Surface Composite

Feed Size 80%-19mm

		Pregnant Solution Analyses					Barren Solution Analyses		Au Extraction		Ag Extraction		NaCN	Au		Ag	
			NaCN														
Date	Days Leached	Vol. l.	Conc. g/l	pH	Au ppm	Ag ppm	Au ppm	Ag ppm	Cum. g/mt ore	Cum. %	Cum. g/mt ore	Cum. %	Consumed kg/mt ore	mg	cum. mg	mg	cum. mg
1/23	147	4.44	0.50	10.2	0.01	1.33	0.00	0.16	0.32	88.9	4.489	18.0	1.36	0.04	23.11	5.50	323.10
1/24	148	5.16	0.70	10.4	0.00	0.61	0.00	0.14	0.32	88.9	4.522	18.1	1.38	0.00	23.11	2.33	325.43
1/25	149	4.88	1.00	12.0	0.00	0.44	0.00	0.13	0.32	88.9	4.542	18.2	1.38	0.00	23.11	1.43	326.86
1/26	150	4.82	0.75	10.3	0.00	0.38	0.00	0.12	0.32	88.9	4.558	18.2	1.40	0.00	23.11	1.17	328.03
1/27	151	5.18	0.75	10.3	0.00	0.29	0.00	0.13	0.32	88.9	4.570	18.3	1.42	0.00	23.11	0.89	328.92
1/28	152	1.35	0.65	10.3	0.00	0.40	0.00	0.11	0.32	88.9	4.574	18.3	1.44	0.00	23.11	0.24	329.16
1/29	153	5.21	0.80	10.4	0.00	0.30			0.32	88.9	4.587	18.3	1.45	0.00	23.11	1.00	330.16
1/30	154			Rest Cycle													
2/12	167						0.00	0.12					1.45	0.00	23.11	0.00	330.16
2/13	168	4.51	0.55	10.2	0.00	1.22	0.00	0.18	0.32	88.9	4.655	18.6	1.49	0.00	23.11	4.89	335.05
2/14	169	4.94	0.75	10.5	0.00	0.59	0.00	0.14	0.32	88.9	4.683	18.7	1.51	0.00	23.11	2.00	337.05
2/15	170	4.90	0.70	10.3	0.00	0.45	0.00	0.16	0.32	88.9	4.704	18.8	1.53	0.00	23.11	1.49	338.54
2/16	171	4.99	0.75	10.3	0.01	0.33	0.00	0.14	0.32	88.9	4.715	18.9	1.55	0.05	23.16	0.83	339.37
2/17	172	4.93	0.80	10.2	0.00	0.31	0.00	0.12	0.32	88.9	4.727	18.9	1.56	0.00	23.16	0.81	340.18
2/18	173	5.01	0.80	10.3	0.00	0.29	0.00	0.13	0.32	88.9	4.738	19.0	1.58	0.00	23.16	0.84	341.03
2/19	174	4.92	0.75	10.3	0.00	0.28			0.32	88.9	4.748	19.0	1.60	0.00	23.16	0.71	341.74
2/20	175			Rest Cycle													
				Rinse Cycle													
3/1	184	0.47	0.10	9.7	0.00	0.42			0.32	88.9	4.751	19.0	1.60	0.00	23.16	0.20	341.94
3/2	185	4.34	0.40	10.4	0.00	0.75			0.32	88.9	4.796	19.2	1.57	0.00	23.16	3.26	345.19
3/3	186	5.07	0.10	10.2	0.00	0.28			0.32	88.9	4.816	19.3	1.57	0.00	23.16	1.42	346.61
3/4	187	5.01	0.10	10.3	0.00	0.16			0.32	88.9	4.827	19.3	1.56	0.00	23.16	0.80	347.41
3/5	188	4.93	0.00	10.3	0.00	0.11			0.32	88.9	4.835	19.3	1.56	0.00	23.16	0.54	347.96
3/6	189	5.15	0.00	10.2	0.00	0.06			0.32	88.9	4.839	19.4	1.56	0.00	23.16	0.31	348.26
3/7	190	4.62	0.00	10.2	0.00	0.04			0.32	88.9	4.842	19.4	1.56	0.00	23.16	0.18	348.45
				Drain Down													
3/13	196	**3.29**	0.00	9.3	0.00	0.03			0.32	88.9	5	20.0	1.56	0.00	23.16	0.10	348.55

	Au g/mt ore	Au %	Ag g/mt ore	Ag %
Extracted, g/mt ore	**0.32**	**88.9**	**5**	**20.0**
Tail , g/mt ore	**0.04**		**20**	
Calculated Head, g/mt ore	**0.36**		**25**	

3829 P-2

		NaCN added	423.30 g	NaCN	1.00 g/L solution
Kilograms	71.75	NaCN Consumption	1.93 kg/mt ore		
Metric Tons	0.072	Lime:	2.7 kg/mt ore		

	g/mt ore	

	Au	Ag
Head Grade	0.84	59
Head Screen	0.82	65
Tail Screen	0.12	44

Daily Column Leach Test Data,
Sample I.D. Underground Composite

Feed Size 80%-19mm

		Pregnant Solution Analyses					Barren Solution Analyses		Au Extraction		Ag Extraction		NaCN	Au		Ag	
			NaCN														
Date	Days Leached	Vol. l.	Conc. g/l	pH	Au ppm	Ag ppm	Au ppm	Ag ppm	Cum. g/mt ore	Cum. %	Cum. g/mt ore	Cum. %	Consumed kg/mt ore	mg	cum. mg	mg	cum. mg
8/30	1								0.000	0.0	0.000	0.0	0.00	0.00	0.00	0.00	0.00
8/31	2								0.000	0.0	0.000	0.0	0.07	0.00	0.00	0.00	0.00
9/1	3								0.000	0.0	0.000	0.0	0.14	0.00	0.00	0.00	0.00
9/2	4	4.07	0.35	9.0	4.88	21.20	0.00	0.03	0.277	35.5	1.203	2.3	0.19	19.86	19.86	86.28	86.28
9/3	5	5.32	0.70	9.9	1.72	10.60	0.00	0.03	0.404	51.8	1.986	3.8	0.21	9.15	29.01	56.24	142.52
9/4	6	4.19	0.65	10.0	1.02	7.83	0.01	0.07	0.464	59.5	2.442	4.7	0.25	4.27	33.29	32.65	175.18
9/5	7	5.11	0.60	10.2	0.59	5.05	0.00	0.03	0.505	64.8	2.796	5.4	0.27	2.96	36.25	25.45	200.63
9/6	8	5.24	0.70	10.0	0.34	3.82	0.00	0.05	0.530	68.0	3.073	5.9	0.29	1.78	38.03	19.86	220.49
9/7	9	4.85	0.80	10.3	0.23	3.17	0.00	0.05	0.546	69.9	3.284	6.3	0.31	1.12	39.15	15.12	235.61
9/8	10	3.99	0.75	10.3	0.20	3.08	0.00	0.05	0.557	71.4	3.451	6.6	0.34	0.80	39.94	12.03	247.64
9/9	11	4.73	0.70	10.2	0.14	2.69	0.00	0.08	0.566	72.6	3.625	7.0	0.37	0.66	40.61	12.47	260.11
9/10	12	5.88	0.70	10.3	0.12	2.28	0.00	0.13	0.576	73.8	3.806	7.3	0.38	0.71	41.31	13.00	273.11
9/11	13	4.66	0.70	10.2	0.09	1.97	0.00	0.10	0.582	74.6	3.925	7.5	0.40	0.42	41.73	8.52	281.63
9/12	14	4.94	0.70	10.4	0.08	1.87	0.00	0.14	0.587	75.3	4.047	7.8	0.43	0.40	42.13	8.73	290.36
9/13	15	4.73	0.65	10.2	0.07	1.72	0.00	0.13	0.592	75.9	4.150	8.0	0.46	0.33	42.46	7.42	297.78
9/14	16	4.53	0.65	10.2	0.06	1.58	0.00	0.13	0.596	76.4	4.241	8.2	0.49	0.27	42.73	6.49	304.27
9/15	17	4.86	0.60	10.3	0.07	1.42	0.01	0.14	0.600	77.0	4.328	8.3	0.52	0.34	43.07	6.24	310.51
9/16	18	4.52	0.50	10.0	0.05	1.23	0.00	0.15	0.603	77.3	4.395	8.5	0.56	0.18	43.25	4.85	315.36
9/17	19	5.42	0.45	10.0	0.06	1.10	0.00	0.17	0.607	77.9	4.468	8.6	0.59	0.33	43.57	5.20	320.55
9/18	20	4.82	0.50	10.0	0.03	0.96	0.00	0.14	0.609	78.1	4.520	8.7	0.63	0.14	43.72	3.76	324.31
9/19	21	4.78	0.55	10.1	0.03	0.96	0.00	0.15	0.611	78.4	4.574	8.8	0.66	0.14	43.86	3.87	328.19
9/20	22	4.58	0.60	10.0	0.03	0.97	0.00	0.16	0.613	78.6	4.625	8.9	0.70	0.14	44.00	3.68	331.87
9/21	23	4.80	0.65	10.2	0.03	0.98	0.00	0.16	0.615	78.9	4.679	9.0	0.73	0.14	44.14	3.89	335.75
9/22	24	4.52	0.70	10.3	0.02	0.96	0.00	0.16	0.616	79.0	4.729	9.1	0.75	0.09	44.23	3.52	339.28
9/23	25	5.89	0.75	10.1	0.03	0.84	0.00	0.20	0.619	79.3	4.786	9.2	0.76	0.18	44.41	4.13	343.41
9/24	26	4.44	0.75	10.0	0.02	0.84	0.00	0.22	0.620	79.5	4.824	9.3	0.79	0.09	44.50	2.71	346.12
9/25	27	4.91	0.75	10.1	0.02	0.89	0.00	0.21	0.622	79.7	4.869	9.4	0.81	0.10	44.59	3.25	349.37
9/26	28	4.93	0.80	10.2	0.02	0.92	0.00	0.28	0.623	79.9	4.917	9.5	0.82	0.10	44.69	3.46	352.83
9/27	29	4.92	0.75	10.4	0.02	0.82	0.00	0.23	0.624	80.0	4.954	9.5	0.84	0.10	44.79	2.61	355.44
9/28	30	4.67	0.75	10.4	0.02	0.78	0.00	0.24	0.626	80.2	4.988	9.6	0.86	0.09	44.88	2.47	357.91
9/29	31	4.93	0.75	10.4	0.02	0.80	0.00	0.25	0.627	80.4	5.026	9.7	0.88	0.10	44.98	2.72	360.63
9/30	32	5.14	0.75	10.4	0.00	0.83	0.00	0.33	0.627	80.4	5.068	9.7	0.90	0.00	44.98	2.99	363.62
10/1	33	4.71	0.70	10.4	0.00	0.86	0.00	0.33	0.627	80.4	5.101	9.8	0.93	0.00	44.98	2.37	365.98
10/2	34	4.89	0.80	10.1	0.00	0.86	0.00	0.30	0.627	80.4	5.136	9.9	0.94	0.00	44.98	2.52	368.51
10/3	35	4.29	0.75	10.2	0.01	0.91	0.00	0.31	0.628	80.5	5.169	9.9	0.97	0.04	45.03	2.37	370.88
10/4	36	4.54	0.80	10.3	0.01	0.93			0.628	80.5	5.206	10.0	0.99	0.05	45.07	2.64	373.52
10/5	37		Rest Cycle														
10/18	50						0.00	0.31					0.99	0.00	45.07	0.00	373.52
10/19	51	5.60	0.55	9.9	0.04	3.00	0.00	0.63	0.631	80.9	5.418	10.4	1.02	0.22	45.30	15.22	388.74
10/20	52	4.52	0.70	10.1	0.05	3.01	0.00	0.41	0.634	81.3	5.563	10.7	1.04	0.23	45.52	10.39	399.13
10/21	53	4.27	0.70	10.0	0.02	1.61	0.00	0.33	0.636	81.5	5.630	10.8	1.07	0.09	45.61	4.78	403.92
10/22	54	5.58	0.70	10.1	0.02	1.16	0.00	0.43	0.637	81.7	5.696	11.0	1.09	0.11	45.72	4.79	408.71
10/23	55	5.00	0.80	10.1	0.00	0.85	0.00	0.37	0.637	81.7	5.725	11.0	1.11	0.00	45.72	2.06	410.76
10/24	56	4.74	0.80	10.0	0.00	0.79	0.00	0.40	0.637	81.7	5.751	11.1	1.12	0.00	45.72	1.86	412.62
10/25	57	3.96	0.75	10.1	0.00	0.85			0.637	81.7	5.769	11.1	1.15	0.00	45.72	1.33	413.95
10/26	58		Rest Cycle														
11/8	71						0.00	0.37					1.15	0.00	45.72	0.00	413.95
11/9	72	5.39	0.55	9.9	0.03	2.45	0.00	0.82	0.639	82.0	5.927	11.4	1.18	0.16	45.88	11.32	425.27
11/10	73	4.36	0.65	10.1	0.03	2.49	0.00	0.60	0.641	82.2	6.020	11.6	1.22	0.13	46.01	6.67	431.94
11/11	74	5.40	0.70	10.1	0.02	1.48	0.00	0.64	0.643	82.4	6.089	11.7	1.23	0.11	46.12	4.93	436.87
11/12	75	4.79	0.75	10.2	0.01	1.18	0.00	0.59	0.643	82.5	6.122	11.8	1.25	0.05	46.17	2.39	439.26
11/13	76	4.89	0.75	10.1	0.00	1.03	0.00	0.54	0.643	82.5	6.150	11.8	1.27	0.00	46.17	2.03	441.29
11/14	77	4.88	0.80	10.1	0.00	0.97	0.00	0.59	0.643	82.5	6.178	11.9	1.29	0.00	46.17	1.98	443.27
11/15	78	4.84	0.75	10.2	0.00	0.93			0.643	82.5	6.199	11.9	1.31	0.00	46.17	1.49	444.76
11/16	79		Rest Cycle														
11/29	92						0.00	0.68					1.31	0.00	46.17	0.00	444.76
11/30	93	4.37	0.50	9.9	0.02	2.58	0.00	0.93	0.645	82.6	6.308	12.1	1.35	0.09	46.25	7.81	452.57
12/1	94	4.83	0.60	10.2	0.02	2.24	0.00	0.83	0.646	82.8	6.392	12.3	1.38	0.10	46.35	6.08	458.64
12/2	95	5.18	0.75	10.2	0.02	1.49	0.00	0.77	0.647	83.0	6.441	12.4	1.40	0.10	46.45	3.49	462.13
12/3	96	4.63	0.75	10.3	0.01	1.30	0.00	0.72	0.648	83.1	6.470	12.4	1.42	0.05	46.50	2.09	464.22
12/4	97	4.90	0.80	10.3	0.00	1.17	0.00	0.71	0.648	83.1	6.499	12.5	1.44	0.00	46.50	2.06	466.28
12/5	98	4.76	0.75	10.3	0.00	1.07	0.00	0.73	0.648	83.1	6.519	12.5	1.46	0.00	46.50	1.47	467.75
12/6	99	4.81	0.80	10.3	0.00	0.98			0.648	83.1	6.533	12.6	1.48	0.00	46.50	0.99	468.74
12/7	100		Rest Cycle														
12/20	113						0.00	0.71					1.48	0.00	46.50	0.00	468.74
12/21	114	4.24	0.45	10.1	0.02	2.45	0.00	0.00	0.649	83.2	6.627	12.7	1.52	0.08	46.59	6.77	475.51
12/22	115	4.52	0.65	10.3	0.00	2.28	0.00	0.04	0.649	83.2	6.771	13.0	1.55	0.00	46.59	10.31	485.82
12/23	116	5.02	0.80	10.4	0.00	1.22	0.00	0.04	0.649	83.2	6.853	13.2	1.57	0.00	46.59	5.92	491.74
12/24	117	5.11	0.75	10.2	0.01	0.53	0.00	0.06	0.650	83.3	6.888	13.2	1.59	0.05	46.64	2.50	494.24
12/25	118	5.01	0.70	10.4	0.02	0.35	0.00	0.09	0.651	83.5	6.909	13.3	1.61	0.10	46.74	1.45	495.69
12/26	119	4.84	0.70	10.5	0.01	0.26	0.00	0.07	0.652	83.6	6.920	13.3	1.63	0.05	46.79	0.80	496.49
12/27	120	4.66	0.85	10.6	0.00	0.29			0.652	83.6	6.934	13.3	1.65	0.00	46.79	0.99	497.48
12/28	121		Rest Cycle														
1/10	134						0.00	0.08					1.65	0.00	46.79	0.00	497.48

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		NaCN added	423.30 g	NaCN	1.00 g/L solution
Kilograms	71.75	NaCN Consumption	1.93 kg/mt ore		
Metric Tons	0.072	Lime:	2.7 kg/mt ore		

	g/mt ore	
	Au	Ag
Head Grade	0.84	59
Head Screen	0.82	65
Tail Screen	0.12	44

Daily Column Leach Test Data,
Sample I.D. Underground Composite

Feed Size 80%-19mm

		Pregnant Solution Analyses					Barren Solution Analyses		Au Extraction		Ag Extraction		NaCN	Au		Ag	
			NaCN														
Date	Days Leached	Vol. l.	Conc. g/l	pH	Au ppm	Ag ppm	Au ppm	Ag ppm	Cum. g/mt ore	Cum. %	Cum. g/mt ore	Cum. %	Consumed kg/mt ore	mg	cum. mg	mg	cum. mg
1/11	135	4.64	0.50	10.0	0.00	1.40	0.00	0.14	0.652	83.6	7.018	13.5	1.69	0.00	46.79	6.09	503.57
1/12	136	4.76	0.70	10.3	0.02	1.32	0.00	0.15	0.653	83.8	7.096	13.6	1.71	0.10	46.88	5.57	509.14
1/13	137	4.90	0.75	10.3	0.01	0.73	0.00	0.14	0.654	83.9	7.135	13.7	1.73	0.05	46.93	2.81	511.95
1/14	138	4.85	0.75	10.3	0.00	0.46	0.00	0.13	0.654	83.9	7.156	13.8	1.75	0.00	46.93	1.52	513.47
1/15	139	5.01	0.80	10.3	0.00	0.40	0.00	0.17	0.654	83.9	7.175	13.8	1.77	0.00	46.93	1.34	514.81
1/16	140	4.71	0.80	10.3	0.00	0.36	0.00	0.16	0.654	83.9	7.187	13.8	1.78	0.00	46.93	0.83	515.64
1/17	141	4.79	0.80	10.4	0.00	0.38			0.654	83.9	7.201	13.8	1.80	0.00	46.93	1.00	516.64
1/18	142			Rest Cycle													
1/31	155						0.00	0.20					1.80	0.00	46.93	0.00	516.64
2/1	156	4.50	0.55	10.1	0.02	1.34	0.00	0.27	0.655	84.0	7.270	14.0	1.84	0.09	47.02	5.01	521.65
2/2	157	4.83	0.75	10.5	0.01	1.24	0.00	0.29	0.656	84.1	7.335	14.1	1.86	0.05	47.07	4.61	526.27
2/3	158	5.12	0.75	10.3	0.01	0.74	0.00	0.30	0.657	84.2	7.367	14.2	1.88	0.05	47.12	2.31	528.57
2/4	159	4.71	0.75	10.4	0.01	0.59	0.00	0.26	0.66	84.6	7.384	14.2	1.90	0.05	47.17	1.25	529.82
2/5	160	4.85	0.80	10.3	0.01	0.53	0.00	0.26	0.66	84.6	7.402	14.2	1.92	0.05	47.21	1.24	531.07
2/6	161	4.57	0.80	10.5	0.00	0.49	0.00	0.25	0.66	84.6	7.414	14.3	1.94	0.00	47.21	0.91	531.98
2/7	162	5.07	0.80	10.5	0.00	0.49			0.66	84.6	7.431	14.3	1.95	0.00	47.21	1.21	533.19
2/8	163			Rest Cycle													
2/21	176						0.00	0.30					1.95	0.00	47.21	0.00	533.19
2/22	177	4.41	0.50	10.1	0.00	1.39	0.00	0.40	0.66	84.6	7.495	14.4	1.99	0.00	47.21	4.60	537.79
2/23	178	5.01	0.70	10.4	0.00	1.22	0.00	0.42	0.66	84.6	7.552	14.5	2.01	0.00	47.21	4.07	541.86
2/24	179	4.92	0.75	10.3	0.01	0.77	0.00	0.35	0.66	84.6	7.575	14.6	2.03	0.05	47.26	1.65	543.51
2/25	180	4.75	0.75	10.3	0.00	0.72	0.00	0.38	0.66	84.6	7.598	14.6	2.05	0.00	47.26	1.64	545.14
2/26	181	4.84	0.80	10.3	0.01	0.62	0.00	0.37	0.66	84.6	7.613	14.6	2.07	0.05	47.31	1.06	546.21
2/27	182	4.58	0.80	10.4	0.01	0.59			0.66	84.6	7.624	14.7	2.09	0.05	47.36	0.82	547.02
				Rinse Cycle													
3/1	184	5.70	0.80	10.4	0.00	0.61			0.66	84.6	7.672	14.8	2.03	0.00	47.36	3.48	550.50
3/2	185	4.21	0.90	10.4	0.00	0.64			0.66	84.6	7.710	14.8	1.97	0.00	47.36	2.69	553.19
3/3	186	4.78	0.45	10.4	0.00	0.43			0.66	84.6	7.739	14.9	1.95	0.00	47.36	2.06	555.25
3/4	187	4.63	0.20	10.5	0.01	0.25			0.66	84.6	7.755	14.9	1.93	0.05	47.40	1.16	556.41
3/5	188	4.86	0.05	10.6	0.00	0.16			0.66	84.6	7.766	14.9	1.93	0.00	47.40	0.78	557.18
3/6	189	5.07	0.00	10.5	0.00	0.10			0.66	84.6	7.773	14.9	1.93	0.00	47.40	0.51	557.69
3/7	190	4.35	0.00	10.5	0.00	0.08			0.66	84.6	7.778	15.0	1.93	0.00	47.40	0.35	558.04
				Drain Down													
3/15	198	**4.05**	0.00	9.2	0.00	0.10			0.66	84.6	8	15.4	1.93	0.00	47.40	0.41	558.44

	Au g/mt ore	Au %	Ag g/mt ore	Ag %
Extracted, g/mt ore	**0.66**	**84.6**	**8**	**15.4**
Tail , g/mt ore	**0.12**		**44**	
Calculated Head, g/mt ore	**0.78**		**52**	

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		NaCN added	423.30 g	NaCN	1.00 g/L solution		g/mt ore	

Kilograms	71.95	NaCN Consumption	1.86 kg/mt ore				Au	Ag
						Head Grade	0.68	44
Metric Tons	0.072	Lime:	2.00 kg/mt ore			Head Screen	0.79	47
						Tail Screen	0.10	40

Daily Column Leach Test Data,
Sample I.D. Master Composite

Feed Size 80%-19mm

		Pregnant Solution Analyses					Barren Solution Analyses		Au Extraction		Ag Extraction		NaCN	Au		Ag	
			NaCN														
Date	Days Leached	Vol. l.	Conc. g/l	pH	Au ppm	Ag ppm	Au ppm	Ag ppm	Cum. g/mt ore	Cum. %	Cum. g/mt ore	Cum. %	Consumed kg/mt ore	mg	cum. mg	mg	cum. mg
8/30	1								0.000	0.0	0.000	0.0	0.00	0.00	0.00	0.00	0.00
8/31	2								0.000	0.0	0.000	0.0	0.07	0.00	0.00	0.00	0.00
9/1	3	1.94	0.55	10.2	5.70	29.30	0.01	0.04	0.154	21.1	0.790	1.6	0.13	11.06	11.06	56.84	56.84
9/2	4	4.70	0.80	11.8	2.29	13.80	0.00	0.03	0.303	41.4	1.689	3.5	0.15	10.71	21.77	64.66	121.50
9/3	5	5.11	0.80	11.8	1.33	10.30	0.00	0.04	0.397	54.4	2.418	5.0	0.16	6.80	28.57	52.48	173.98
9/4	6	4.99	0.80	11.6	0.62	5.69	0.01	0.06	0.440	60.3	2.810	5.9	0.18	3.09	31.66	28.19	202.17
9/5	7	4.92	0.85	11.2	0.41	4.35	0.00	0.05	0.467	64.0	3.103	6.5	0.19	1.97	33.63	21.10	223.26
9/6	8	5.17	0.85	10.6	0.28	3.61	0.00	0.06	0.487	66.8	3.359	7.0	0.20	1.45	35.07	18.41	241.67
9/7	9	4.97	0.75	10.6	0.22	3.09	0.00	0.05	0.503	68.9	3.568	7.4	0.22	1.09	36.17	15.05	256.72
9/8	10	4.89	0.90	10.6	0.18	2.75	0.00	0.08	0.515	70.5	3.751	7.8	0.23	0.88	37.05	13.19	269.92
9/9	11	4.58	0.90	10.4	0.13	2.46	0.00	0.08	0.523	71.7	3.902	8.1	0.24	0.60	37.64	10.86	280.77
9/10	12	5.58	0.85	10.4	0.13	2.11	0.00	0.13	0.533	73.0	4.060	8.5	0.24	0.73	38.37	11.37	292.14
9/11	13	5.02	0.75	10.3	0.08	1.72	0.00	0.10	0.539	73.8	4.171	8.7	0.26	0.40	38.77	7.97	300.11
9/12	14	5.04	0.70	10.3	0.08	1.57	0.00	0.12	0.544	74.6	4.274	8.9	0.29	0.40	39.17	7.40	307.51
9/13	15	4.91	0.60	10.3	0.06	1.45	0.00	0.12	0.549	75.1	4.364	9.1	0.32	0.29	39.47	6.51	314.02
9/14	16	4.88	0.45	10.2	0.06	1.30	0.00	0.11	0.553	75.7	4.444	9.3	0.36	0.29	39.76	5.73	319.75
9/15	17	4.98	0.45	10.4	0.06	1.18	0.00	0.10	0.557	76.3	4.518	9.4	0.40	0.30	40.06	5.32	325.07
9/16	18	4.77	0.50	10.1	0.05	1.10	0.00	0.11	0.560	76.7	4.584	9.5	0.43	0.24	40.30	4.74	329.81
9/17	19	5.22	0.60	10.2	0.05	1.07	0.00	0.13	0.564	77.2	4.654	9.7	0.46	0.26	40.56	5.02	334.83
9/18	20	4.94	0.65	10.1	0.04	1.04	0.00	0.12	0.566	77.6	4.716	9.8	0.49	0.20	40.76	4.47	339.31
9/19	21	5.05	0.65	10.1	0.04	0.99	0.00	0.15	0.569	78.0	4.777	10.0	0.51	0.20	40.96	4.39	343.69
9/20	22	4.92	0.65	10.0	0.03	0.98	0.00	0.16	0.571	78.3	4.833	10.1	0.54	0.15	41.11	4.06	347.75
9/21	23	4.98	0.70	10.2	0.03	1.02	0.00	0.16	0.573	78.5	4.892	10.2	0.56	0.15	41.26	4.26	352.01
9/22	24	4.82	0.75	10.3	0.02	1.02	0.00	0.17	0.575	78.7	4.949	10.3	0.58	0.10	41.35	4.10	356.11
9/23	25	5.64	0.75	10.2	0.02	0.87	0.00	0.20	0.576	78.9	5.006	10.4	0.59	0.11	41.46	4.04	360.15
9/24	26	4.79	0.75	10.1	0.02	0.91	0.00	0.22	0.578	79.1	5.052	10.5	0.61	0.10	41.56	3.34	363.49
9/25	27	5.06	0.75	10.1	0.02	0.92	0.00	0.20	0.579	79.3	5.101	10.6	0.63	0.10	41.66	3.53	367.03
9/26	28	5.05	0.75	10.3	0.02	0.96	0.00	0.08	0.580	79.5	5.154	10.7	0.65	0.10	41.76	3.83	370.85
9/27	29	5.11	0.75	10.4	0.02	0.84	0.00	0.22	0.582	79.7	5.208	10.9	0.67	0.10	41.86	3.88	374.74
9/28	30	4.96	0.75	10.4	0.02	0.80	0.00	0.23	0.583	79.9	5.248	10.9	0.69	0.10	41.96	2.85	377.58
9/29	31	5.11	0.75	10.4	0.01	0.83	0.00	0.25	0.584	80.0	5.291	11.0	0.71	0.05	42.02	3.07	380.65
9/30	32	5.17	0.80	10.4	0.00	0.82	0.00	0.31	0.584	80.0	5.332	11.1	0.72	0.00	42.02	2.96	383.62
10/1	33	4.86	0.75	10.4	0.01	0.89	0.00	0.28	0.585	80.1	5.370	11.2	0.74	0.05	42.06	2.74	386.36
10/2	34	4.96	0.75	10.1	0.02	0.88	0.00	0.27	0.586	80.3	5.411	11.3	0.76	0.10	42.16	2.94	389.30
10/3	35	4.52	0.70	10.2	0.02	0.89	0.00	0.29	0.587	80.4	5.447	11.3	0.79	0.09	42.25	2.65	391.94
10/4	36	4.66	0.75	10.3	0.01	0.89			0.588	80.5	5.485	11.4	0.81	0.05	42.30	2.67	394.61
10/5	37		Rest Cycle														
10/18	50						0.00	0.29					0.81	0.00	42.30	0.00	394.61
10/19	51	5.62	0.45	9.9	0.08	3.70	0.00	0.67	0.594	81.4	5.753	12.0	0.84	0.45	42.75	19.32	413.93
10/20	52	4.81	0.60	10.1	0.05	2.39	0.00	0.41	0.597	81.8	5.865	12.2	0.87	0.24	42.99	8.08	422.01
10/21	53	4.46	0.65	10.0	0.03	1.51	0.00	0.33	0.599	82.1	5.930	12.4	0.90	0.13	43.12	4.64	426.65
10/22	54	5.64	0.75	10.1	0.03	1.12	0.00	0.42	0.602	82.4	5.994	12.5	0.92	0.17	43.29	4.63	431.28
10/23	55	5.14	0.75	10.2	0.00	0.86	0.00	0.38	0.602	82.4	6.026	12.6	0.93	0.00	43.29	2.28	433.56
10/24	56	4.94	0.75	10.1	0.01	0.82	0.00	0.41	0.602	82.5	6.055	12.6	0.95	0.05	43.34	2.11	435.67
10/25	57	4.23	0.70	10.1	0.01	0.86			0.603	82.6	6.077	12.7	0.98	0.04	43.38	1.55	437.22
10/26	58		Rest Cycle														
11/8	71						0.00	0.38					0.98	0.00	43.38	0.00	437.22
11/9	72	5.44	0.45	9.9	0.05	3.01	0.00	0.88	0.607	83.1	6.277	13.1	1.02	0.27	43.66	14.44	451.66
11/10	73	4.65	0.55	10.1	0.03	2.15	0.00	0.62	0.609	83.4	6.354	13.2	1.06	0.14	43.80	5.51	457.17
11/11	74	5.44	0.65	10.1	0.02	1.48	0.00	0.62	0.610	83.6	6.422	13.4	1.08	0.11	43.91	4.89	462.06
11/12	75	4.69	0.75	10.2	0.01	1.25	0.00	0.58	0.611	83.7	6.459	13.5	1.10	0.05	43.95	2.70	464.76
11/13	76	5.21	0.80	10.1	0.00	1.06	0.00	0.57	0.611	83.7	6.495	13.5	1.11	0.00	43.95	2.56	467.32
11/14	77	5.03	0.75	10.2	0.00	0.98	0.00	0.63	0.611	83.7	6.523	13.6	1.13	0.00	43.95	2.02	469.34
11/15	78	4.99	0.75	10.2	0.00	0.98			0.611	83.7	6.547	13.6	1.15	0.00	43.95	1.68	471.02
11/16	79		Rest Cycle														
11/29	92						0.00	0.70					1.15	0.00	43.95	0.00	471.02
11/30	93	4.46	0.45	10.1	0.04	3.14	0.00	0.89	0.613	84.0	6.692	13.9	1.19	0.18	44.13	10.43	481.46
12/1	94	5.04	0.50	10.3	0.02	2.05	0.00	0.86	0.615	84.2	6.772	14.1	1.23	0.10	44.23	5.79	487.25
12/2	95	5.31	0.75	10.2	0.01	1.48	0.00	0.81	0.615	84.3	6.820	14.2	1.24	0.05	44.28	3.47	490.72
12/3	96	4.79	0.75	10.3	0.00	1.34	0.00	0.74	0.615	84.3	6.852	14.3	1.26	0.00	44.28	2.29	493.01
12/4	97	5.06	0.75	10.3	0.00	1.21	0.00	0.77	0.615	84.3	6.885	14.3	1.28	0.00	44.28	2.35	495.36
12/5	98	4.95	0.75	10.3	0.00	1.11	0.00	0.76	0.615	84.3	6.907	14.4	1.30	0.00	44.28	1.57	496.92
12/6	99	4.75	0.75	10.3	0.00	1.05			0.615	84.3	6.922	14.4	1.32	0.00	44.28	1.11	498.04
12/7	100		Rest Cycle														
12/20	113						0.00	0.69					1.32	0.00	44.28	0.00	498.04
12/21	114	4.72	0.55	10.3	0.04	2.90	0.00	0.03	0.618	84.7	7.063	14.7	1.36	0.19	44.47	10.17	508.21
12/22	115	4.94	0.65	10.4	0.02	1.99	0.00	0.05	0.619	84.9	7.198	15.0	1.38	0.10	44.57	9.68	517.88
12/23	116	4.83	0.65	10.4	0.00	0.99	0.00	0.05	0.619	84.9	7.261	15.1	1.41	0.00	44.57	4.53	522.41
12/24	117	5.21	0.75	10.2	0.00	0.53	0.00	0.07	0.619	84.9	7.296	15.2	1.43	0.00	44.57	2.51	524.92
12/25	118	5.19	0.70	10.4	0.00	0.40	0.00	0.11	0.619	84.9	7.319	15.2	1.45	0.00	44.57	1.72	526.63
12/26	119	4.98	0.70	10.5	0.00	0.33	0.00	0.09	0.619	84.9	7.335	15.3	1.47	0.00	44.57	1.08	527.72
12/27	120	4.80	0.75	10.6	0.00	0.35			0.619	84.9	7.351	15.3	1.49	0.00	44.57	1.22	528.94
12/28	121		Rest Cycle														
1/10	134						0.00	0.09					1.49	0.00	44.57	0.00	528.94

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		NaCN added	423.30 g	NaCN	1.00 g/L solution	g/mt ore	
Kilograms	71.95	NaCN Consumption	1.86 kg/mt ore			Au	Ag
					Head Grade	0.68	44
Metric Tons	0.072	Lime:	2.00 kg/mt ore		Head Screen	0.79	47
					Tail Screen	0.10	40

Daily Column Leach Test Data,
Sample I.D. Master Composite

Feed Size 80%-19mm

		Pregnant Solution Analyses					Barren Solution Analyses		Au Extraction		Ag Extraction		NaCN	Au		Ag	
			NaCN														
Date	Days Leached	Vol. l.	Conc. g/l	pH	Au ppm	Ag ppm	Au ppm	Ag ppm	Cum. g/mt ore	Cum. %	Cum. g/mt ore	Cum. %	Consumed kg/mt ore	mg	cum. mg	mg	cum. mg
1/11	135	4.76	0.40	10.1	0.02	1.74	0.00	0.17	0.621	85.0	7.460	15.5	1.54	0.10	44.67	7.82	536.76
1/12	136	4.91	0.55	10.3	0.02	1.16	0.00	0.17	0.622	85.2	7.527	15.7	1.57	0.10	44.77	4.83	541.59
1/13	137	4.95	0.70	10.2	0.01	0.72	0.00	0.16	0.623	85.3	7.565	15.8	1.59	0.05	44.81	2.70	544.29
1/14	138	5.03	0.75	10.3	0.00	0.52	0.00	0.16	0.623	85.3	7.590	15.8	1.61	0.00	44.81	1.80	546.09
1/15	139	5.18	0.75	10.2	0.00	0.46	0.00	0.18	0.623	85.3	7.612	15.9	1.63	0.00	44.81	1.57	547.65
1/16	140	4.87	0.75	10.2	0.00	0.43	0.00	0.17	0.623	85.3	7.628	15.9	1.65	0.00	44.81	1.18	548.83
1/17	141	4.94	0.75	10.3	0.00	0.44			0.623	85.3	7.646	15.9	1.67	0.00	44.81	1.31	550.14
1/18	142		Rest Cycle														
1/31	155						0.00	0.20						0.00	44.81	0.00	550.14
2/1	156	4.60	0.50	10.4	0.03	1.82	0.00	0.30	0.625	85.6	7.748	16.1	1.71	0.14	44.95	7.35	557.49
2/2	157	4.96	0.55	10.4	0.01	1.14	0.00	0.28	0.625	85.7	7.806	16.3	1.74	0.05	45.00	4.12	561.61
2/3	158	5.41	0.65	10.2	0.00	0.76	0.00	0.29	0.625	85.7	7.843	16.3	1.76	0.00	45.00	2.68	564.30
2/4	159	4.89	0.75	10.3	0.00	0.63	0.00	0.26	0.625	85.7	7.865	16.4	1.78	0.00	45.00	1.60	565.90
2/5	160	5.06	0.75	10.3	0.00	0.56	0.00	0.25	0.625	85.7	7.886	16.4	1.80	0.00	45.00	1.51	567.41
2/6	161	4.76	0.75	10.4	0.00	0.51	0.00	0.25	0.625	85.7	7.902	16.5	1.82	0.00	45.00	1.15	568.56
2/7	162	5.22	0.75	10.4	0.00	0.50			0.625	85.7	7.921	16.5	1.84	0.00	45.00	1.34	569.89
2/8	163		Rest Cycle														
2/21	176						0.00	0.30					1.84	0.00	45.00	0.00	569.89
2/22	177	4.50	0.45	10.1	0.02	1.73	0.00	0.44	0.627	85.9	8	16.7	1.88	0.09	45.09	6.26	576.15
2/23	178	5.21	0.65	10.3	0.00	1.15	0.00	0.41	0.627	85.9	8	16.7	1.90	0.00	45.09	3.75	579.90
2/24	179	5.07	0.70	10.3	0.00	0.79	0.00	0.33	0.627	85.9	8	16.7	1.92	0.00	45.09	1.91	581.81
2/25	180	4.93	0.80	10.3	0.01	0.74	0.00	0.35	0.627	85.9	8	16.7	1.94	0.05	45.14	1.97	583.78
2/26	181	5.00	0.75	10.3	0.00	0.63	0.00	0.34	0.627	85.9	8	16.7	1.96	0.00	45.14	1.37	585.14
2/27	182	4.69	0.70	10.3	0.01	0.59			0.628	86.0	8	16.7	1.99	0.05	45.19	1.03	586.17
			Rinse Cycle														
3/1	184	5.88	0.70	10.4	0.00	0.59			0.628	86.0	8	16.7	1.93	0.00	45.19	3.47	589.64
3/2	185	4.46	0.80	10.4	0.00	0.61			0.628	86.0	8	16.7	1.88	0.00	45.19	2.72	592.36
3/3	186	4.77	0.20	10.3	0.00	0.34			0.628	86.0	8	16.7	1.86	0.00	45.19	1.62	593.99
3/4	187	5.11	0.10	10.4	0.00	0.19			0.628	86.0	8	16.7	1.86	0.00	45.19	0.97	594.96
3/5	188	4.86	0.00	10.4	0.00	0.15			0.628	86.0	8	16.7	1.86	0.00	45.19	0.73	595.68
3/6	189	5.26	0.00	10.2	0.00	0.09			0.628	86.0	8	16.7	1.86	0.00	45.19	0.47	596.16
3/7	190	4.37	0.00	10.2	0.00	0.08			0.628	86.0	8	16.7	1.86	0.00	45.19	0.35	596.51
			Drain Down														
3/15	198	**3.59**	0.00	9.1	0.00	0.10			0.63	86.3	8	16.7	1.86	0.00	45.19	0.36	596.87

Extracted, g/mt ore	**0.63**	**86.3**	**8**	**16.7**
Tail , g/mt ore	**0.10**		**40**	
Calculated Head, g/mt ore	**0.73**		**48**	

Table A6-1. - Drain Down Rate Tests, Column Leached Residues, Longstreet Mine Composites, 80%-19mm Feed Size

	Effluent Solution								
Drain	Surface Composite			Underground Composite			Master Composite		
Time, hours	Liters	Cum. L/mt ore	Rate, L/hr/mt	Liters	Cum. L/mt ore	Rate, L/hr/mt	Liters	Cum. L/mt ore	Rate, L/hr/mt
0.08	0.017	0.24	2.951	0.015	0.21	2.611	0.015	0.21	2.604
0.25	0.032	0.68	2.614	0.030	0.63	2.458	0.218	3.24	17.810
0.50	0.051	1.39	2.833	0.047	1.28	2.618	0.046	3.88	2.556
1.0	0.104	2.83	2.889	0.097	2.63	2.702	0.094	5.18	2.611
2.0	0.179	5.32	2.486	0.780	13.50	10.864	0.176	7.63	2.444
4.0	0.191	7.97	1.326	0.220	16.56	1.532	0.208	10.51	1.444
8.0	0.160	10.19	0.556	0.190	19.21	0.662	0.188	13.13	0.653
24	0.191	12.85	0.166	0.301	23.40	0.262	0.257	16.69	0.223
48	0.085	14.03	0.049	0.176	25.85	0.102	0.129	18.49	0.075
72	0.026	14.39	0.015	0.080	26.96	0.046	0.053	19.22	0.031
96	0.006	14.47	0.003	0.035	27.45	0.020	0.024	19.56	0.014
120				0.019	27.72	0.011	0.011	19.71	0.006
144				0.011	27.87	0.006	0.004	19.76	0.002